STATE OF OHIO DEPARTMENT OF HIGHWAYS

UI - 1057(4)

CUY-90-15.45 PROJECT NO. 43 OHIO UI 1057 (4)

> CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT CUY - 42R-17.50

> > PART 2

CUY - 42R - 17.50

# INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42R-175 CUYAHOGA COUNTY CITY OF CLEVELAND

# PART 2 SUBSTRUCTURE

THIS IMPROVEMENT HAS BEEN DECLARED A LIMITED ACCESS HIGHWAY OR FREEWAY BY ACTION OF THE DIRECTOR OF HIGHWAYS IN ACCORDANCE WITH THE PROVISIONS OF SECTION 5511. 02 REVISED CODE OF OHIO.

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38.39 DOCK WALL

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TITLE SHEET

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**EXISTING CONDITIONS** 10,11 RAILROAD TRACK MODIFICATIONS

40-43 CONSTRUCTION IN ERIE RAILROAD YARD 10,11,35 R.R. FORCE ACCOUNT WORK 12,13 EXISTING CONDITIONS AT PIER LOCATIONS 36A REVISED SHEET No. 36 14-22 PIER FOOTINGS

### LINE DATA

BEGIN PROJECT END PROJECT

UI - 1057(4)UI - 1057 (4)

STA. 16 + 13.02 STA. 43 + 34.72

2,721.7 LIN. FT. or 0.515 MILES NET LENGTH UI- 1057 (4) AND WORK

DELIVERY POINT - N.Y.C. & ST. L. R.R. FREIGHT STATION \* AVERAGE HAUL - ONE HALF MILE

THE STANDARD SPECIFICATIONS OF THE STATE OF OHIO DEPARTMENT OF HIGHWAYS INCLUDING CHANGES AND SUPPLEMENTAL SPECIFICATIONS LISTED IN THE PROPOSAL SHALL GOVERN THIS IMPROVEMENT. I HEREBY APPROVE THESE PLANS AND DECLARE THAT THE MAKING OF THIS IMPROVEMENT WILL NOT REQUIRE THE CLOSING TO TRAFFIC OF THE HIGHWAY

AND THAT PROVISIONS FOR THE MAINTENANCE AND SAFETY OF TRAFFIC WILL BE AS SET FORTH IN THE PLANS AND ESTIMATE. THE RIGHT OF WAY FOR THIS IMPROVEMENT WILL BE PROVIDED BY THE STATE

OF OHIO. Louis L. Drasler DATE 9-2-54 DIRECTOR OF PUBLIC SERVICE, CITY OF CLEVELAND DATE 9/19/54 DEPUTY DIRECTOR OF PLANNING AND PROGRAMMING 9-8-54 ENGINEER OF BRIDGES

DATE\_\_\_\_\_ENGINEER OF LOCATION & DESIGN DATE 8-31-54 CHIEF ENGINEER, ERIE RAILROAD

F. H. Simpson DATE 8-31-54 CHIEF ENGINEER, NEW YORK CENTRAL SYSTEM APPROVED

MAR 1 5 1962

DATE CHIEF ENGINEER, NEW YORK, CHICAGO AND SAINT LOUIS RAILROAD CO. PRINT APPROVED BY K. J. Wagoner DATE 9-2-54 CHIEF ENGINEER, BALTIMORE AND OHIO RAILROAD

HOWARD NEEDLES TAMMEN & BERGENDOFF CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK

CONTRACT NO.

H.G. SOURS ASSOCIATE COLUMBUS

00077 FILE NO. CUYAHOGA COUNTY DATE OF LETTING

LOCATION PLAN SCALE IN FEET PORTION TO BE IMPROVED

SUPPLEMENTAL SPECIFICATIONS NUMBER DATE DATE R. 3-/9-5 *1-24-5*3 M-101.7

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	NUMBER	DATE	NUMBER	DATE
*	I-8 MH No. 1	5-1-52		
*	G - 7.07	1-2-53		
* *	I-8MHNº1-A	6-1-54		
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ROUND PHOTOLA DEPARTMENT OF COMMERCE BUREAU OF PUBLIC ROADS

**APPROVED** 

DISTRICT ENGINEER

DATE

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ITEM	DESCRIPTION	TOTAL	UNIT	Pil	ER I	PIE	R 2	PIE	R 3	PIE	R 4	PIE	R 5	PIE	R 6	PIE	R 7	PIE	R 8	WEST E	ND PIER	EAST	<del></del>	STRUCTURE	1	PROJECT IN
and the second second second				IN	IS	2N	25	3N	38	4 N	45	5N	5S	6 N	65	7N	75	8 N	85	WN	WS	EN	ES	REMOVAL	SYSTEM	GENERAL
	Cofferdams, Cribs and Sheeting Unclassified Excavation	20 17,227	Each Cu. Yds.	/,395	1,419	829	8/6	975	1,035	802	975	829	916	82.9	829	776	975	1,150	776	543	610	355	393	·		
									7																	
	Class "E" Concrete , Footings Class "E" Concrete , above Footings	5,098 5,171	Cu. Yds.	395.6	395.6 177.7	308.0	351.3	395.4	395.4	308.0	395.7	308.0	395,7	308.2	308.0	308.0	395.7	307.9	307.9 184.6		/25./		140.4° 370.6			
υ-/ 	<u>-</u>	<u> </u>		1764	177.7	209.0	2,33.0	207.0	201.0	273.3	275.0	200.9.	200.9	210.2	210.2	200.1	400.1	104.0	104.0	200.0	170.0	370.0	7 370.0			
3-4	Reinforcing Steel	1,393,558	Lbs.	78,627	7 78,627	79,962	75,499	83,018	83,018	81,411	85,231	82,639	86,592	80,941	80,941	80,532	84,485	74,470	74,470	26,237	16,910	27, 980	31,968			
5-7	Structural Steel 17 160-17		, , , , , , , , , , , , , , , , , , ,	12.49	16.40	1575	1575	10.50	1017	1,617	1,622	1,608	1,608	1,608	1,617	1,608	1,608	1,449	1449	842	847	926	1,057			
<del></del>	Structural Steel Wrought Iron Ladder Rungs 60-17	+	425 Lbs.	1,649		1,575 399		1,617 406	1,617 406	413	413	427	427	427	427	4/3	4/3	280	280	224	119					
		1																								
5-8	ield Painting of Structural Steel 2 Coats	,	Lump Sur	<u>-</u>		-							;													
5-9	z" Sponge Rubber Expansion Joint Material Sec.M-10.02	7/6	59. Ft.		38.5	38.5	38.5	38.5	<i>38</i> .5	<i>3</i> 8.5	38.5	38.5	<i>3</i> 8.5	38.5	38.5	38.5	38.5	38.5	38.5	25.0	25.0	25.0	25.0		VENTON 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
S- 17	First Pile Test Load		1																							Lump Sum
		4 9 -5	Lump sum Each	7													<u> </u>	1								5
0 10		4570	Lin. Ft.																		2220					
3-10 S-18	Steel Bearing Piles (12 BP 53) 60-8 14" Cast-in-place Reinforced Concrete Piles 60-5,6861	728, 491 128, 491 2 113,045	Lin. Ft.	7740	7740	7.2.90	7200	8100	8100	7290	7740	6885	73/0	6/60	6480	5670	6020	4860	4860	2,400	2,280	1,680	1,920			
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	Removal of Existing Structure No.1 Removal of Existing Structure No.2		Lump sum																					/		
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	Removal of Existing Structure No. 4		Lump sum	7			- 1.																	1		
5-24	Removing Existing Concrete Pedestals which		Lump sum	7		<u> </u>																				Lump Sum
	WELL STATES WITH WEW COLLECTION		Larrip Sarri																							
S-25	Electrical Grounds		Lump sun	η																						Lump Sum
5-29	8" Wrought Iron Pipe , Including Specials	1,036	Lin.Ft.	33	33	59	59	59	59	6/	61	63	63	61	61	60	60	45	45	<b>3</b> 9	22	45	4.8			
	8" Pipe for Storm Sewers	6	Lin.Ft.		30		0,0											7,0							6	
	12" Pipe for Storm Sewers	1,333	Lin.Ft.								<u> </u>										:				1333 251	
I-2	IZ" Pipe for Storm Sewers under Pavement	251	Lin.Ft.																						201	
	15" Pipe for Storm Sewers 15" Extra Strength Reinforced Concrete Culvert Pipe	335	Lin.Ft.							1															335	
	Sec. M-6.6 (c) for Storm Sewers	288	Lin.Ft.						e i																288	
	18" Pipe for Storm Sewers under Pavement	80	Lin.Ft.																						80 142	
	21" Pipe for Storm Sewers 24" Pipe for Storm Sewers	932	Lin.Ft.																1						932	
<del></del>	24" Extra Strength Reinforced Concrete Pipe								-	- And the state of																
	Sec. M-6.6 (c) for Storm Sewers	290	Lin.Ff.		· · · · · · · · · · · · · · · · · · ·																				290	
I-2	24" Pipe for Storm Sewers Under Pavement	(16)	Lin.Ft.															***************************************							(1/6)-	-84
I-2	24" Paved Bituminous Coated Corrugated Metal Pipe,		90																						60-	- 01
I-2	Sec. M - 6.4 (d) for Storm Sewers 27" Paved Bituminous Coated Corrugated Metal Pipe,	60)	Lin.Ft.							:															OUF	20
	Sec. M-6.4 (d) for Storm Sewers	80	Lin. Ft.																						80	
I-2	36" Extra Strength Reinforced Concrete Culvert Pipe	3.4	, :_ ~·																						30	
	Sec. M-6.6 (c) for Storm Sewers	30	Lin.Ft.	<u></u>			***************************************								K			***************************************	· · · · · · · · · · · · · · · · · · ·	<u> </u>						
	Pipe Special , 12" 35° Wye	1	Each																							
	Pipe Specials, 8" to 12" Increaser Pipe Specials, 8" to 15" Increaser	16	Each Each																						16	
	Manholes , Standard No.1	16	Each																						16	
Spec.	Outlet Structure "C"	1 × 1 × 1 × 1	Lump sun																							
	Alteration to Manhole "A"  Alteration to Manhole "B"		Lump sum	<del></del>	1					- Lin-			<u> </u>													
I-8	Alteration to Maπhole "C"		Lump sun	n .																						
	Alteration to Manhole "D"  Alteration to Manhole "F"		Lump sum								1		1.													
	Outlet Structure "A"		Lump sum Lump sum	<del></del>						<u> </u>																
Spec.	Outlet Structure "B"		Lump sum	7																						
I-16	Removal of Manhole "E"		Lump sun		CHDDO	) T C		DIE	DAIL	DOAD	TDAC	CKC				<u> </u>				<u></u>	[					. :
ITE	DESCRIPTION	ТО	TAL U	NIT	SUPPOF ITEM	XI P	UR E	. ITIC. 1	RAIL	NUAU	TRAC	<u> </u>	DESC	RIPTION	<u></u>			<del></del>		· · · · · · · · · · · · · · · · · · ·		TOTAL	UNIT	_		
-1 & Spe	c. Roadway Excavation	5, 9	40 Cu.		-7 <b>¢</b> Spec	. Steel	sheet pi	ling inclu	iding re	einforcir	ng plate ,	steel H a	anchor p	oiles and s	steel wale	es, and til	nber con	nection a	ingles , for	r dock wa	211 848 8	77,000				
-4 & Spi		3,00	00 Cu.	Yds. S	:-7 ¢ Spec	c. Steel a	enchor ro	ods, turnbi	ickles, pipe	esleeves a	ind fastenin	ngs for doc	ckwalls (i	ncluding	payment	for neces	sary exc	avation,	sheeting	and brac	ring) 👸 🗷	13,500-	Pounds			
S-1 S-4	Class "E" concrete , anchor caps  Reinforcing steel in anchor caps	7, 9	·	. Yds. unds	S-13 Special			nber ten timber o	· · · · · · · · · · · · · · · · · · ·		ui, INClu	ding har	uware	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					· · · · · · · · · · · · · · · · · · ·			2.40 1,965	M.B.M. Sq. Ft.	<del></del>		
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FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	2
2	оню	UI 1057 (4)	1 1 N	43

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT CUY- 42 R - 17.50

### CONTINUATION OF GENERAL NOTES (From Sheet 3)

#### 32. PILING (Continued from Sheet 3)

An effort shall be made to avoid great differences in the penetrated length of the individual piles in a footing. In striving for additional penetration, beyond 65 tons, piles of relatively short penetration shall be driven to a greater rate of blows-per-foot than longer piles.

The Contractor shall submit to the Engineer, at least 15 days before the beginning of pile driving, for approval by the Director, a plan showing the order in which he proposes to drive the piles in a footing. It is intended that the piles nearest the middle of the footing be driven first, to insure as great penetration for them as for the outer piles, after which successive outer piles will be driven. piles will be driven.

PENCIL REVISIONS SEPT. 20, 1955

Revised As-Buill DLM. 12/30/57

U. S. ROUTE 42 RELOCATION

NNER BELT FREEWAY - CENTRAL VIADUCT

QUANTITIES

CLEVELAND CUYAHOGA COUNTY

SCALE NOME

MADE GA DATE 6-22-54

TRCD AH DATE 6-22-54

CKD JGS DATE 7-9-54

KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET- 1.02

PART 2

#### 1 DESIGN SPECIFICATIONS

\*Design Specifications for Highway Structures ... State of Ohio Department of Highways dated October, 1951 revised July 15, 1952 and April 1, 1954 (with a load frequency rating of CF 1200-SI) are used in the design of this project.

#### 2. CONSTRUCTION SPECIFICATIONS

"Construction and Material Specification". State of Ohio, Department of Highways. dated January 1, 1953, as modified by notes on the plans and in the proposal, shall

#### 3. SCOPE OF CONTRACT

Work scheduled in this contract consists of the construction of two end piers, piers ! through 8, the construction of storm sewers, a 200' dockwall section, railroad roadbed grading, the removal of certain fenders and two existing piers from the river, and removal of some of the masonry pedestals of the former Central Viaduct. The steel superstructure of the former Central Viaduct has been removed but the masonry substructure remains in place. All track work will be handled by railroad forces. Railroad grading and cribwall construction in the vicinity of Pier I will be done by the contractor.

#### 4. MINIMUM TEMPORARY CONSTRUCTION CLEARANCE FOR RAILROAD TRACKS

The minimum temporary construction clearance for railroad tracks shall be 2/4 - 0" vertically above top of rail and 8' - 0" horizontally from the centerline of the nearest track.

#### 5. REOPENING OF STREETS

When any street is closed to traffic, and not then permanently closed, work on that particular street shall be prosecuted to the fullest to allow for its reopening as soon as possible. Existing streets adjacent to the project shall remain open as long as possible.

#### 6. FIELD OFFICE

The contractor shall provide a suitable field office in accordance with sec. S+0.01(b) having a minimum of 300 sq. ft. of floor space. The contractor shall have a telephone installed and maintained for the duration of the contract.

#### 7. WORK BY THE CITY - OF CLEVELAND

Within the corporate limits of the city of Cleveland the city will perform any pavement repair due to sewer construction and will seal and fill (by mud jack) the existing sewers that are to be abandoned.

The city will also wreck and remove certain existing buildings within the limits of the easement lines. The city will wreck the buildings to the ground line or tops of foundations near the ground surface, or to the top of the existing cellar foundations and remove all the resulting debris.

#### 8. RAILROAD TRAFFIC

Portions of this project shall be constructed under traffic, and the contractor, to the satisfaction of the engineer, shall plan and conduct his operations so that traffic shall be maintained as herein specified.

At piers 1. 3. 4 and 5 construction operations will interfere with traffic on existing railroad tracks. The tracks will, in some cases, be relocated by the owners, and in other cases will be removed. Temporary trestles may be constructed to span across footing excavations, and the contractor shall coordinate his construction operations so as to interfere the least possible amount with train movements. Flagmen and watchmen shall be supplied as required by the railroads, at the expense of the contractor.

#### 9. BLASTING

Where blasting is necessary, the contractor will be required to take all necessary precautions to protect the work already completed and the adjacent property and he shall be responsible for any and all damage to the work or to adjacent property and injury to persons.

#### 10. BORINGS

The log of each of the test hole borings is shown on these plans.

#### 11. PILING (See also No. 31 on this sheet and No. 32 on Sheet 2.)

locations which were not checked in the preliminary test pile project.

The piles in the west end pier shall be 12BP53 steel bearing piles, and in Piers I through 8 and in the east end pier 14" cast-in-place reinforced concrete piles. Preliminary test piles were driven at this site and loaded. A copy of the report on this test pile project may be inspected by bidders in the Division Office of the Department of Highways at Cleveland or in the Bureau of Bridges at Columbus. Copies of this report will be made available to the Contractor for this substructure project and to the engineering personnel, and should be consulted as a guide in the driving of the piles. A first pile test load shall be applied where directed by the engineer. Subsequent test loads shall be applied if and where directed by the Engineer. The Engineer may direct a subsequent load to be applied on the same pile as a previous load or on another pile in the same footing or in a different footing. The maximum amount of load required shall be equal to 3R unless the "yield point" is reached at a lesser tonnage. The purpose of this testloading (im addition to that done in the preliminary test pile project) is to calibrate the capacity formula and determine the required number of blows per foot for the actual driving conditions which exist during construction (with respect to the type and size of hammer and the type, section and driven length of the pile) and/or to calibrate the formula for some

The nominal design capacity is 65 tons. The capacity formula shall be adjusted (according to test loading indications) to determine the number of blows per foot required to provide an "R" of 65 tons (that is, a "yield point" of 130 tons). After this rate of blows per foot has been attained, driving shall be continued to cause each pile to penetrate to an average penetration of 15 feet per pile

greatest length of penetration at which the rate of blows per foot for an R of 65 tons has been observed. However, this additional driving (beyond 65 tons) shall be stopped if damage to a pile becomes apparent. The total penetration per pile at the west end pier shall be not less than 60 feet, and at Piers I thru 8 and at the east end pier not less than 40 feet.

The hammer used shall have an energy rating of not less than 15,000°#, and the type and size of hammer used when the required length of penetration to provide an R of 65 tons is being attained shall be the same as used in the driving of the pertinent test-loaded pile. The average length of the piles is estimated as follows: West End Pier. 60 Feet; Pier I. 90 feet; Pier 2, 90 feet; Pier 3, 90 feet; Pier 4, 90 feet; Pier 5, 85 feet; Pier 6, 80 feet; Pier 7, 70 feet; Pier 8, 60 feet; and East End Pier, 40 feet.

#### 12. DISPOSAL OF SURPLUS EXCAVATION

The contractor shall be responsible for the disposal of any surplus excavation outside the limits of the right-of-way at his own expense.

#### 13. UTILITIES

Except as hereinafter provided any utility facilities encountered at the site of the work which will interfere with the construction of the substructure units included in this contract will be removed or relocated by others. The contractor shall coordinate his operations with the work of the utility owners, or others who may be making the re-

locations, and shall notify the owners of the utilities of his schedule sufficiently in advance to permit them to make the necessary alterations.

#### 14. INTERFERENCES WITH CONSTRUCTION

VICINITY OF WEST END PIER

University Road near the west end pier will be temporarilly closed to traffic. No utilities are known to exist which would interfere with pier construction.

#### VICINITY OF PIER 1

FLB 25 Pier I is located in the Erie Railroad yards southwest of the Cuyahoga River., Track relocation will be coordinated by the railroad company and the contractor during sewer, dockwall, roadbed and pier construction. See Note 30.

#### VICINITY OF PIER 2

The concrete drain trough from the wash stalls of the Goff-Kirby Ready-Mix Plant is to be reconstructed by the owners to clear the pier shafts.

Existing concrete pedestals of the old Central Viaduct which fall within the limits of footing 2N are to be removed by the Contractor before Pier 2N can be built.

#### VICINITY OF PIER 3

C.C.C. & St. L. Tracks will be relocated by the owners until the pier is completed. Truck wash stalls will be removed by the owner and rebuilt after pier construction is completed. One existing concrete pedestal of the old Central Viaduct must be removed by the contractor before Pier 3 can be built.

#### VICINITY OF PIER 4

One existing pedestal of the old Central Viaduct must be removed by the Contractor before Pier 4N can be built. One track of the C.C.C. & St. L. will be relocated by the owners prior to the beginning of construction.

#### VICINITY OF PIER 5

C.C.C. & St. L. tracks will be temporarily relocated by the Railroad Co. prior to the beginning of construction, at the site of Pier 55. A temporary trestle will be constructed by the Railroad Co. to bridge the C.C.C. & St. L. track over the corner of the excavation for Pier 5N. This work will be done prior to beginning construction at this site. The contractor's operations in excavating and pile driving must be coordinated with train movements on the C.C.C. & St. L. Track. Two existing pedestals of the old Central Viaduct must be removed by the contractor before Pier SN can be built. The railroad company

as shown on Sheet 11 One concrete pedestal of the old Central Viaduct must be removed by the contractor prior to beginning construction of Pier 6N. Pier 6S will be built on the site of a two story brick building owned by the United Garage and Service Corporation. The building will be removed by the City to the floor level. There is no basement but has a concrete floor with a lower level on the west side, roughly 15 ft by 40 ft. about 4 ft below the ground level. Two 10,000 gallon tanks and one 2,000 gallon tank are located below the floor and encased in concrete. The amount of encasement is not known. Plans for this structure are available 19. CONCRETE for review by bidders at the Division Office of the Department of Highways at Cleveland,

#### VICINITY OF PIER 7

An existing one story brick and frame building with a concrete floor at the site of Pier 7N will be removed by the City prior to the beginning of construction. Foundations and floor of this building shall be removed by the contractor and payment therefor will be made under "Item E-2. Unclassified Excavation." Manhole No. "E" in West 3rd Street and the existing 18" brick sewer shall be removed and rebuilt by the Contractor as shown.

#### VICINITY OF PIER 8

One and two story brick buildings interfering with the construction of Pier 8 will be removed by the city prior to beginning construction. Foundations are sandstone blocks about 18 inches thick. Basements and stacks are at one level about 8 feet below ground on the street side and open to the same level as the ground on the south side. Foundations and any other underground constructions connected with the buildings shall be removed by the contractor as "Item E-2, Unclassified Excavation". 4-inch and 8-inch gas lines crossing the location of Pier 85 will be removed by the owners when so notified by the contractor.

#### VICINITY OF EAST END PIER

No attempt will be made to salvage materials of an existing 12" sewer line crossing the location of the north footing. This sewer will be abendoned and a by-pass constructed as described elsewhere. No other utilities are known to interfere with pier construction.

#### 15. REMOVAL OF ABANDONED PIERS AND PEDESTALS OF FORMER CENTRAL VIADUCT

Seven masonry pedestals of the former Central Viaduct interfere with construction of piers 2N. 3N. 4N. 5N and 6N. They shall be removed to at least one foot below the surface of the ground. Payment therefor will be made as a lump sum, "Item S-24, Removing Existing Concrete Pedestals which Interfere with New Construction." Removal of that portion of the pedestals below a point one foot below the surface of the ground shall be included in the unit price bid for "Item E-2. Unclassified Excavation." for the respective pier footings. Two piers of the former Central Viaduct in the Cuyahoga River are partially within the limits of the established dock lines. Plans for these piers are shown on Sheet 9. All portions of the pier walls shall be removed down to Elevation 576.0 and all masonry, concrete, timber, steel and piling shall be removed riverward of the established docks lines to Elevation 540.5. Also, piles below this elevation shall be extracted except portions which break off in Payment for the removal of Structure No. I shall be "Item S+24. Removal of Existing Structure No. 1" and payment for the removal of Structure No. 2 shall be "Item S-24. Removal of Existing Structure No. 2."

#### cout. Prints are available, for reference, in cleveland. 16. REMOVAL OF EXISTING FENDERS

Steel pile fenders (Structures Nos. 3 and 4) are to be removed from the Cuyahoga River to Elev: 540:5: Construction plans for these fenders are not available. Payment for the removal of these fenders shall be the lump sum bid price for "Item S-24. Removal of Existing Structure No. 3." and "Item S-24. Removal of Existing Structure No. 4."

#### 17. BRIDGE DRAINAGE AND STORM SEWER SYSTEM

Roadway drainage will be conducted thru pipes and flumes to the tops of the piers by others. in a subsequent contract. The Contractor will place wrought iron pipes within the pier shafts extending to points below the ground surface where horizontal wrought iron pipes extend thru and I'-O" outside the pier shaft walls. Connection of these drainage pipes is made thru sewer pipe increasers to the storm sewer laterals. At the west end pier, a lateral from the SW End Pier Shaft connects to and the NW End Pier drainage empties through a short section of 8" sewer pipe into new manhole No. 13 near the north shaft. A new sewer extends and connects to existing manhole "A". At Pier I, laterals will be connected to an existing manhole "B". A 12" Y pipe special will connect both laterals to a single drop pipe. Manholes "A" and "B" are on an existing No. 7 brick sewer running approximately parallel to the bridge center line and emptying into the Cuyahoga River. On this sewer line, about Sta. 18+76. existing manhole "C" shall be removed to elev. 585.0 and the opening covered with a 10" thick concrete slab. Eastward to the Cuyahoga River, the existing 12" cast iron sewer line shall be replaced by a 36" reinforced concrete pipe and outfall structure "C". A new storm sewer nearly parallels the bridge center line from East bank of the Cuyahoga River to Pier 5. Laterals extend from each pier shaft to manholes Nos. 1, 2, 3 and 4 on the new sewer line near Piers 2, 3, 4 and 5 respectively.

Laterals from each shaft of Pier 8 connect into a new manhole No. 6 about Sta. 39+75, on a 15" sewer line from manhole No. 5 in Third Street, about Sta. 36+95. Laterals from the shafts of Pier 7 also connect to manhole No. 5. The existing 18" brick sewer is to be removed and detoured around Pier 7 North footing. Existing manhole "E" is to be abandoned. A new storm sever shall be built on Third Street, from manhole No. 5 Southeast to the Cuyahoga River. A lateral from the north shaft of Pier No. 6 runs to new manhole No. 12 into which the south shaff drainage empties through a short section of 8" sewer pipe. A new 12" sewer connects new manhale No. 12 to new manhale No. 8 in Harrison Street, (about Sta. 35+00). A new 12" sewer shall be built connecting manhole No. 8 with manhole No. 9 on the new Third Street sewer line.

On Third Street, at the north side of Stones Levee, manhole No. 16 shall be built on the new Third Street sewer line, and connection made to the existing catch basin at the N. E. corner of the street intersection, using the existing material. See Sheet 36.

At the east end pier, laterals from the pier shafts connect into new manhole No. 7 at Sta. 43+00. A 12" sewer shall be built from manhole No. 7 to the existing manhole "D" on an existing No. 4 sewer in Commercial Road.

The Contractor shall build manholes No. 14 and No. 15 with the connecting sewer lines, near the east end Pier, to reroute an existing 12 inch sewer around the location of the north pier footing. See Sheet 36.

All wrought iron drainage pipes inside the piers, with couplings and specials, shall be standard weight and conform to Section M-6.10, "Welded Wrought Iron Pipe." ASTM designation A72. Joints may be threaded, welded, or have bolted flanges, or have any combination thereof.

The proposed elevations and locations of catch basins, manholes, and sewer pipes, and the estimated lengths of pipes may be adjusted by the Engineer during construction, as per Section

Payment for the above drainage and storm sewer system will be made as follows: For the wrought iron pipes from the top of pier shafts to the connection to sewer laterals below ground, a unit price per linear foot for "Item S-29, 8" Wrought Iron Pipe, Including Specials." For the laterals and pipes of the drainage system from the pier shafts to the manholes or outlet structures at the Cuyahoga River, a unit price per linear foot for "Item I-2, (size) inch pipe for Storm Sewers", (with a separate bid price for each size listed); "Item I-2 (size) inch Pipe for Storm Sewers under Pavement"; "Item I-2, (size) inch Extra Strength Reinforced Concrete Culvert Pipe, Sec. M-6.6(c) for Storm Sewers"; "Item I-2 (size) inch Paved Invert Corrugated Metal Pipe, Sec. M-6.4(d) for Storm Sewers; "Item I-8 Each, Standard No. I Manholes"; Lump Sum , Alteration to Manhole "A", "B", "D", or "F"; Lump sum, "Outlet Structure "A". "B". or "C": "Item I-5 Pipe Specials". (description). The specials shall conform to the same strength class as the adjoining sewer. For payment purposes, each special shall be considered as having a length of 3 feet.

#### 18. EXISTING PIPE AND UTILITIES

The location, size and depth of all existing pipe and utility appurtenances represent the best information obtainable at the time of survey, but the State of Onio does not quarantee the correctness thereof.

Concrete shall be Class "E".

At: least 15 days before concrete form construction is begun, the contractor shall submit to the Engineer for approval by the Director, a plan showing where he proposes to place construction joints and showing the extent and sequence of individual pours. The concrete shall be placed in one continuous operation between the construction joints that have been proposed and approved. Construction joints shall be so located and arranged as to least impair the strength and appearance of the concrete, and to reduce shrinkage stresses to a minimum.

The concrete in shoe seat areas shall be finished 1/8 inch to 1/4 inch high and ground down to the elevations shown.

# 20. BAR CLEARANCES

The clearance between reinforcing bars and the surface of the concrete shall be 3 inches for the footing bars and 2 inches for the horizontal bars in the pier shafts.

#### 21. REINFORCING BAR SIZE

The first digit in the bar mark if there are three digits, and the first"two if there are four, indicates the bar size number.

#### 22. MISCELLANEOUS METAL

Anchor bolts, nuts, washers, anchor bolt frames, doors, door frames, hand hold pipes in door openings and all fasteners for wrought iron pipes within the pier shafts, shall be structural carbon steel. ASTMA-7. Payment will be made by the pound on the computed weight in pounds as bid for "Item S-7, Structural Steel".

The ladder rungs shall be wrought iron and will be paid for at the price per pound bid for "Item S-7. Wrought Iron Ladder Runas".

All welding shall be class "A". - See section 5-7.22.

Dimensions given are measured horizontally and at 60° F.

# 25. DATUM PLANE FOR ELEVATIONS (See I.O.C. 11/26/54 H.R. Craig)

All elevations pertaining to the dock walls are shown in feet above mean tide at New York. All other elevations are regional geodetic survey datum. Elevation 570.50 above mean tide at New York City equals elevation 570.07 Cleveland regional geodetic survey datum.

## 26. MAINTAINING AND SAFEGUARDING TRAFFIC

The contractor shall provide for the maintaining and safeguarding of traffic on all of the streets and drives immediately beyond the ends of this project and within the limits of this project, that are affected by his operations, in accordance with the provisions of Sec. 6-7.07 and Sec. G-4.05. Payment therefor will be made in the lump sum price bid for "Maintaining and safeguarding traffic, including lights, signs, barricades and watchmen".

## 27. ELECTRICAL GROUNDS

A solid No. O bare copper wire electrical ground shall be embedded in the concrete of all pier shafts. The wire shall be brazed to a concrete pile casing or a steel H pile at its lower end, and its upper end shall extend sufficiently above the top of the concrete to provide for a suitable splice and extension for connection, by the contractor for the superstructure. Payment therefor will be made at the lump sum price bid for "Item S-25, Electrical Grounds."

#### 28. COFFERDAMS, CRIBS AND SHEETING

FEDERAL AID PROJECT NO. FED. ROAD STATE OHIO UI 1057 (4)

#### CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY

Plans for sheeting and bracing to be used in cofferdams adjacent to railroad tracks and in trenches for sewers placed under operated tracks shall be submitted to the Director of Highways for approval by the Department of Highways and by the Railroad Company. The contractor must obtain such approval before work is begun.

CUY-42R-17.50 CENTRAL VIADUCT

Cofferdams, cribs and sheeting shall be paid for per unit of cofferdam per pier shaft, with all work to be done according to Item E-Z. Any cofferdams, cribs and sheeting associated with the construction reconstruction and removal of parts of the sewer system, and the removal of existing structures, shall be considered as paid for in the prices bid for such construction and removal.

#### 29. SHEET PILE DOCKWALL

The proposed 200 foot dockwall section in the vicinity of Pier I requires that structure #1 be removed before construction can be completed. The proposed dockwall shall consist of a front wall and anchor piles connected with tie rods. The front wall is located with the face of the timber fenders at the established dock line.

The existing 3 inch high pressure gas line will be raised or lowered as required by the utility company.

The cost of any excavation, sheeting and bracing incidental to the installation of the dockwall items shall be included in the price bid for the respective items.

The sheet piling shall be U. S. Steel section MZ=38 or Bethlehem section ZP=38 or approved equivalent. Fabricated connections shall be of size and strength to correspond with the rolled members. The fabricated members may be built up by either welding or riveting. Steel for sheet piling shall be in accordance with Sec. M-7.4(c).

The driving of a sheet pile, if directed by the Engineer, shall be stopped before the top of the pile reaches the required elevation, to permit cutting off of metal that is deformed due to driving. Such cutting shall be neatly done to a straight line. Defective piles shall be removed and replaced. A pile shall be considered defective if injured to an extent that would reduce the strength of its section more than 20 percent.

The penetration of the sheet piles shall be such as to reach the elevations shown unless obstructions are encountered. In case obstructions, such as boulders or large stones. prevent the penetration of a sheet pile at least to Elev. 537.0, such obstructions shall be removed.

The vertical steel H anchor piles shall be 12 BP 53 except where otherwise shown on the plans and the battered pile 14 BP 73. The vertical piles shall be driven to a capacity of 40 tons and the battered piles to a capacity of 60 tons. The pile driving shall be governed by Item S-18.

The sheet piling will be paid for at the contract unit price per pound bid. The number of pounds paid for shall be the actual weight of piling in place and accepted, plus an allowance for cut-off. In determining the weight to be paid for, the length of each sheet pile (and special section) shall be considered the length below the specified top of sheeting plus the length of cut-off but not to exceed 6 inches of cut-off. Payment for the quantity determined as described above shall constitute full compensation for furnishing, fabricating, driving, cutting-off and connecting all steel sheet piling and special sections required, and for removal of obstructions.

The steel H Piling shall be paid for at the contract unit price per pound bid. The number of pounds paid for shall be the actual weight of the number of feet of piling in place plus the length of cut-off but not to exceed 2 feet of cut-off per pile.

Class "E" concrete shall be paid for at the contract unit price bid per cubic yard for Item "S-I, Class "E" concrete, anchor caps."

Payment for reinforcing steel will be made per contract unit price bid per pound, for Item "S-4, Reinforcing Steel in Anchor Caps.

Payment will be made for dockwall at the contract unit price bid per pound for Item \*S-7 and Special, Steel Sheet Piling, Steel H Anchor Piles and Steel Wales, for dockwall. Payment shall be made for anchor rods, turnbuckles, etc., at the contract unit price bid

per pound for Item "S-7 and Special, Steel Anchor Rods, Turnbuckles, Pipe Sleeves and fastenings for dockwall (including payment for necessary excavation, sheeting and bracing). " Payment shall be made for the timber fenders for the dockwall at the contract unit price bid per MBM for Item "S-13, Creosoted Timber Fenders for Dockwall including hardware."

#### 30. ERIE RAILROAD TRACK WORK

The Erie Railroad Company shall furnish and place ballast and accomplish all track work upon the completed subgrades constructed by the contractor.

The several phases of work by the contractor and the railroad company will require close cooperation and coordination. The contractor shall notify the railroad company sufficiently in advance of all track moves so that traffic and work schedule interruptions will be held to a minimum.

The contract unit price bid for Item "Special Temporary Timber Crib Wall" per square foot shall be complete compensation for furnishing, installing and maintaining a temporary cribwall and embankment to the elevations and grades shown on the plans for the period of time necessary and the subsequent removal thereof upon completion of the construction phase of which they are a part. Any track ballast remaining after any track shift and not reclaimed by the railroad shall be considered part of the temporary fill and removed from the site or deposited in permanent fill areas by the contractor. The basis of measurement shall be the number of square feet of surface on the face of the cribwall. The height shall be measured along the battered face of the wall. Any excavation and subsequent backfilling necessary in the course of the track shifts shall be considered as incidental to the performance of this pay item and the contract unit price bid shall include payment therefor.

## REVISIONS announced Oct. 6, 1954, made Dec 6, 1954 PART 2

31. PILING (Continued) It will be the Contractor's responsibility to provide a

> shell or casing, for the cast-in-place reinforced concrete piles, of adequate wall thickness, but this thickness shall be not less than No. 7 gauge if the casings are driven without a mandrel.

No "Item S-16, First Test Pile" is provided in the quantities. The first test pile of each type. together with all labor, material, equipment and incidentals therefor, will be paid for per linear foot under the pertinent "S-18" item or per pound under the pertinent "S-7 and Special" item. Continued on Sheet 2.

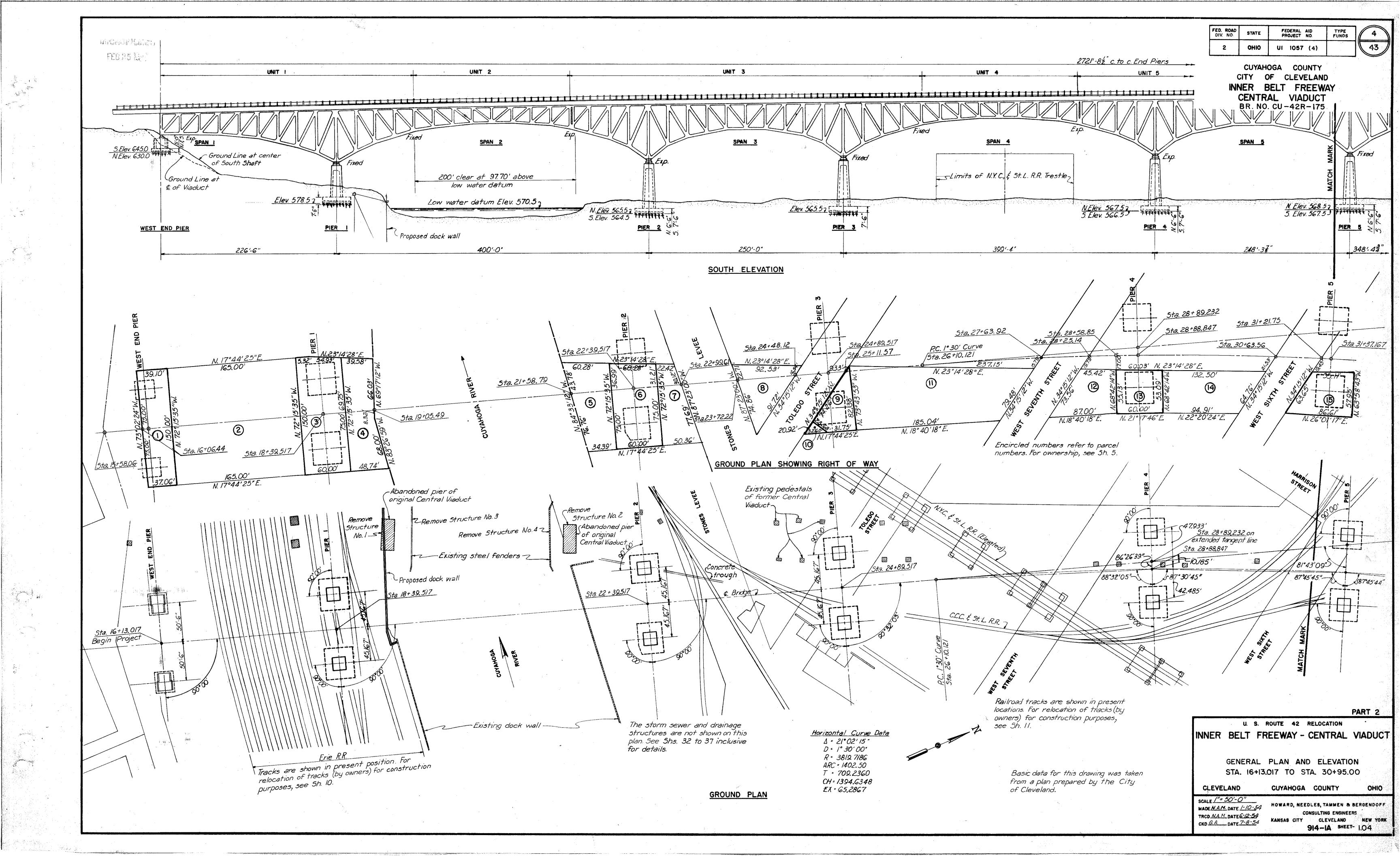
U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

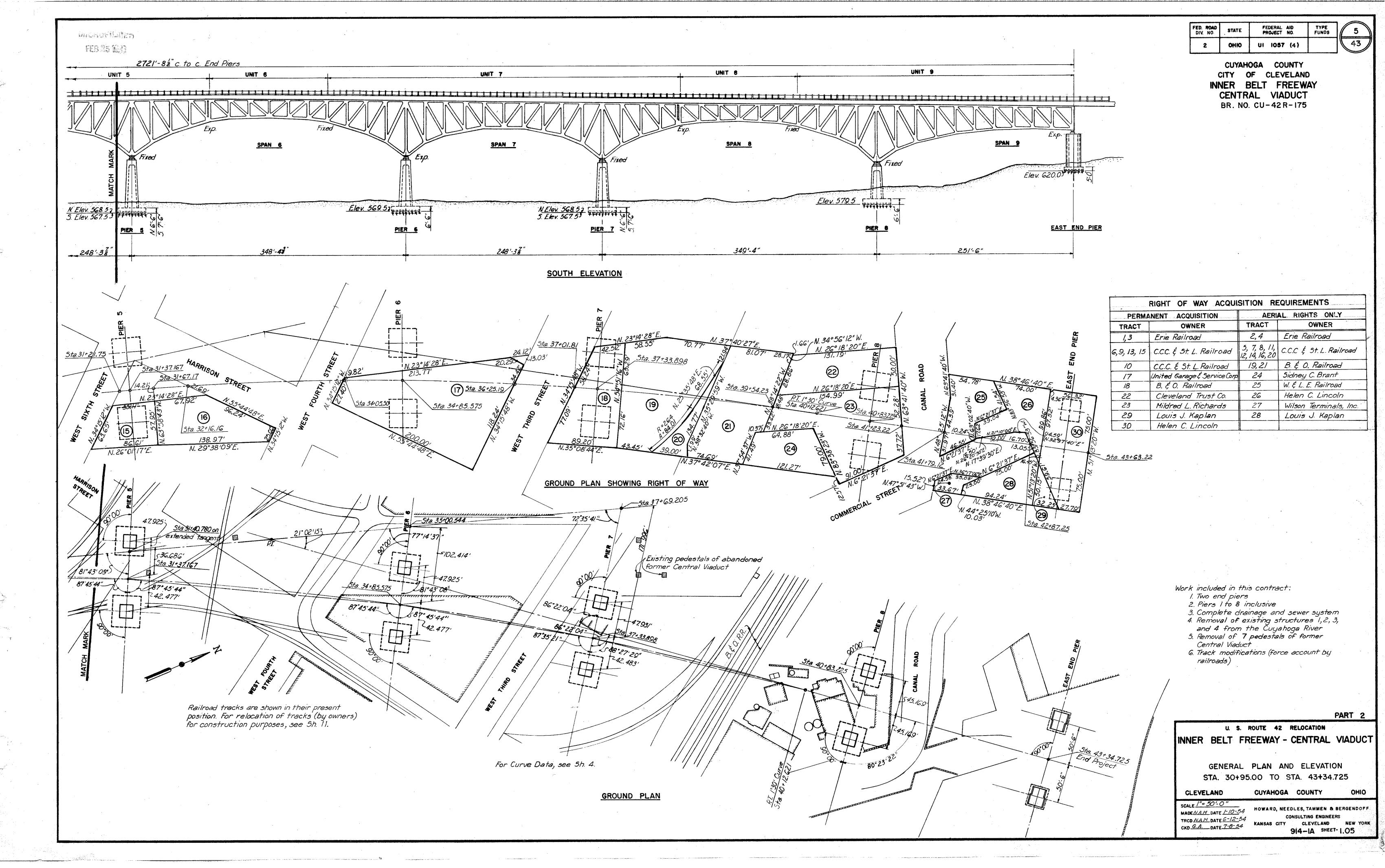
GENERAL NOTES

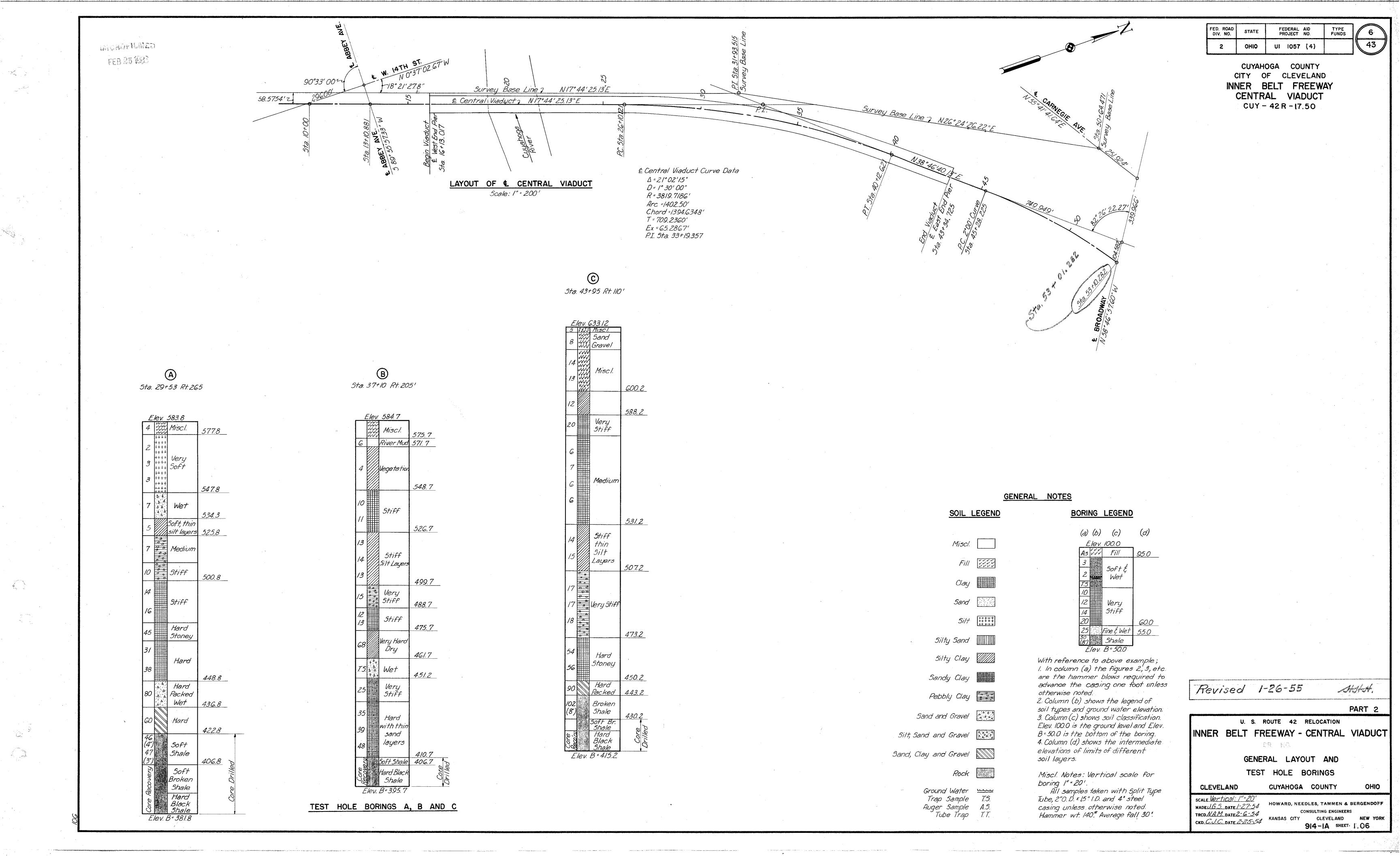
CUYAHOGA COUNTY CLEVELAND MADE G.A. DATE 6-28-54

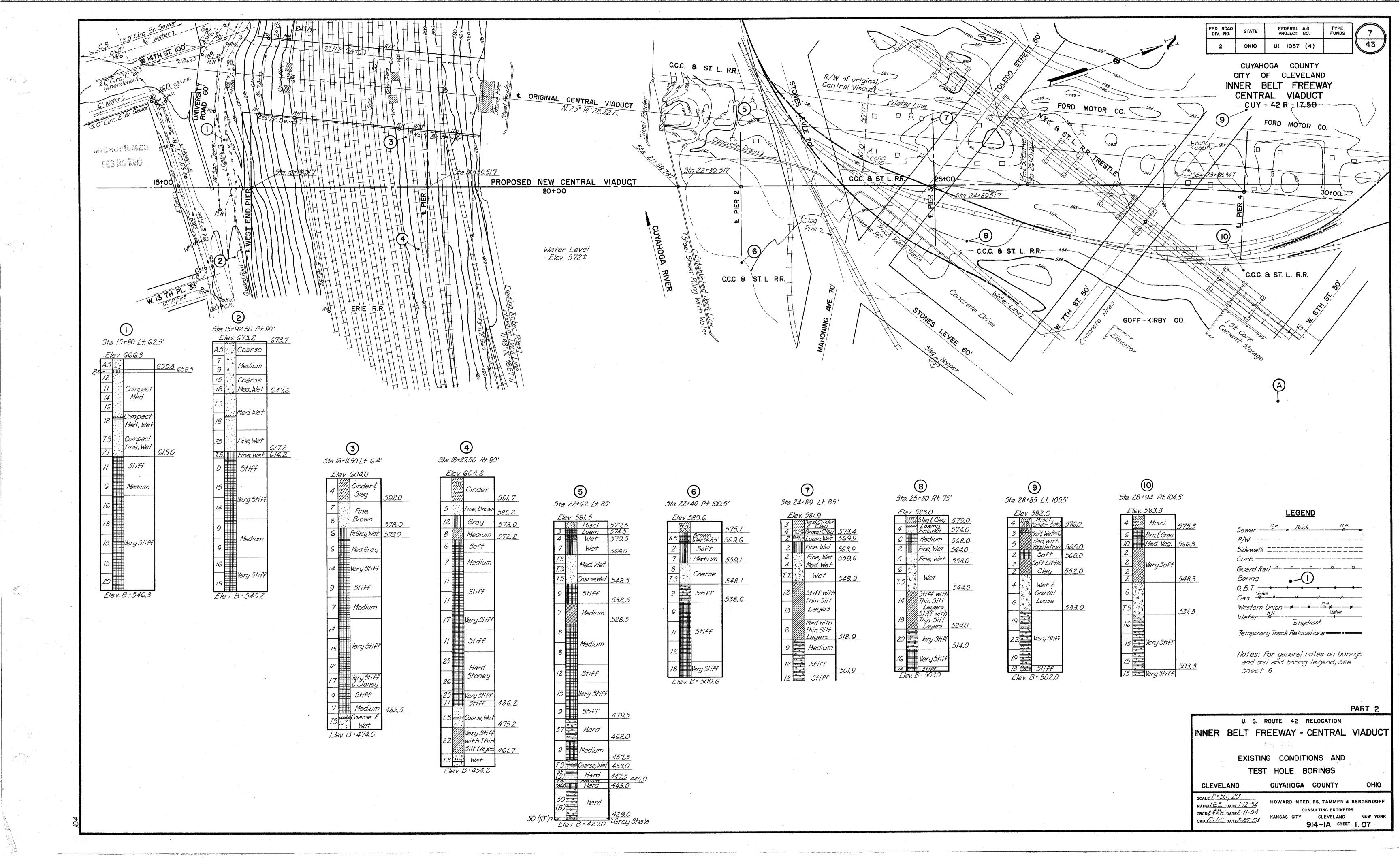
HOWARD, NEEDLES, TAMMEN & BERGENDOFF CONSULTING ENGINEERS TRCDJB. DATE 7-2-54 KANSAS CITY CLEVELAND NEW YORK CKD. C.J.C. DATE 7-8-54

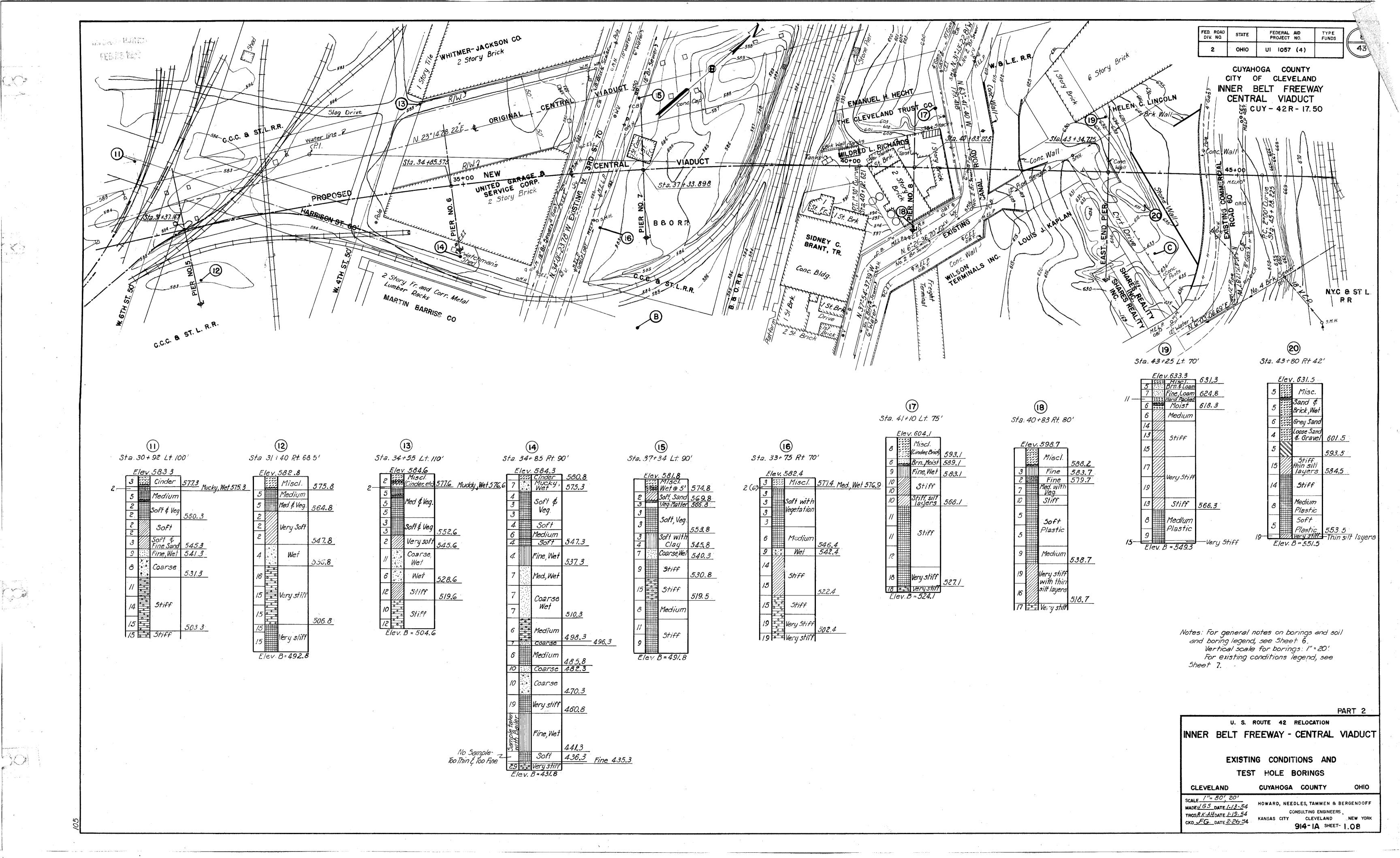
914-1A SHEET- 1.03 REV 9-24-54

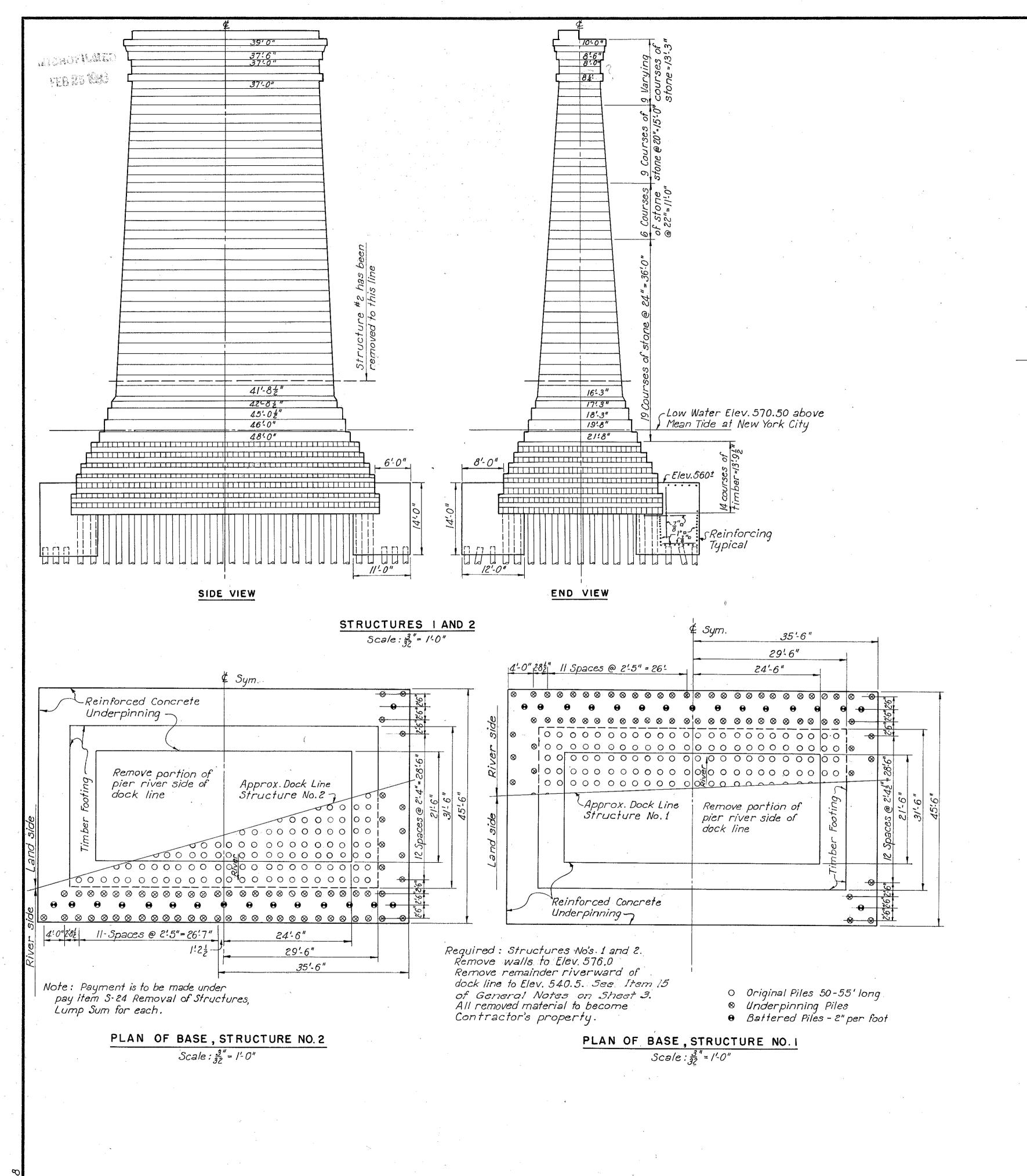


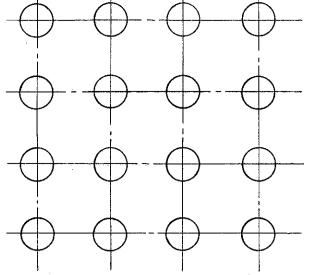


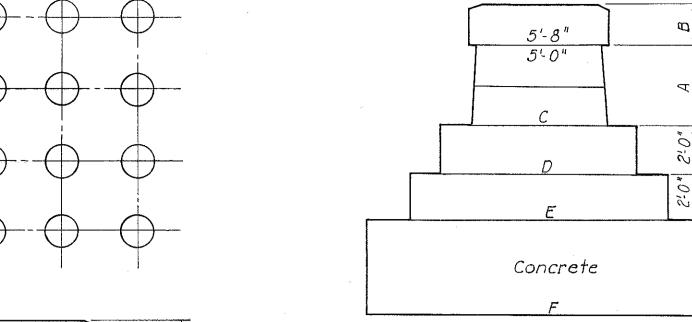


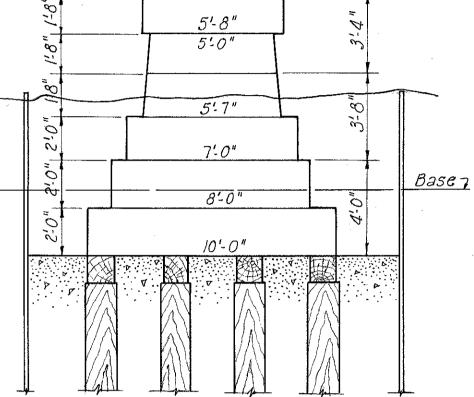












TAB	LE OF	PED	ESTA	L DIM	ENSIC	NS
Pier	А	В	С	D	E	F
3	31-0"	/'- 6"	5'-6"	7-0"	9'-0"	1/20"
4	310"	1-6"	5'-6"	7:0"	9'-0"	11-0"
5	3'-4"	1'-8"	5'-6 3'	7-6"	10:0"	13:0"
J	340"	1-6"	5'-6"	7-0"	9'-0"	11-0"
6	3!4"	1'-8"	5-6 3	8:0"	10-6"	/4'.0"

#### PEDESTALS AT PIER 2

#### PEDESTALS AT PIERS 3, 4,5 AND 6

Existing pedestals of the old Central Viaduct substructure which interfere with new construction shall be removed as necessary to avoid interference with new construction, including pile driving. Payment for pedestal removal to at least one foot below the surface of the ground shall be made by Item S-24, "Removing existing concrete pedestals which interfere with new construction" That portion of the pedestals beneath one foot below the ground shall be removed by the contractor, payment therefor being included in the bid price per cubic yard under pay item E-2, unclassified excavation.

FEDERAL AID PROJECT NO. TYPE FUNDS 43 OHIO UI 1057 (4)

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT CUY - 42 R - 17.50

PART 2

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

> EXISTING PIERS AND PEDESTALS TO BE REMOVED

CLEVELAND

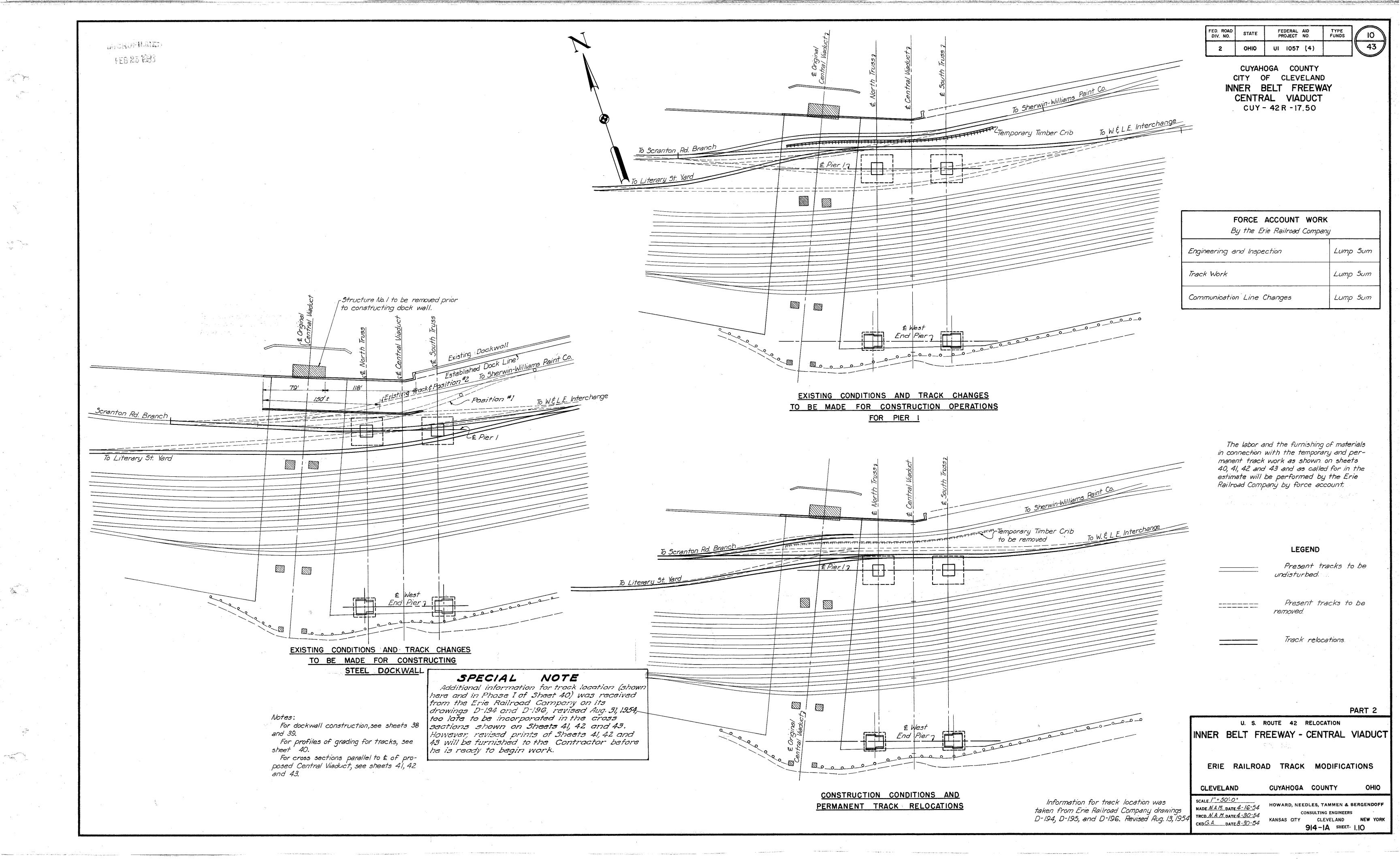
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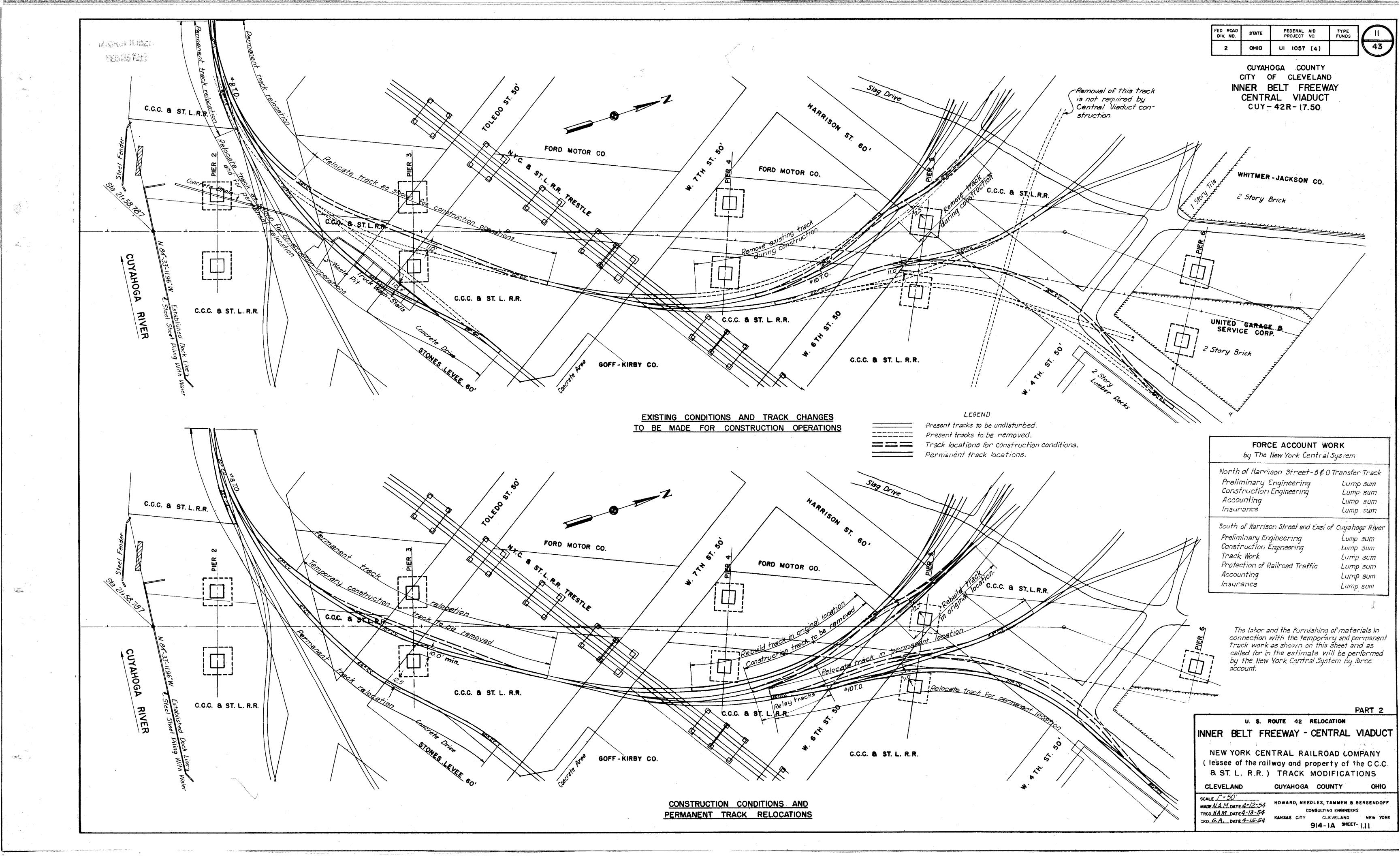
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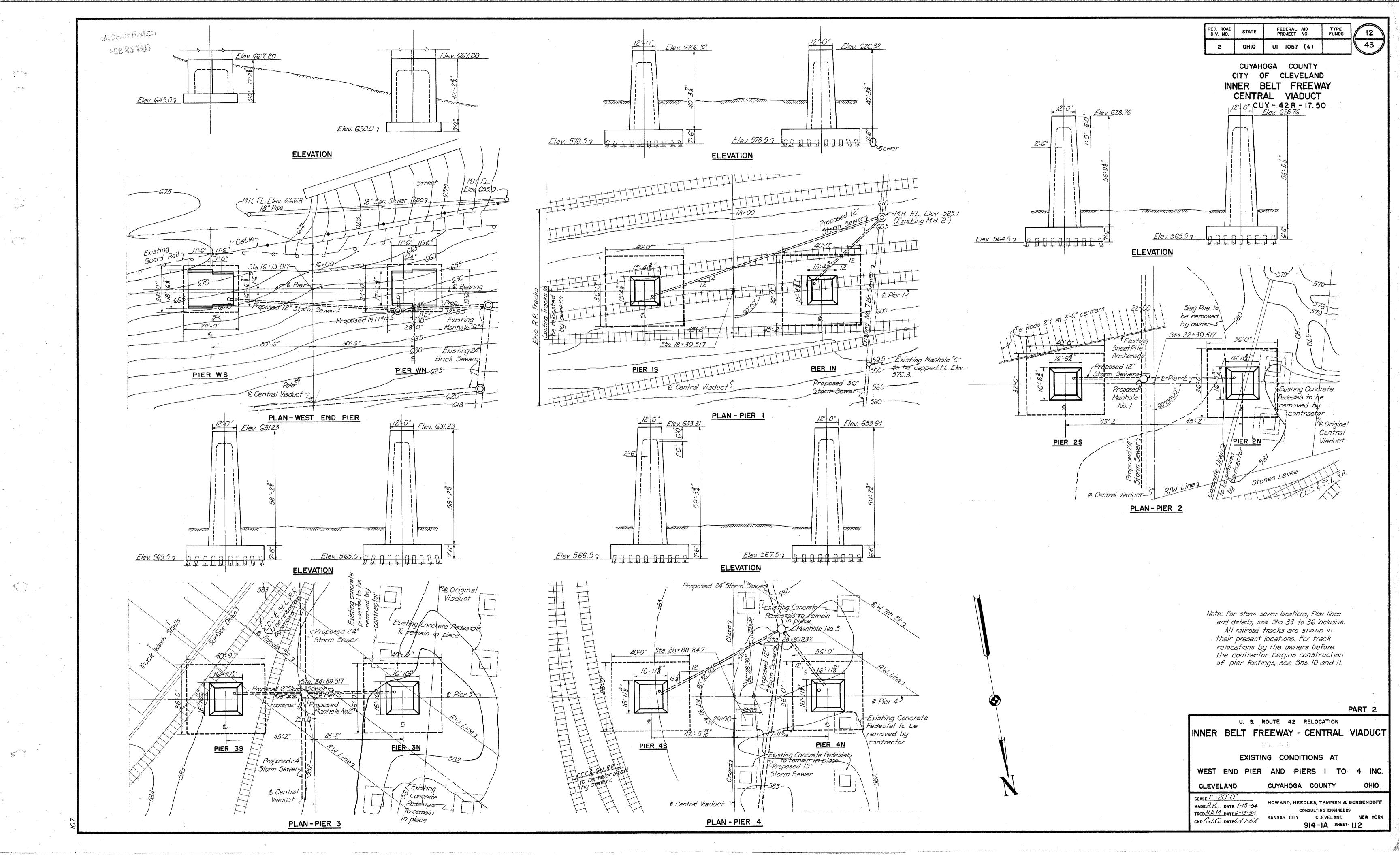
CUYAHOGA COUNTY SCALE AS Shown HOWARD, NEEDLES, TAMMEN & BERGENDOF!

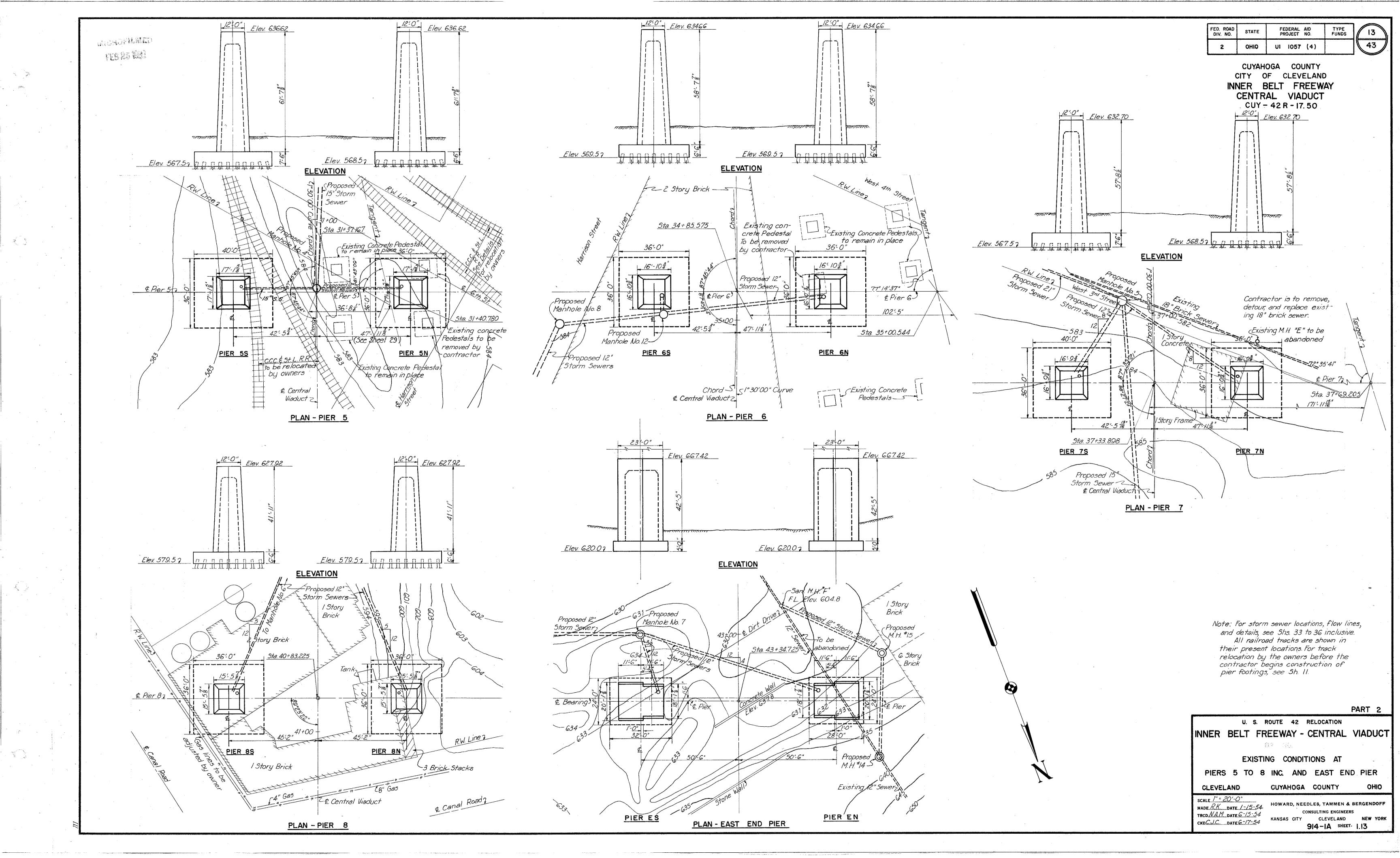
CLEVELAND NEW YORK

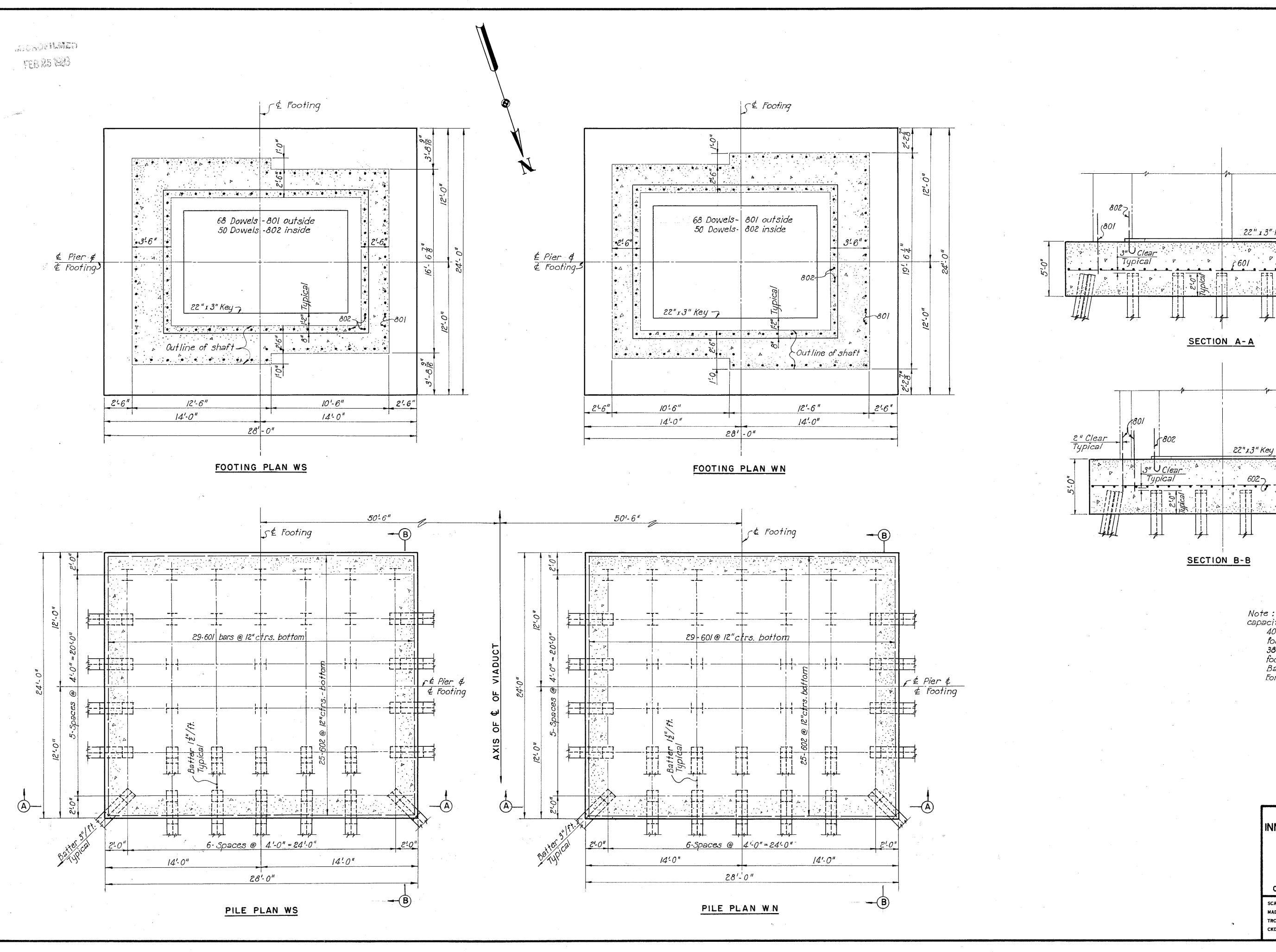
914-1A SHEET- 1.09





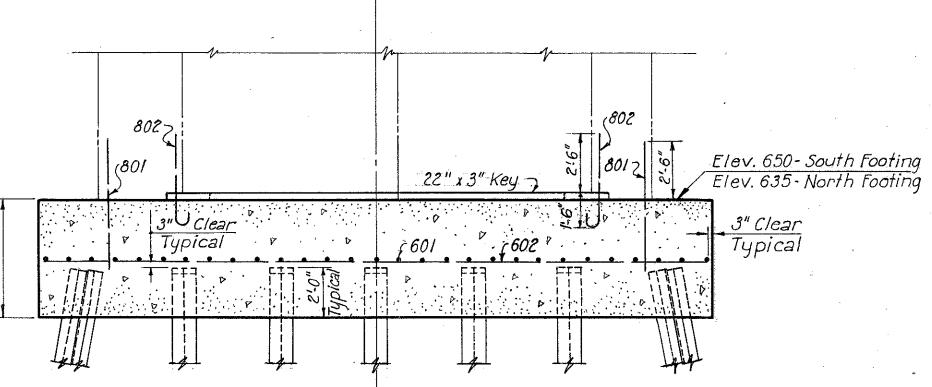


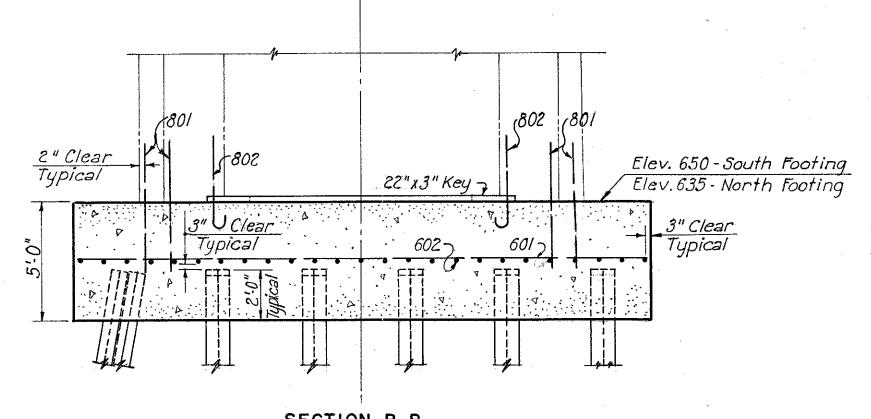




FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. TYPE FUNDS 43 UI 1057 (4)

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT CUY - 42 R - 17.50





Note: 12" BP 53 steel piles with a nominal design capacity of 65 tons each.

40 piles, estimated length 60 feet each, for footing W N.

38 piles, estimated length 60 feet each, for footing W S.

Batter 3" per foot and 1½" per foot as shown.

For reinforcing schedule, see Sheet 32.

PART 2

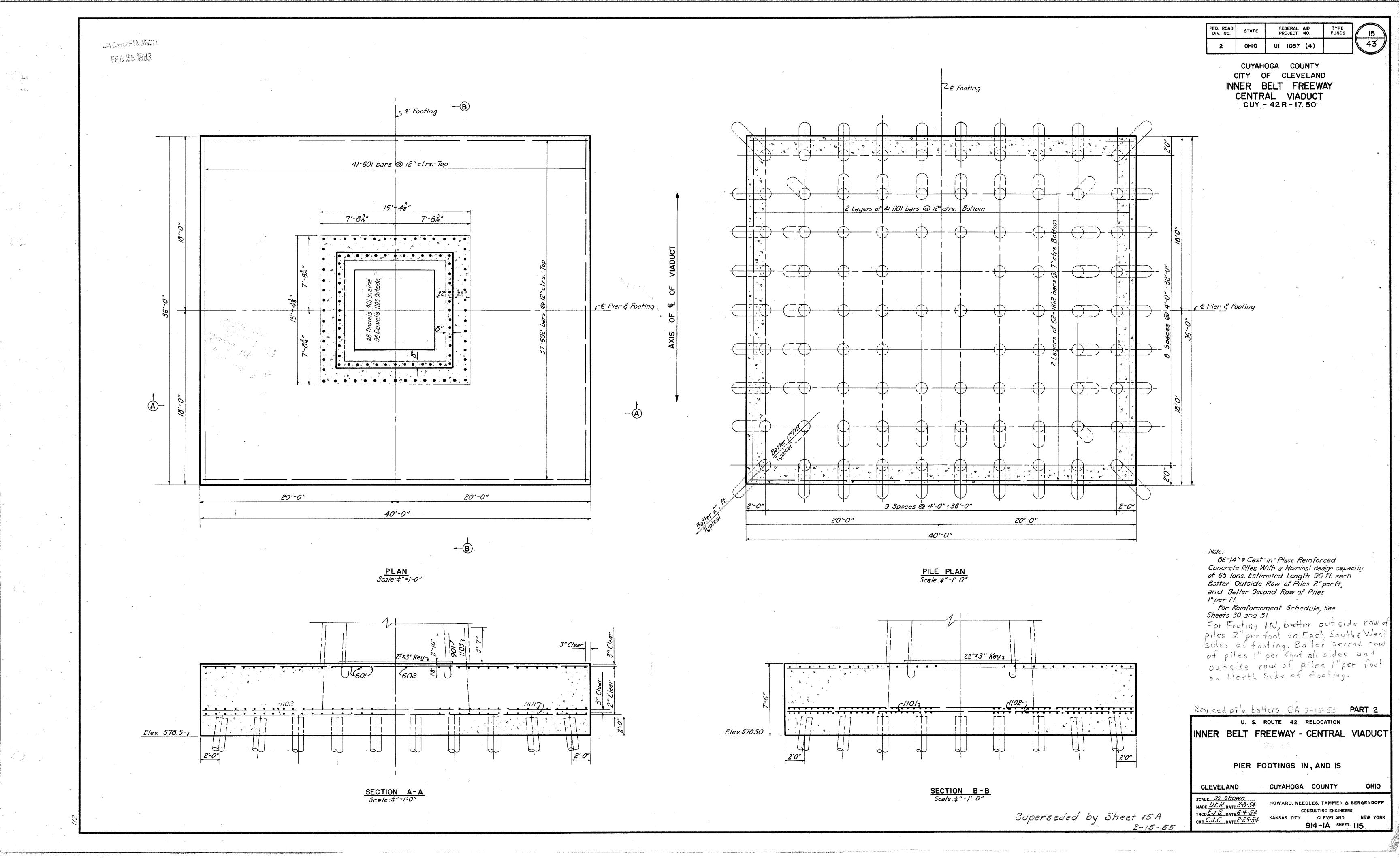
U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

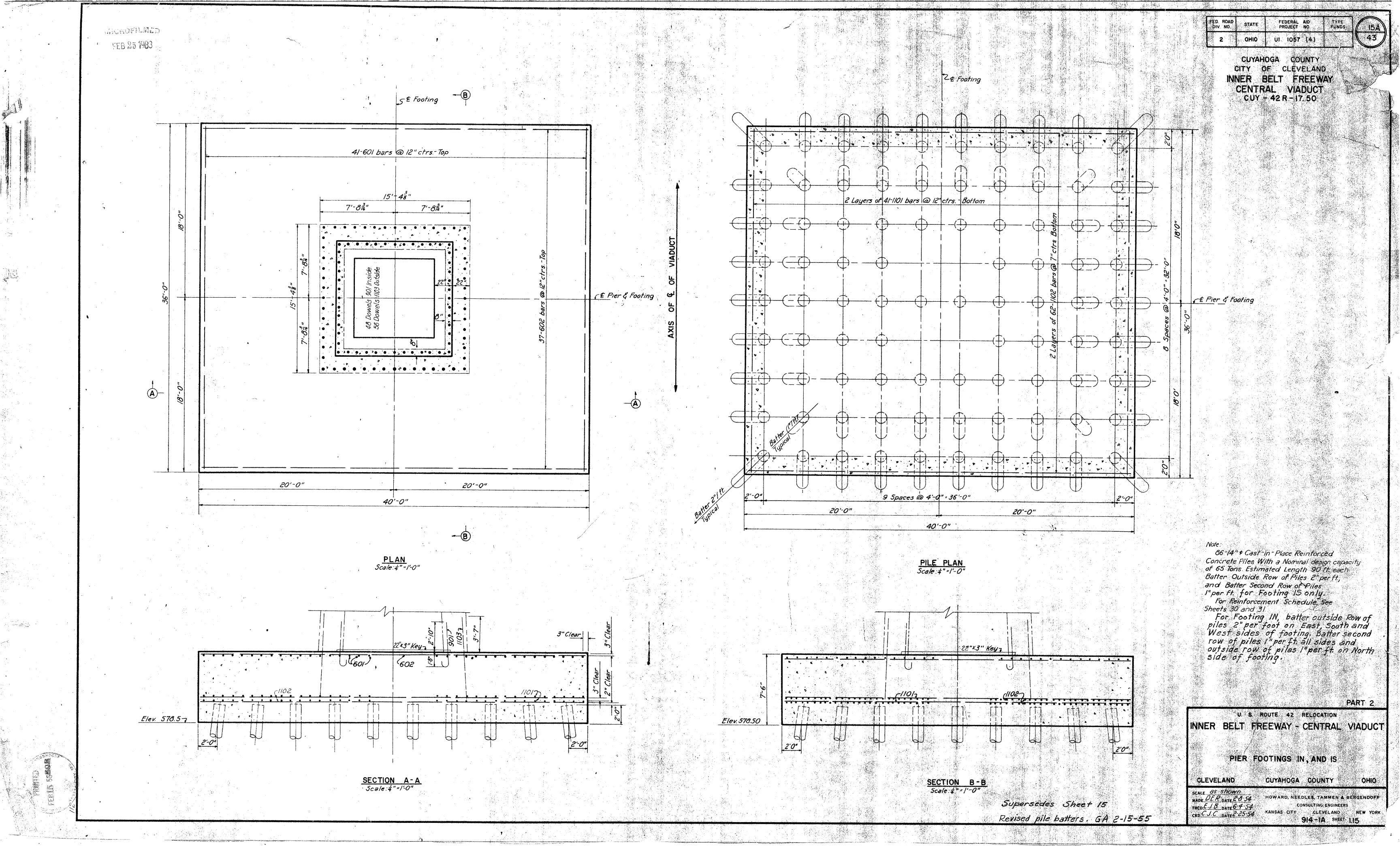
WEST END PIER FOOTINGS, WN AND WS

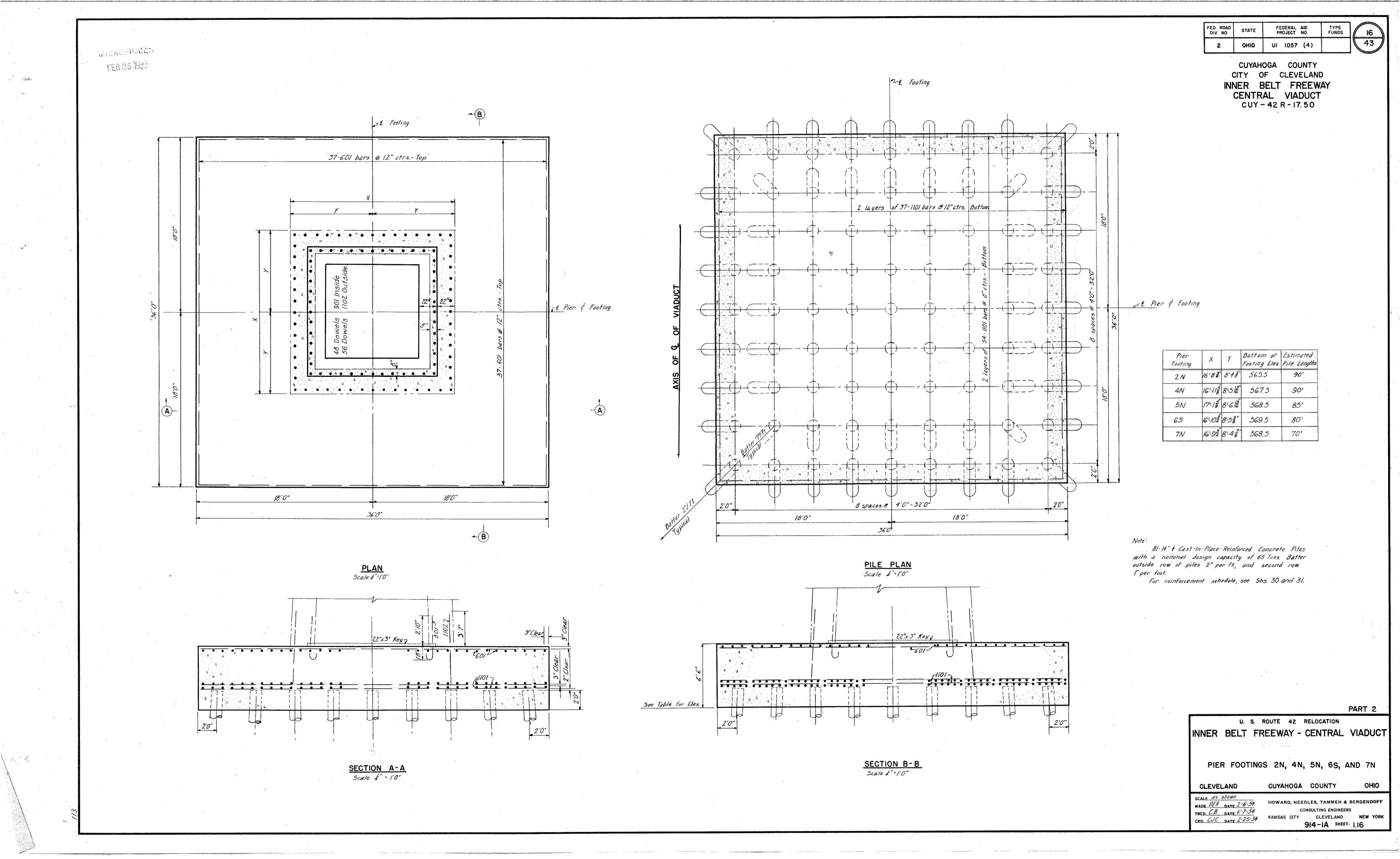
CLEVELAND CUYAHOGA COUNTY SCALE 4"= 1'-0"

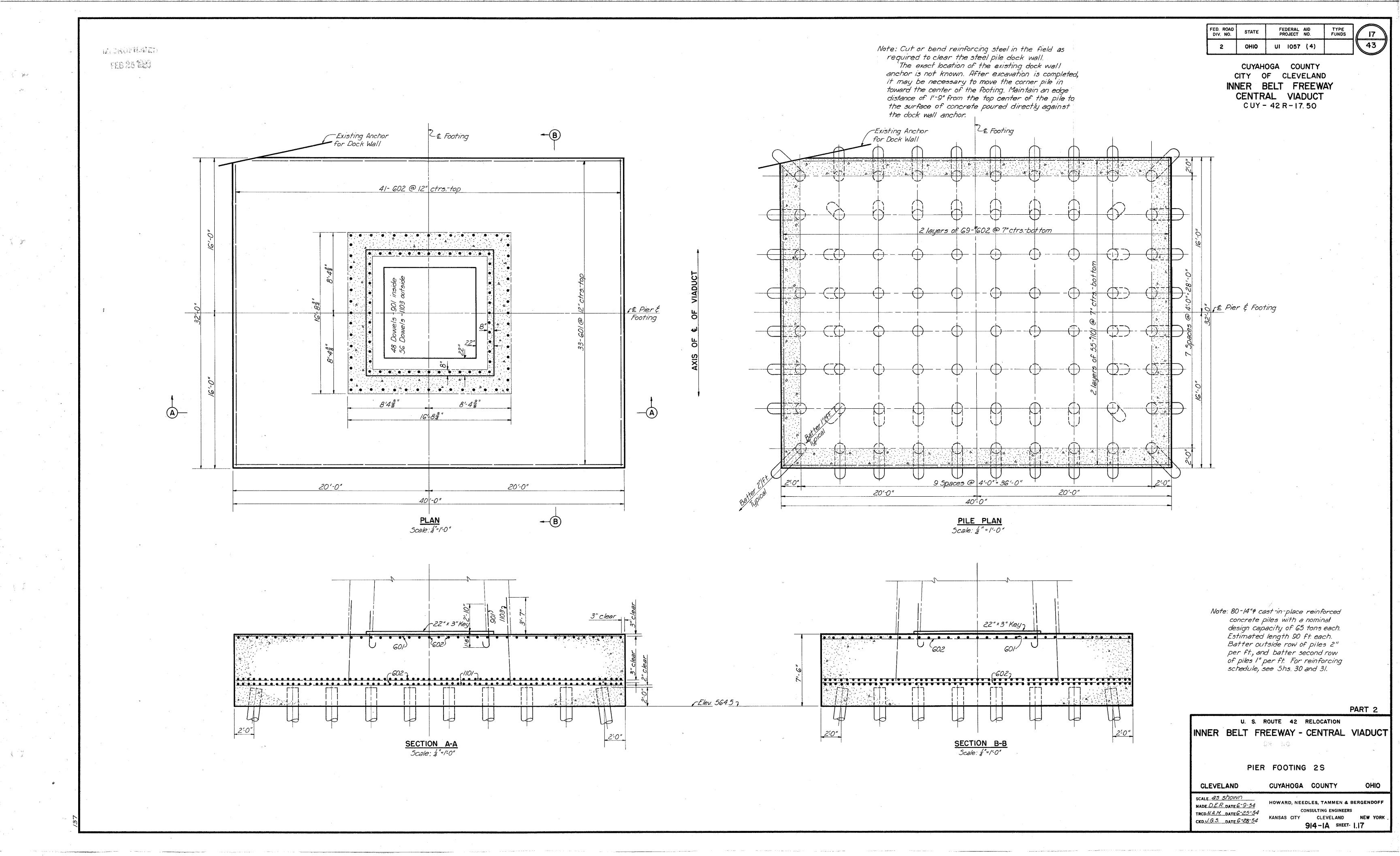
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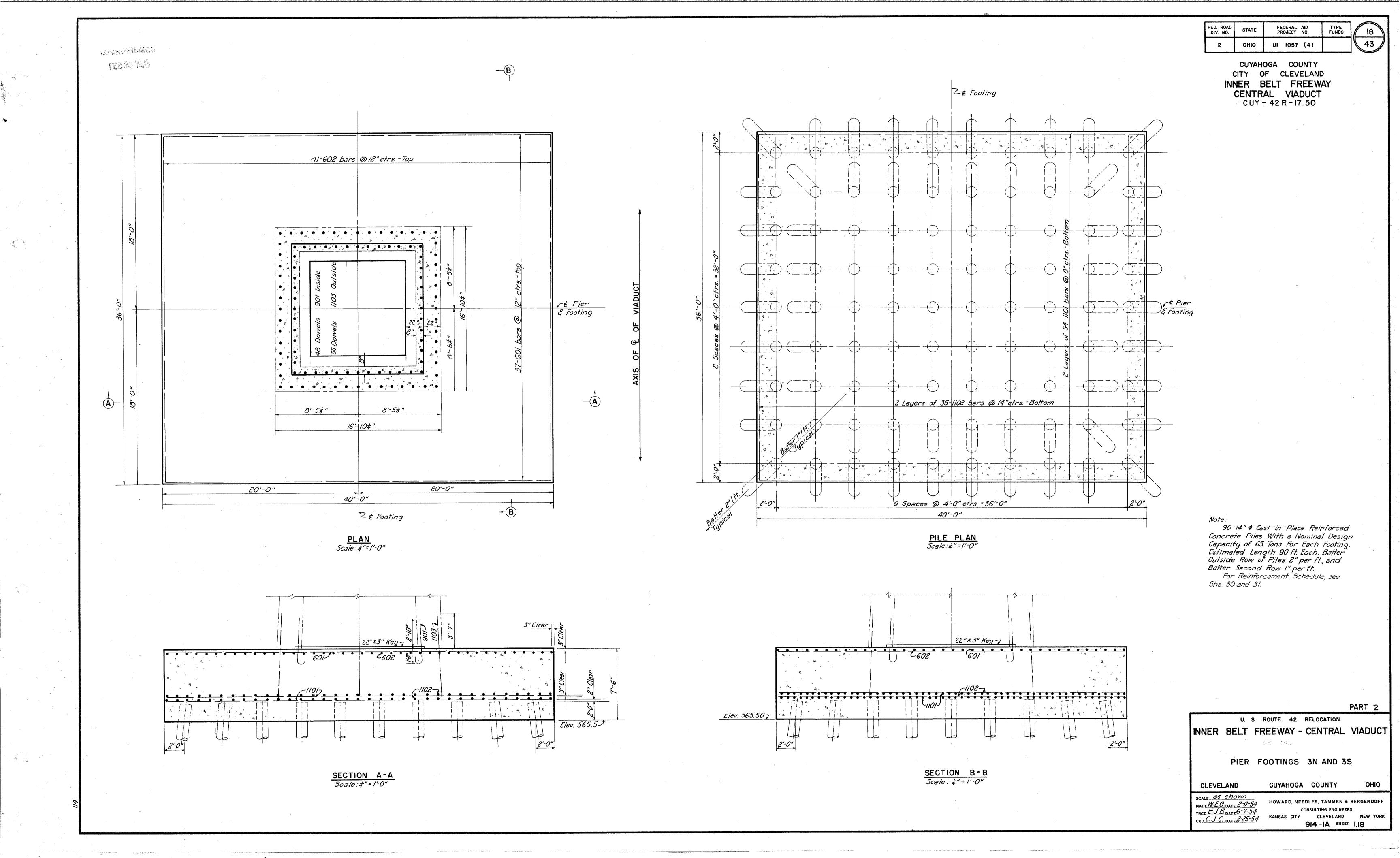
HOWARD, NEEDLES, TAMMEN & BERGENDOF CLEVELAND NEW YORK 914-1A SHEET- 1.14

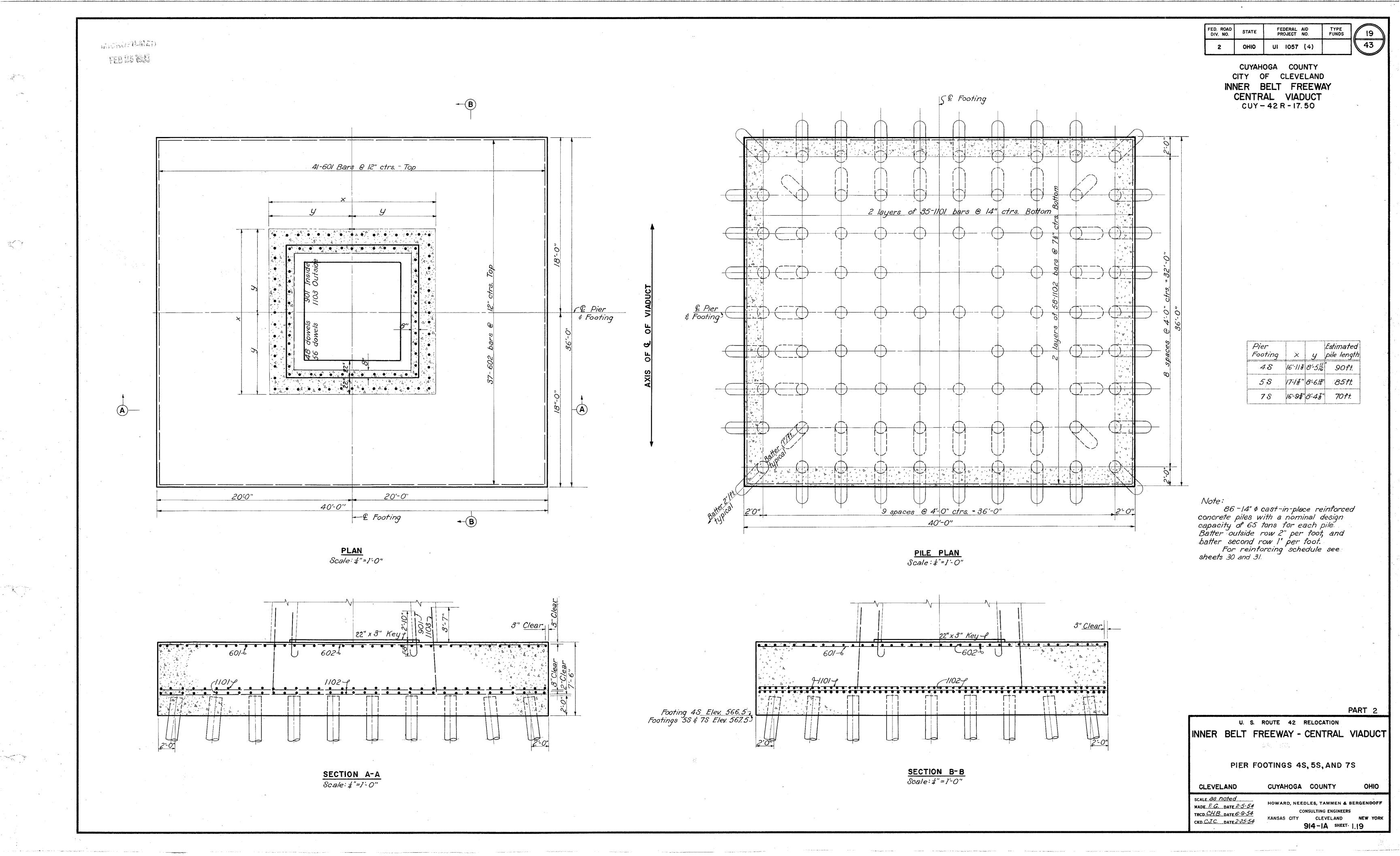


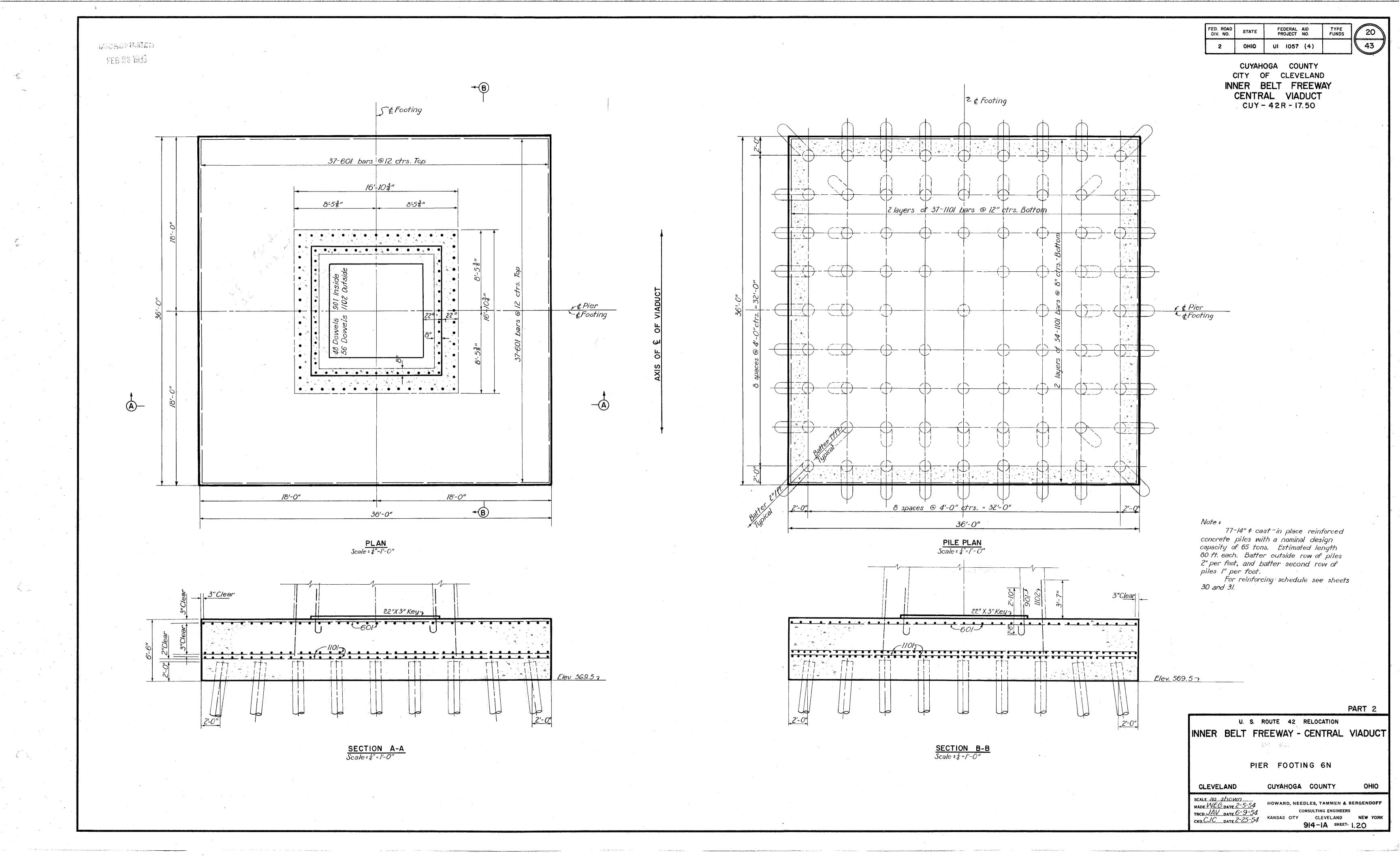


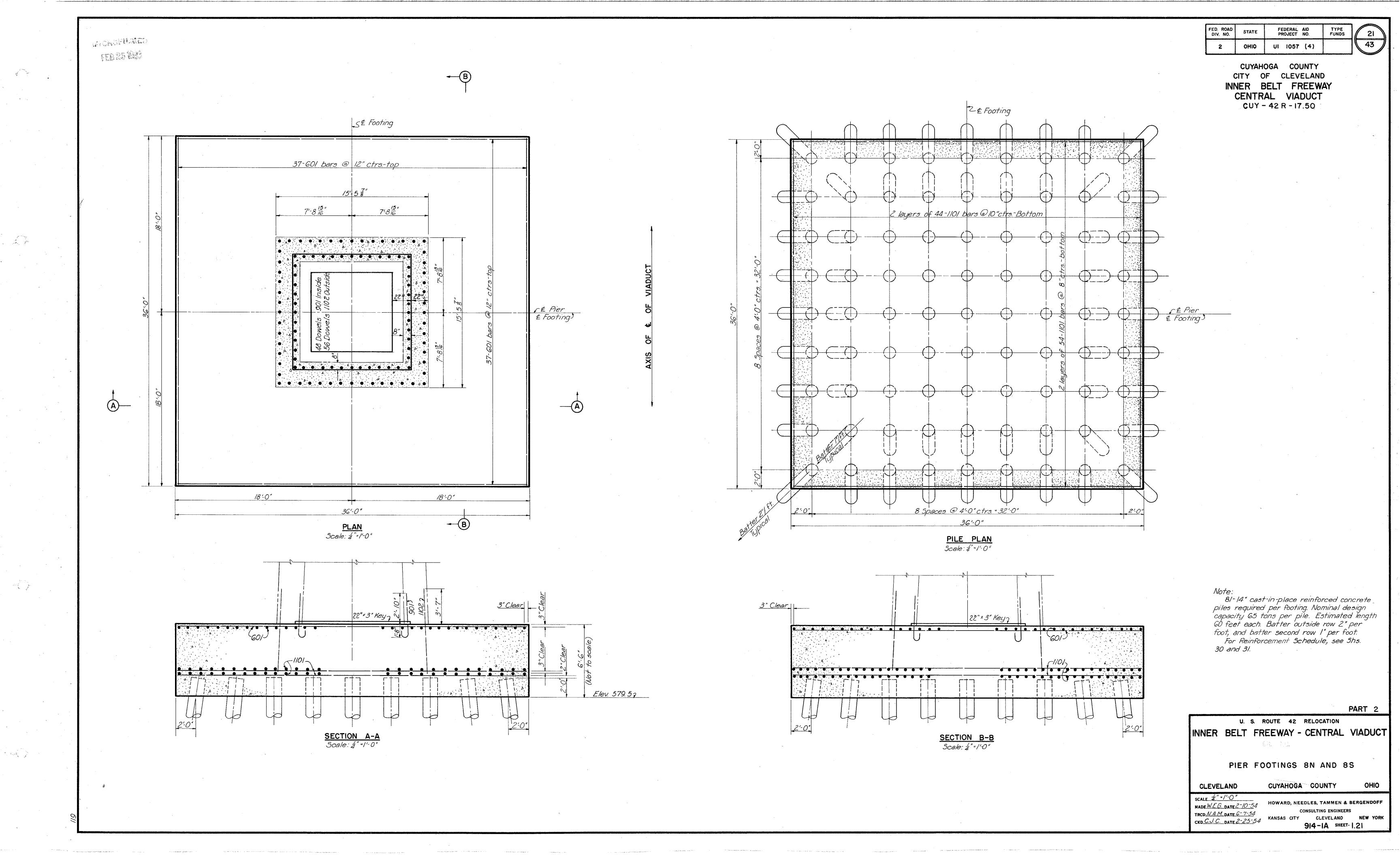


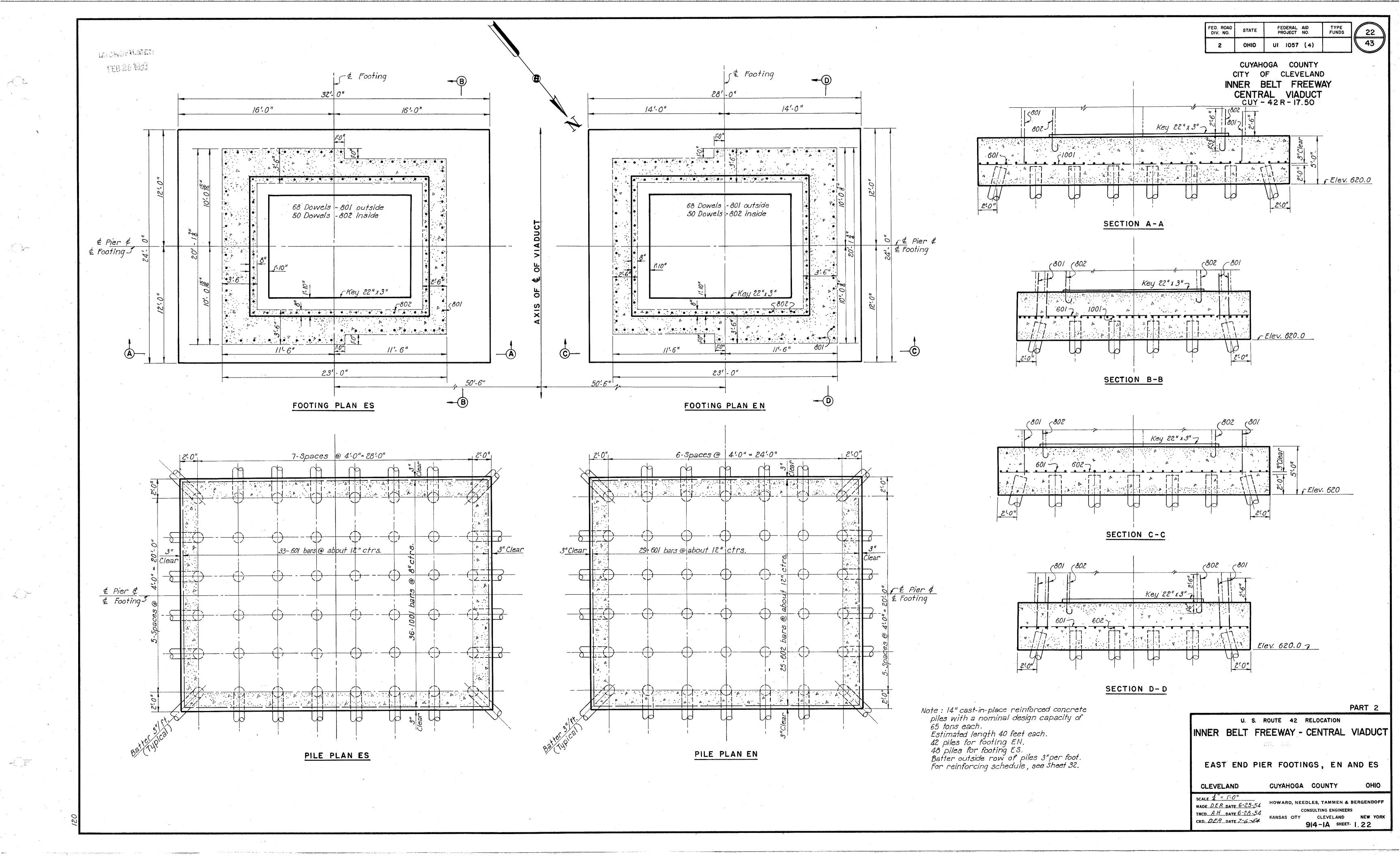


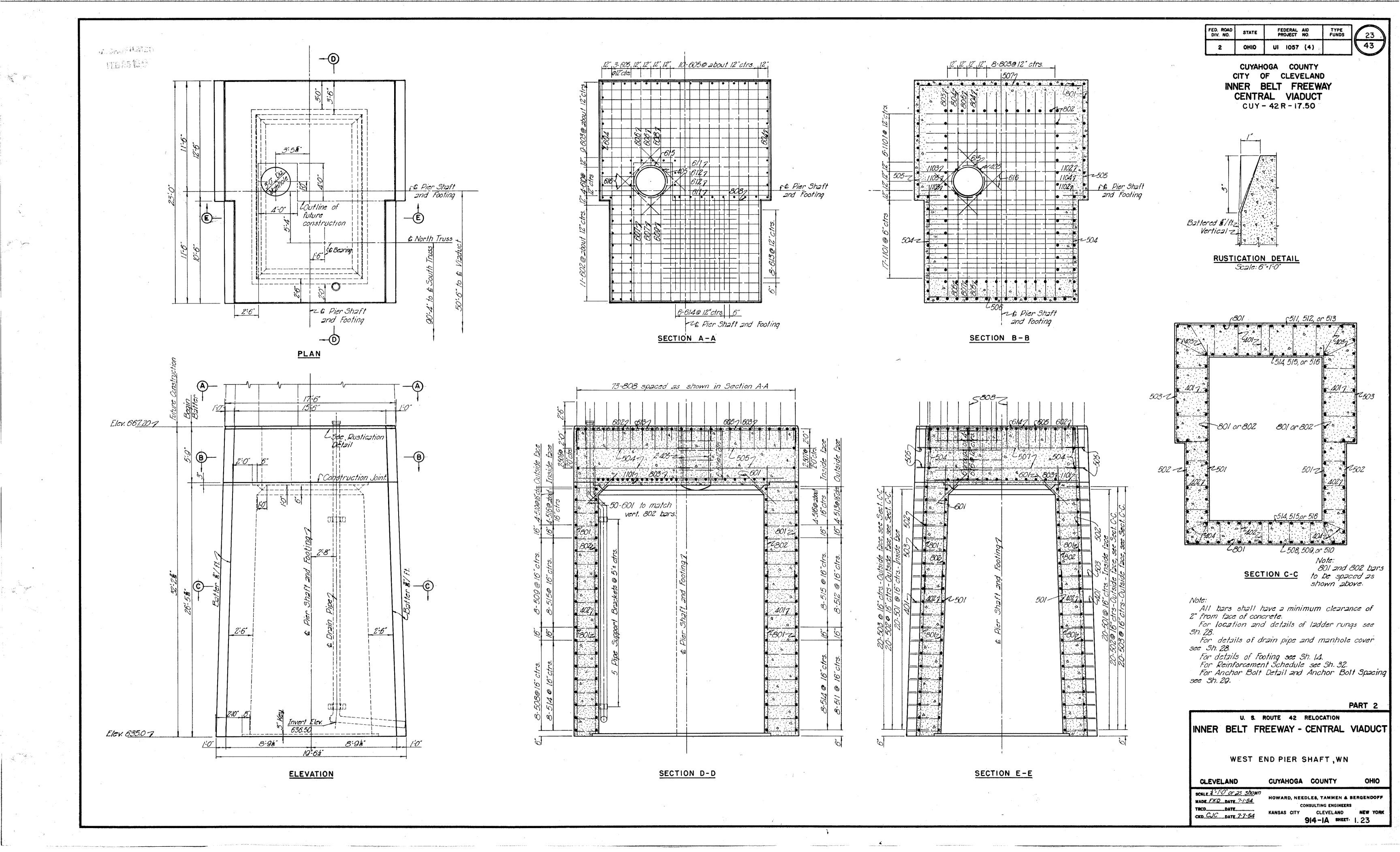


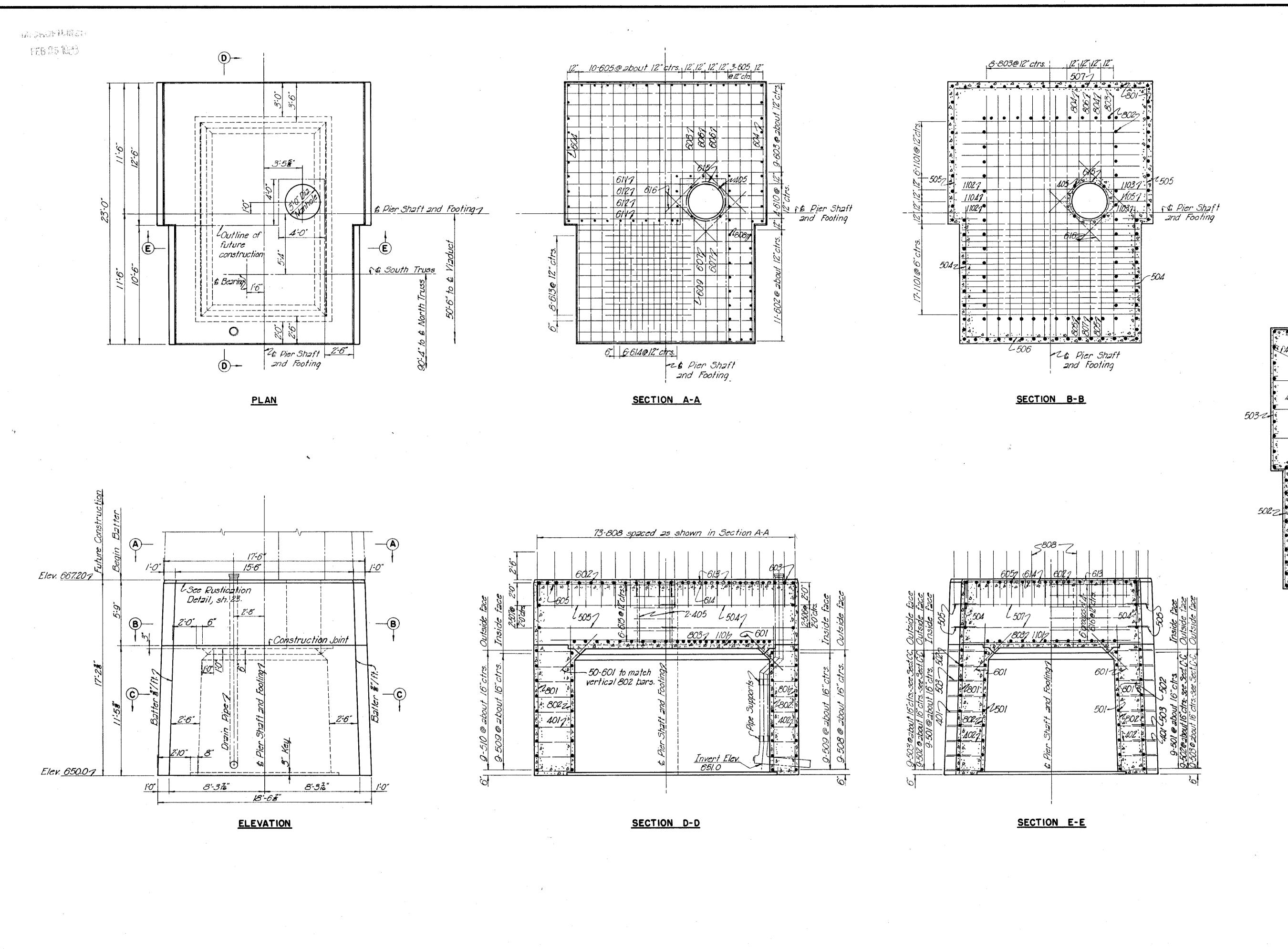








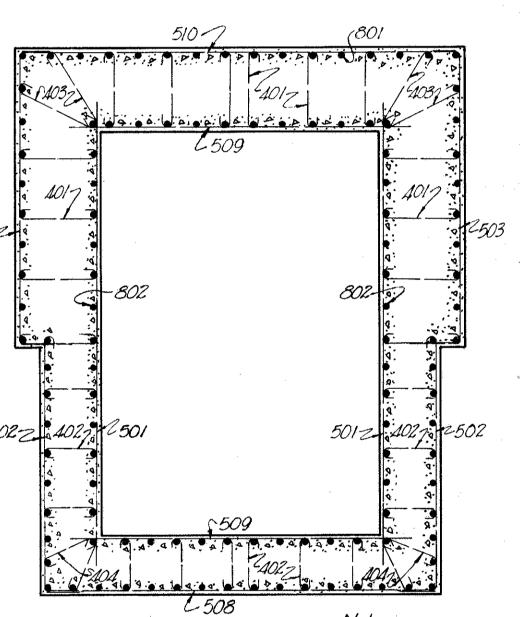




FED. ROAD DIV. NO. STATE FEDERAL AID PROJECT NO. FUNDS

2 OHIO UI 1057 (4)

CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT
CUY - 42 R - 17.50



SECTION C-C

Note:

All bars shall have a minimum clearance of 2" from face of concrete.

For location and details of ladder rungs see

For location and details of ladder rungs see 5h. 28.

For details of drain pipe and manhole cover see 5h. 28.

see Sh. 28.

For details of Footing see Sh. 14.

For Reinforcement Schedule see sh. 32.

For Anchor Bolt Detail and Anchor Bolt

Spacing see sh. 29.

U. S. ROUTE 42 RELOCATION
INNER BELT FREEWAY - CENTRAL VIADUCT

Note: 801 and 802 bars to be spaced as shown

WEST END PIER SHAFT, WS

CLEVELAND CUYAHOGA COUNTY OHIO

SCALEX 100 HOWARD, NEEDLES, TAMMEN & BERGENDOFF

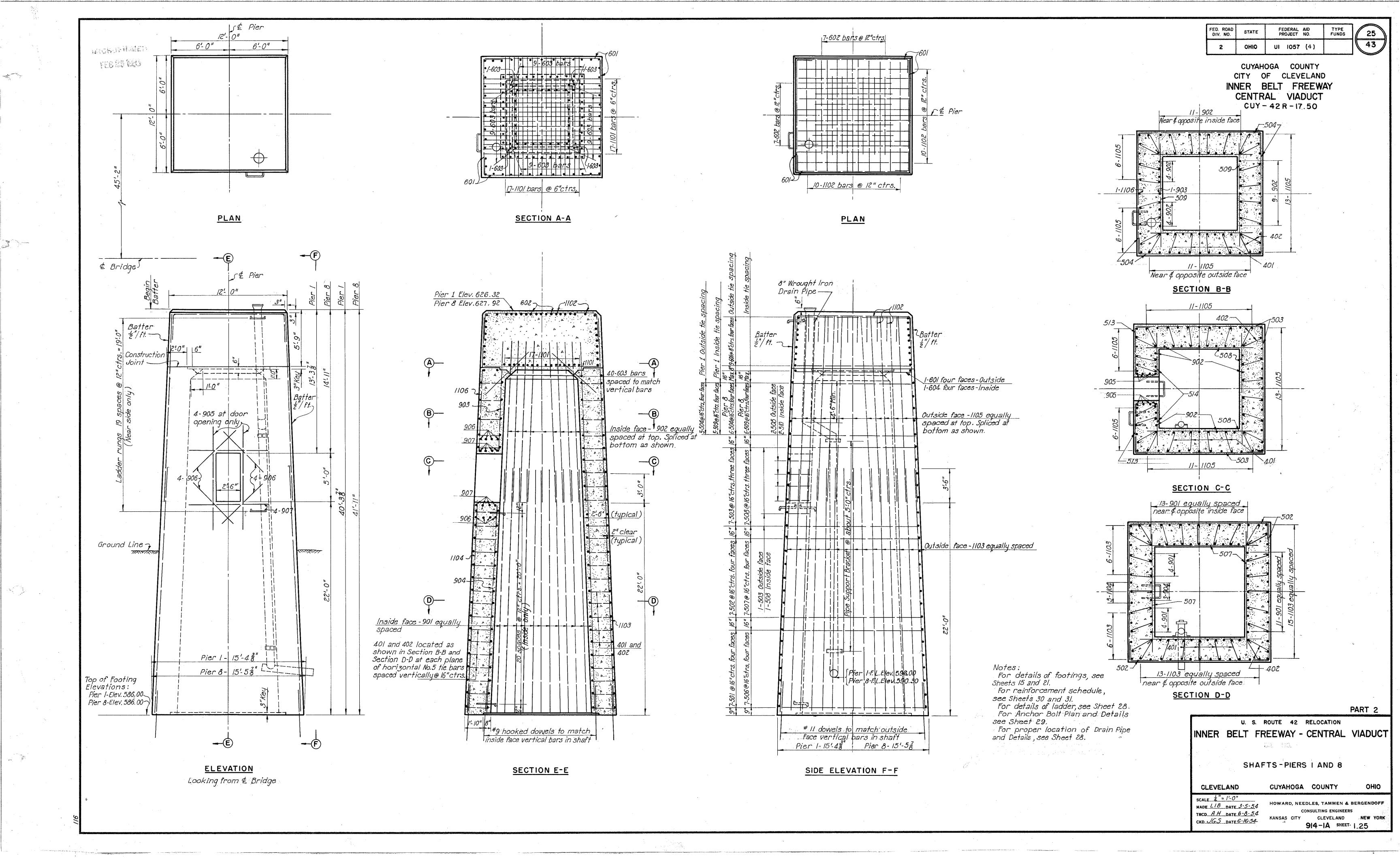
CONSULTING ENGINEERS

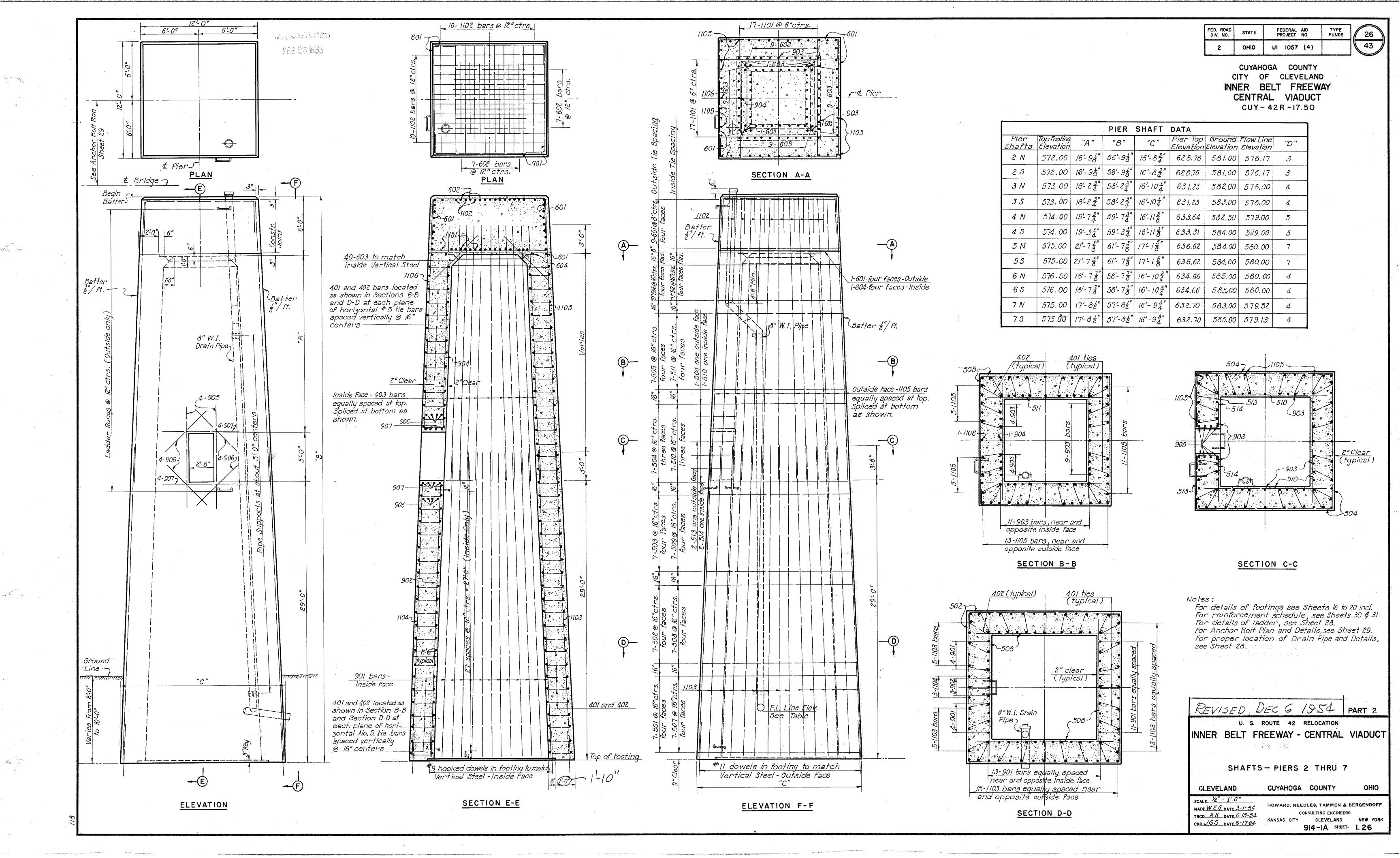
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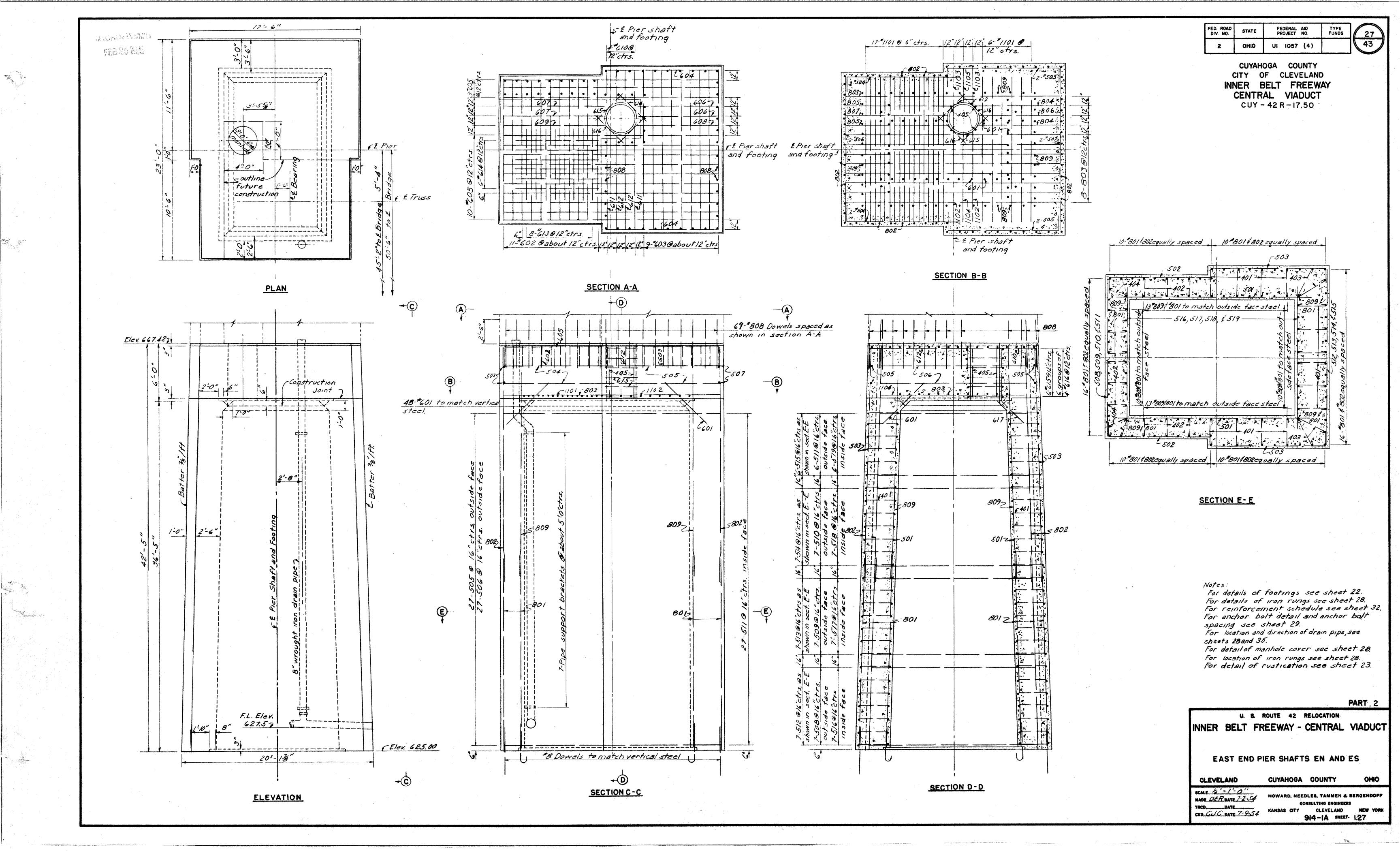
CKD CJC DATE 7-7-54

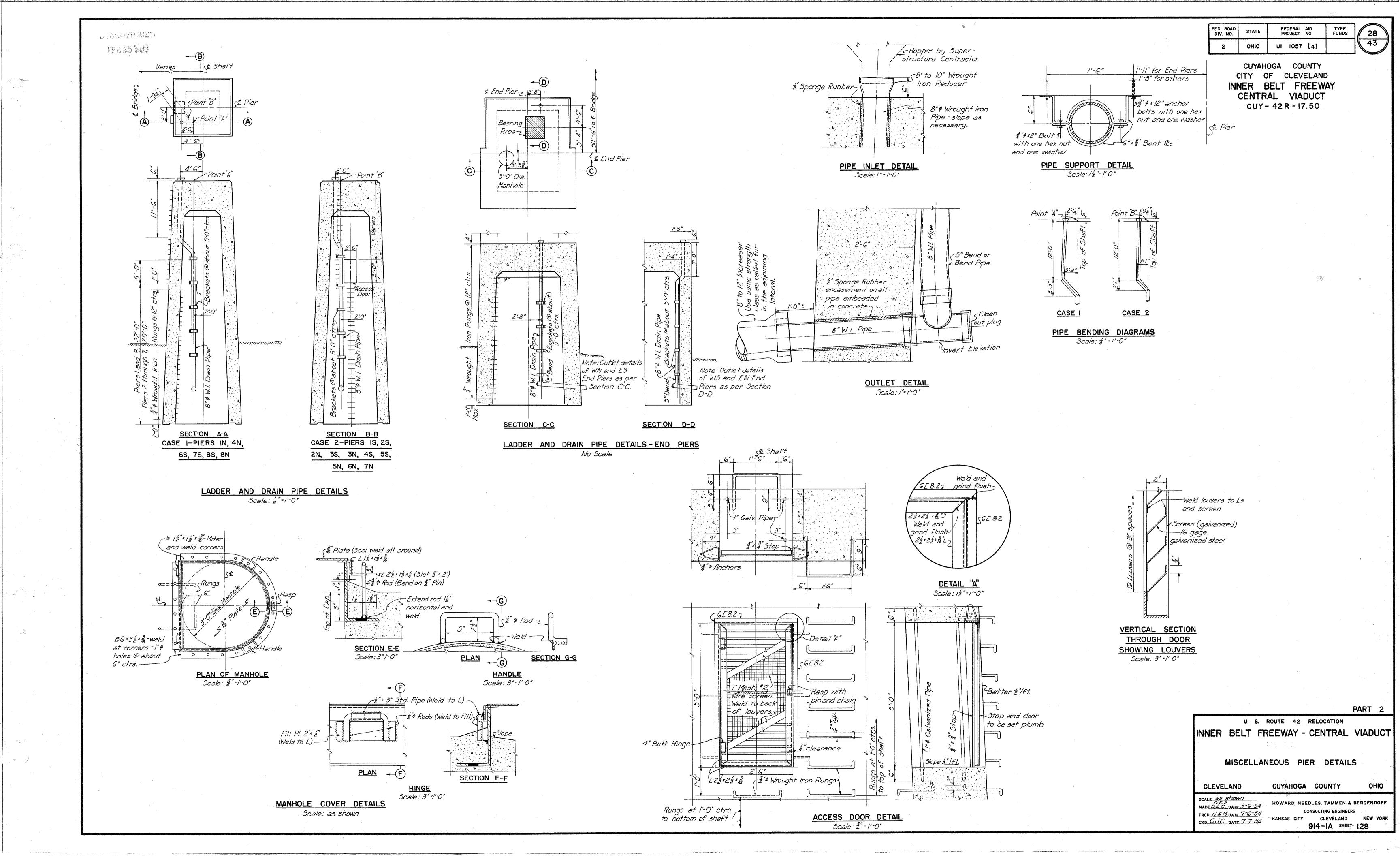
KANSAS CITY CLEVELAND NEW YORK

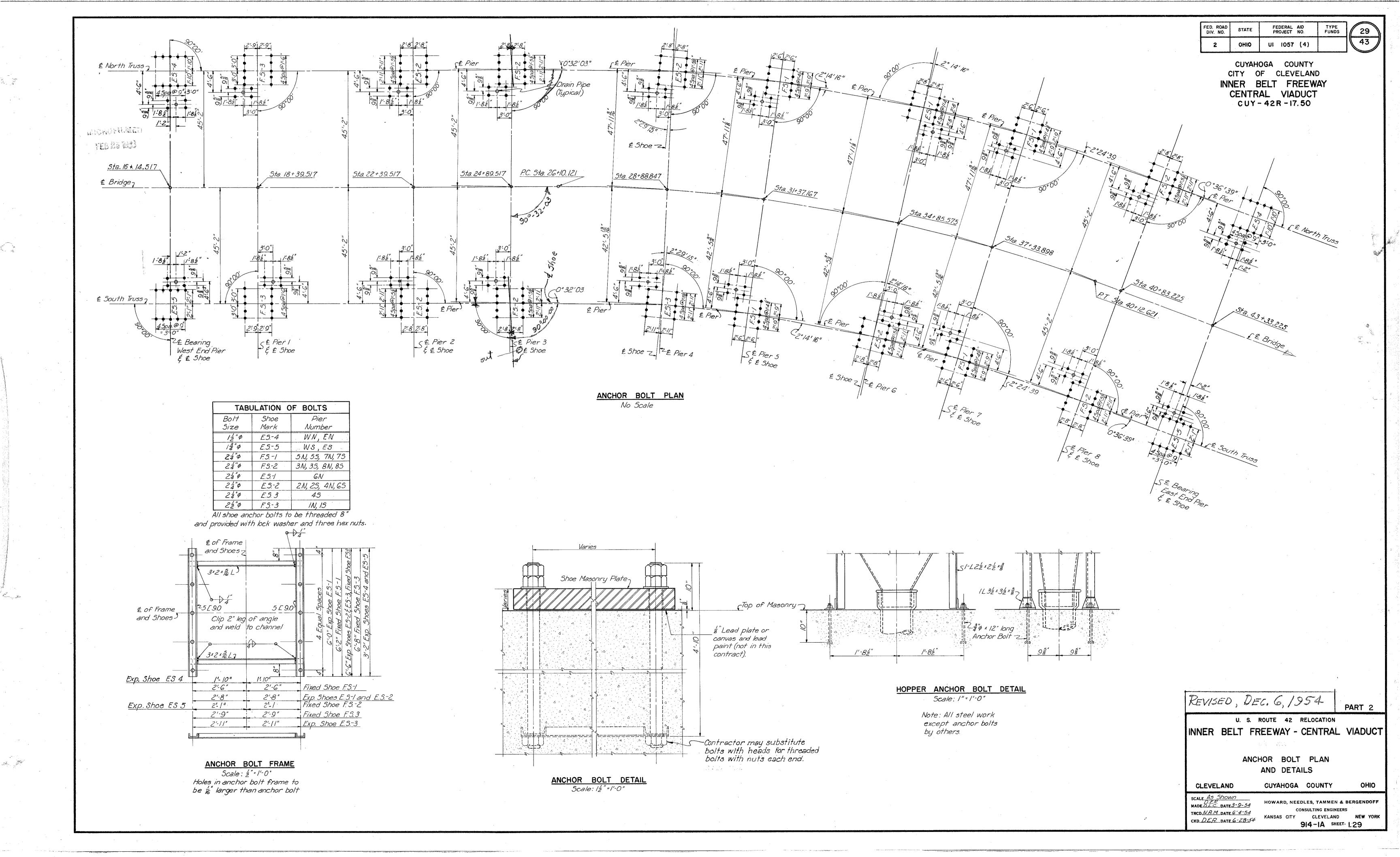
914-1A SHEET 1.24











PESIT RES

	SIZE	NO.	LENGTH	TYPE	DIMENSION A B	WEIGHT
	<del></del>		PIER FO	OTING	1-N	
601	6 6	41	35' - 6" 39' - 6"	Str.		2,186
602	•	37		otr.		2,195
901	9	48	5' - 9"	101	rt a - f fa-	8 <b>" 938</b>
1101,	11		35' + 6"	Str.		15,466
1102	11	1 <u>2</u> 4	39" - 6" 9" - 0"	Str.		26,023 2,678
1100		50				
			PIER FO	OTING	I-S	
601	6	41	35' - 6"	Str.		2,186
602	6		391 - 6"	Str.		2,195
901	9	48	5* - 9*	101	d 1, 1,-	8 938
1101	11	82	35" - 6"	Str.	`	15.466
1102	11	124	391 - 6"	Str.		26,023
1103	11	56	9' - 0"	Str.		2,678
	<u> </u>		OIED FO	OTING	2 N	
	<del>,</del>		PIER FO		Z-IN	A
601	6	74	35' - 6"	Str.	that have real?	3,946
901	9	48	5' - 9"	101	41 - 1711-	8 938
1101	11	182	35" - 6"	Str.		34,327
1102	11	56	8t - O#	Str.		2,380
			· · · · · · · · · · · · · · · · · · ·			
	,	<del>,</del>	PIER FO		2-5	
601	6	3 <b>3</b>	39 <b>' - 6"</b> 31' - 6"	Str.	·	1.958 8.469
901	9	48	5' - 9"	101	4" - 1" ["-	
1101	11	110	39" - 6"	Str.		23,085
1102	11	56	9' - 0"	Str.		2,678
<del> </del>	<del></del>	<del> </del>		OTING	3-N	
601 602	6	37 41	39' - 6" 35' - 6"	Str.		2,195 <b>2,</b> 186
901	9	48	<u>5' - 9"</u>	101	4, - 1, 1,-	8 938
1101	,	108	39' - 6"	Str.		22,665
1102	11	70 56	35! - 6" 9! - 0"	Str.		13,203 2,678
			PIER FO	OTING	3 <b>-</b> S	
601	6 6	37 41	39' - 6" 35' - 6"	Str.		2,195 2,186
602	0	41	əə⁻. <b>-</b> 0	JIT.	-	
901	9	48	51 - 9"	101	41 - 1" 11-	8 938
1101		108	39' - 6"	Str.		22,665
1102	11	70 .56	35" - 6" 9" - 0"	Str.		13,203 2,678
<del></del>			PIER FO	OTING	4-N	
601	6	74	351 - 6"	Str.		3,946
901	9	48	5' - 9"	101	H4 In I4-	8 938
1101 1102	 	182 56	35' - 6" 8' - 0"	Str.		34,327 2,380
1144	41	70	<u> </u>	J, 1 ·		2,300
				+		
	<u> </u>		PIER FO	OTING	4-S	
601	6	41	35+ - 6*	Str.		2,186
602	6	37	39' - 6"	Str.		2,195
901	9	48	51 - 9"	101	40 - 10 10-	8 938
		70				13,203
1101		. /tii	351 - 6"	Str.		1 10,403
1101	11	116 56	391 - 6" 91 - 0"	Str.		24,344 2,678

	SIZE	NO.	LENGTH	TYPE	DIMENSIO A	N	WEIGHT LBS.
	<u>L</u>	<u>.                                    </u>	PIER FOO	DTING	5-N _		<u> </u>
601	6	74	35' - 6"	Str.	<u> </u>		3,94
901	9	48	51 - 91	101	u -   +	11-8	
						-0	
1101	11	182 56	35" - 6" 8" - 0"	Str.			34,32° 2,380
		•	PIER FOO	TING	5-S		
601	6	41	35' - 6"	Str.			2,180
602	6	37	39' - 6"	Str.			2,19
901	9	48	5' - 9"	101	tt 1.	1 -8	938
1101	11	70	35* - 6*	Str.		<del> </del>	13,20
1102	11	116	39" - 6" 9" - 0"	Str. Str.			24,341 2,678
1103	11	56	3 0.	30.			2,612
<del></del>						-	· • · · · · · · · · · · · · · · · · · ·
	<u> </u>		PIER FO	DTING	6-N		
601	6	74	35' - 6"	Str.	0 14	]	3,94
901	9	48	5' - 9"	101	#1 - 1"	1'-8"	931
1101	11	182	35* - 6*	Str.			34,327
1102	11	56	81 - 0"	Str.			2,38(
	L		PIER FO	OTING	6-6	<u> </u>	
601	6	74	351 - 6"	Str.	0-3	Ţ .	3,940
901	9	48	5! - 9"	101	. #1 - 1 m	8"	938
1101	j i	182 56	35' - 6" 8' - 0"	Str.			34,327
1102		20	8, -0	Str.			2,380
`							
	<u></u>		PIER FO	OTING	7-N	<u> </u>	. :
601	6	74	351 - 6"	Str.			3,946
001		МО	5" 9"	101	ψ* ;= 1*	#-8"	
901	. 9	<b>48</b>		101	<b>4</b> , <b>-</b> 1	r-0	938
1101	11	182 .56	35" - 6" 8" - 0"	Str.			34,327 2,380
							2,000
			-				
,			PIER FO	OTING	7 <b>-</b> S		
601	6	41	35' - 6"	Str.			2,186
	6	37	39' - 6"	Str.			2,19
602		48				<b> </b>	026
901	9	70	51 9*	101	t + - f	F-87	300
901					rt + - 1 =	F-8"	
901 1101 1102	11	70 116	35' - 6" 39' - 6"	Str.	4* - 1*	F-8	13,203
901	11	70	35' - 6"	Str.	4* - 1*	F-8	13,203
901 1101 1102	11	70 116	35' - 6" 39' - 6"	Str.	4* - 1*	8-8	13,203
901 1101 1102	11	70 116	35' - 6" 39' - 6" 9' - 0"	Str. Str. 5tr.		F-8	13,203
901 1101 1102	11	70 116	35' - 6" 39' - 6" 9' - 0"	Str.		8-7	13,203 24,344 2,678
901 1101 1102 1103	11	70 116 .56	35' - 6" 39' - 6" 9' - 0" PIER FOO	Str. Str. Str. OTING	8-N		13,203 24,344 2,678
901 1101 1102 1103	11	70 116 56	35' - 6" 39' - 6" 9' - 0"	Str. Str. 5tr.		F-8*	13,203 24,344 2,678 3,946
901 1101 1102 1103 601 901	6	70 116 56 74 48	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str.  OTING Str.  101	8-N		3,946 36,968
901 1101 1102 1103 601	6 9	70 116 56 74 48	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6"	Str. Str. Str. OTING	8-N		13,203 24,344 2,678 3,946
901 1102 1103 601 901	6	70 116 56 74 48	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str.  OTING Str.  101	8-N		3,946 36,968
901 1102 1103 601 901	6	70 116 56 74 48	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9" 35' - 6" 9' - 0"	Str. Str. Str. OTING Str. 101 Str. Str.	8-N		13,203 24,344 2,678 3,946 938
901 1102 1103 601 901	6	70 116 56 74 48	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9" 35' - 6" 9' - 0"	Str. Str. Str. OTING Str. 101 Str. Str.	8-N		13,203 24,344 2,678 3,946 938 36,968 2,678
901 1101 1102 1103 601 901 1101 1102	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6"	Str. Str. Str.  OTING Str.  OTING Str.  Str.  Str.	8-N 4' - I"	F-8*	3,946 3,946 3,946
901 1102 1103 601 901 1101 1102	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO	Str. Str. Str. OTING Str. IOI Str. Str.	8-N		13,203 24,344 2,678 3,946 938
901 1102 1103 601 901 1101 1102	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str. OTING Str. OTING Str. OTING Str.	8-N 4' - I"	F-8*	3,946 3,946 3,946 3,946 3,946 3,946 3,946
901 1102 1103 601 901 1101 1102	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6"	Str. Str. Str.  DTING Str.  101 Str. Str.  Str.  101	8-N 4' - I"	F-8*	3,946 3,946 3,946
901 1101 1102 1103 601 901 1101 901	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str. OTING Str. OTING Str. OTING Str.	8-N 4' - I"	F-8*	3,946 3,946 36,968 2,678 3,946 3,946 3,946
901 1102 1103 601 901 1101 1102	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str. OTING Str. OTING Str. OTING Str.	8-N 4' - I"	F-8*	3,946 3,946 36,968 2,678 3,946 3,946 3,946
901 1101 1102 1103 601 901 1101 901	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str. OTING Str. OTING Str. OTING Str.	8-N 4' - I"	F-8*	3,946 3,946 36,968 2,678 3,946 3,946 3,946
901 1102 1103 601 901 1101 1102	6 9	70 116 56 74 48 196 56	35' - 6" 39' - 6" 9' - 0" PIER FOO 35' - 6" 9' - 0" PIER FOO 35' - 6" 5' - 9"	Str. Str. Str. OTING Str. OTING Str. OTING Str.	8-N 4' - I"	F-8*	3,946 3,946 36,968 2,678 3,946 3,946 3,946

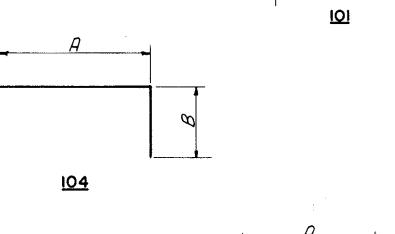
	MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIO		WEIGHT
401			L		L	A 8N	<b>B</b>	LBS.
	401	ц	505				1	1.097
502   5   28   15' - 11'   104   13! - 6'   2-5'   194     503   5   24   15' - 1'   104   11' - 8'   2-5'   378     504   5   24   14' - 4'   104   11' - 11'   2-5'   359     506   5   28   13' - 6'   5tr   378     507   5   28   13' - 6'   5tr   378     508   5   24   12' - 9'   5tr   372     509   5   24   12' - 6'   5tr   372     509   5   24   12' - 6'   5tr   372     509   5   24   12' - 6'   5tr   372     509   5   24   12' - 9'   5tr   372     514   5   8   8' - 5'   120   4' - 5'   1-11'   70     601   6   40   13' - 8'   104   11' - 2'   2' 5'   821     602   6   14   7' - 0'   5tr   350     603   6   40   6' - 0'   5tr   366     604   6   4   11' - 0'   5tr   378     905   9   30   17' - 0'   5tr   378     902   9   30   17' - 0'   5tr   378     903   9   1   11' - 9'   5tr   329     904   9   3   21' - 6'   5tr   321     907   9   6   8' - 6'   5tr   323     907   9   6   8' - 6'   5tr   323     100   11   34   12' - 0'   5tr   323     100   11   32   12' - 0'   5tr   323     100   11   32   12' - 0'   5tr   323     100   11   47   19' - 6'   5tr   378     100   11   47   19' - 6'   5tr   378     100   11   47   19' - 6'   5tr   378     503   5   24   14' - 4'   100   12' - 2'   2'-5'   494     100   11   47   19' - 6'   5tr   378     503   5   24   14' - 4'   100   12' - 2'   2'-5'   494     504   5   28   16' - 7'   104   14' - 2'   2'-5'   494     505   5   28   15' - 1'   104   12' - 2'   2'-5'   494     504   5   24   14' - 4'   104   11' - 11'   2'-5'   355     503   5   24   14' - 4'   104   11' - 11'   2'-5'   355     504   5   24   14' - 4'   104   11' - 11'   2'-5'   356     505   5   28   13' - 6'   5tr   378     506   5   28   13' - 6'   5tr   378     507   5   28   15' - 1'   104   14' - 2'   2'-5'   494     509   5   24   11' - 0'   5tr   394     500   5   24   14' - 0'   5tr   394     501   5   8   8' - 5'   120   4' - 5'   1-11'   2'-5'   395     503   5   24   14' - 0'   5tr   394     504   5   24   14' - 0'   5tr   394     505   5   28   15' - 0'   5tr   394     506   5   6   14'			+					
502   5   28   15' - 11'   104   13! - 6'   2-5'   194     503   5   24   15' - 1'   104   11' - 8'   2-5'   378     504   5   24   14' - 4'   104   11' - 11'   2-5'   359     506   5   28   13' - 6'   5tr   378     507   5   28   13' - 6'   5tr   378     508   5   24   12' - 9'   5tr   372     509   5   24   12' - 6'   5tr   372     509   5   24   12' - 6'   5tr   372     509   5   24   12' - 6'   5tr   372     509   5   24   12' - 9'   5tr   372     514   5   8   8' - 5'   120   4' - 5'   1-11'   70     601   6   40   13' - 8'   104   11' - 2'   2' 5'   821     602   6   14   7' - 0'   5tr   350     603   6   40   6' - 0'   5tr   366     604   6   4   11' - 0'   5tr   378     905   9   30   17' - 0'   5tr   378     902   9   30   17' - 0'   5tr   378     903   9   1   11' - 9'   5tr   329     904   9   3   21' - 6'   5tr   321     907   9   6   8' - 6'   5tr   323     907   9   6   8' - 6'   5tr   323     100   11   34   12' - 0'   5tr   323     100   11   32   12' - 0'   5tr   323     100   11   32   12' - 0'   5tr   323     100   11   47   19' - 6'   5tr   378     100   11   47   19' - 6'   5tr   378     100   11   47   19' - 6'   5tr   378     503   5   24   14' - 4'   100   12' - 2'   2'-5'   494     100   11   47   19' - 6'   5tr   378     503   5   24   14' - 4'   100   12' - 2'   2'-5'   494     504   5   28   16' - 7'   104   14' - 2'   2'-5'   494     505   5   28   15' - 1'   104   12' - 2'   2'-5'   494     504   5   24   14' - 4'   104   11' - 11'   2'-5'   355     503   5   24   14' - 4'   104   11' - 11'   2'-5'   355     504   5   24   14' - 4'   104   11' - 11'   2'-5'   356     505   5   28   13' - 6'   5tr   378     506   5   28   13' - 6'   5tr   378     507   5   28   15' - 1'   104   14' - 2'   2'-5'   494     509   5   24   11' - 0'   5tr   394     500   5   24   14' - 0'   5tr   394     501   5   8   8' - 5'   120   4' - 5'   1-11'   2'-5'   395     503   5   24   14' - 0'   5tr   394     504   5   24   14' - 0'   5tr   394     505   5   28   15' - 0'   5tr   394     506   5   6   14'	501	F.	20	161 - 74	LOU	U	2-5*	ii oii
5	502	5	28	15" - 11"	104	13' - 6"	2'-5"	
513   5			1				7	378
Soc   5   28   13' - 6'   Str.   394			_				<del></del>	
507   5   28   12' - 9"   Str.   372						4, - 11	2 -5	
Solid   Soli		5	28	12" - 9"	Str.			372
5   8   8   -5"   120			<b></b>				1	300
100						41 - 5"	1-11	70
100	601	6	40	13! - 8"	ION	11! - 2"	2*6#	821
00			<del>}</del>					
901 9 45 24' - 9" Str. 3.787 902 9 39 17' - 0" Str. 2.255 903 9 1 11' - 9" Str. 2.255 903 9 1 11' - 9" Str. 2.255 905 9 8 11' - 0" Str. 2.29 906 9 16 5' - 9" Str. 2.31 907 9 8 8' - 6" Str. 2.31 1101 111 34 12' - 0" Str. 2.31 1102 11 20 19' - 0" 121 2.018 1103 11 53 25' - 6" Str. 3.75 1106 11 1 47 19' - 6" Str. 4.870 1106 11 1 1 47 19' - 6" Str. 7.5 1106 11 1 1 47 19' - 6" Str. 7.5 1107 1 5 28 16' - 7" 104 14' - 2" 2'-5" 464 1502 5 28 15' - 11" 104 13' - 6" 2'-5" 464 1503 5 24 15' - 1" 104 12' - 8" 2'-5" 355 1504 5 28 13' - 6" Str. 2.25 1505 5 28 13' - 6" Str. 2.25 1506 5 28 13' - 6" Str. 2.25 1507 5 28 12' - 9" Str. 2.26 1509 5 24 11' - 3" Str. 2.26 1509 5 24 12' - 9" Str. 2.26 1509 6 40 13' - 8" 104 11' - 11" 2'-5" 355 1509 5 24 12' - 9" Str. 2.26 1509 6 40 13' - 8" 104 11' - 1" 2'-5" 359 1509 6 9 16 6' - 0" Str. 2.26 1509 7 9 8 8 8' - 5" 120 4' - 5" 1-1" 70 1109 9 45 24' - 9" Str. 2.26 1109 9 16 5' - 9" Str. 2.26 1109 11 3 41' - 0" Str. 2.26 1109 11 3 41' - 0" Str. 2.26 1109 11 3 41' - 0" Str. 3.28 1100 11 3 41' - 0" Str. 3.28 1100 11 3 41' - 0" Str. 3.29 1101 11 34 12' - 0" Str. 3.21							<del>  </del>	
902 9 39 17' - 0" Str. 903 9 1 11' - 9" Str. 909 9 9 1 11' - 9" Str. 909 9 3 21' - 6" Str. 219 905 9 8 11' - 0" Str. 219 905 9 8 11' - 0" Str. 219 907 9 8 8' - 6" Str. 231 1100 11 34 12' - 0" Str. 231 1100 11 34 12' - 0" Str. 231 1100 11 32 11 - 9" Str. 311 32 11 104 11 3 21' - 9" Str. 311 32 11 104 11 3 21' - 9" Str. 347 1105 11 47 19' - 6" Str. 75 1106 11 1 1 14' - 3" Str. 75 1106 11 1 1 14' - 3" Str. 75 1106 11 1 1 14' - 3" Str. 75 1106 11 1 1 14' - 3" Str. 100 11' - 11" 1,097 1402 4 216 3' - 4" 100 2' - 0" 981 15' - 11" 104 11' - 2" 2' -5" 464 1503 5 24 15' - 11" 104 11' - 12' - 8" 2' -5" 464 1503 5 24 15' - 1" 104 11' - 11" 2' -5" 359 153 5 24 15' - 1" 104 11' - 11" 2' -5" 359 153 5 28 12' - 9" Str. 327 2550 5 24 11' - 3" Str. 329 30 39 17' - 0" Str. 329 30 3	#U 0	0	4	11' - 0"	str.			66
903 9 1 11 9 9 Str. 40 904 9 3 21 6 8 Str. 219 905 9 8 11 0 8 Str. 219 906 9 16 5 9 9 Str. 313 907 9 8 8 11 2 0 Str. 313 907 9 8 8 8 9 6 Str. 313 907 9 8 8 8 9 6 Str. 313 907 9 8 8 8 9 6 Str. 313 907 9 8 8 8 9 6 Str. 313 907 9 8 8 8 9 6 Str. 313 907 1 10 1 1 34 12 0 12 0 Str. 110 1 1 1 2 2 0 19 1102 11 20 19 0 121 2 2 0 19 1103 11 53 25 6 Str. 7, 181 1104 11 3 21 9 Str. 31 1105 11 47 19 6 Str. 31 34 1105 11 47 19 6 Str. 75 1106 11 1 1 14 3 21 9 Str. 31 1106 11 1 1 14 3 21 9 Str. 75 1107 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	901	9	45		Str.			3,787
904 9 3 21' - 6" Str. 219 905 9 8 11' - 0" Str. 229 906 9 16 5' - 9" Str. 231 907 9 8 8' - 6" Str. 231 907 9 8 8' - 6" Str. 231 907 9 8 8' - 6" Str. 231 1101 11 34 12' - 0" Str. 241 1102 11 20 19' - 0" 121 1103 11 53 25' - 6" Str. 7, 181 1104 11 3 21' - 9" Str. 38, 1104 11' - 2" 2' - 5" 821 1106 11 1 1 14' - 3" Str. 75  401 4 505 3' - 3" 100 1' - 11" 1,097 402 4 216 3' - 4" 100 2' - 0" 481 501 5 28 16' - 7" 104 13' - 6" 2' -5" 494 502 5 28 15' - 11" 104 12' - 8" 2' -5" 494 503 5 24 15' - 1" 104 12' - 8" 2' -5" 494 504 5 28 13' - 6" Str. 39 507 5 28 12' - 9" Str. 39 508 5 24 12' - 0" Str. 39 509 5 24 11' - 3" Str. 322 508 5 24 12' - 0" Str. 300 601 6 40 13' - 8" 100 11' - 2" 2' -5" 821 602 6 14 7' - 0" Str. 300 601 6 40 6' - 0" Str. 366 604 6 4 11' - 0" Str. 366 604 6 4 11' - 0" Str. 366 901 9 45 24' - 6" Str. 312 907 9 8 8' - 6" Str. 312 101 11 34 12' - 0" Str. 360 907 9 8 8' - 6" Str. 312 101 11 34 12' - 0" Str. 360 907 9 8 8' - 6" Str. 312 101 11 34 12' - 0" Str. 360 907 9 8 8' - 6" Str. 312 101 11 34 12' - 0" Str. 329 908 9 16 5' - 9" Str. 329 909 9 16 5' - 9" Str. 329 900 9 16 5' - 9" Str. 312 101 11 34 12' - 0" Str. 312 102 11 20 19' - 0" Str. 312 103 11 53 25' - 6" Str. 312 104 11 3 21' - 9" Str. 312 105 11 47 19' - 6" Str. 7. 181 105 11 47 19' - 6" Str. 7. 181			39		<del>                                     </del>			
905  9  8  111 - 0"  Str.  299 906  9  16  5' - 9"  Str.  313 907  9  8  8' - 6"  Str.  221  1101  111  34  12' - 0"  Str.  2.168  1102  11  20  19' - 0"  121 1103  11  53  25' - 6"  Str.  7.181 1104  11  3  21' - 9"  Str.  337 1105  11  47  19' - 6"  Str.  7.5  1106  11  1  14' - 3"  Str.  7.5  1107  11  47  19' - 6"  Str.  7.5  1108  11  47  19' - 6"  Str.  7.5  1109  11  1  14' - 3"  Str.  7.5  1100  11  1  14' - 3"  Str.  7.5  1100  12  14' - 3"  Str.  7.5  1100  13  14' - 10'  14' - 2"  2'-5"  484 1100  12' - 0"  481 1100  13' - 6"  2'-5"  484 1100			1 2				<del>  </del>	·····
906						<u> </u>	1 1	
	906	9	16	51 - 9"	Str.			313
	907	9	8	8' - 6"	Str.			231
1102	1101	11	34		Str.			2.168
1103	1102			19' - 0"	. I			2.019
1105	1103		53	25* - 6*	Str.		1	7,181
		_					<del>                                     </del>	
101			1					75
101								
101								
101								
101								
402					SHAFT		,	
Soi   S   28   16' - 7"   104   14' - 2"   2' - 5"   484				3' - 3"				
502         5         28         15' - 11"         104         13' - 6"         2'-5"         464           503         5         24         15' - 1"         104         12' - 8"         2'-5"         378           504         5         24         14' - 4"         104         11' - 11"         2'-5"         359           513         5         8         7' - 4"         104         4' - 11"         2'-5"         61           506         5         28         13' - 6"         Str.         394         372           507         5         28         12' - 9"         Str.         372         372           508         5         24         12' - 0"         Str.         300         300           509         5         24         12' - 0"         Str.         282         514         5         8         8' - 5"         120         4' - 5"         1-11"         70           601         6         40         6' - 0"         Str.         360         40         6' - 0"         Str.         360           604         6         4         11' - 0"         Str.         3.787         3.787           902 </td <td>702</td> <td></td> <td>210</td> <td></td> <td>100</td> <td>2 0</td> <td></td> <td>701</td>	702		210		100	2 0		701
502         5         28         15' - 11"         104         13' - 6"         2'-5"         464           503         5         24         15' - 1"         104         12' - 8"         2'-5"         378           504         5         24         14' - 4"         104         11' - 11"         2'-5"         359           513         5         8         7' - 4"         104         4' - 11"         2'-5"         61           506         5         28         13' - 6"         Str.         394         372           507         5         28         12' - 9"         Str.         372         372           508         5         24         12' - 0"         Str.         300         300           509         5         24         12' - 0"         Str.         282         514         5         8         8' - 5"         120         4' - 5"         1-11"         70           601         6         40         6' - 0"         Str.         360         40         6' - 0"         Str.         360           604         6         4         11' - 0"         Str.         3.787         3.787           902 </td <td>501</td> <td>5</td> <td>28</td> <td>16' - 7"</td> <td>1 04</td> <td> 4" - 2"</td> <td>2'-5"</td> <td>484</td>	501	5	28	16' - 7"	1 04	4" - 2"	2'-5"	484
504         5         24         14" - 4"         104         11" - 11"         2'-5"         359           513         5         8         7" - 4"         104         4" - 11"         2'-5"         61           506         5         28         13" - 6"         3tr.         394           507         5         28         12" - 9"         3tr.         300           508         5         24         12" - 0"         3tr.         282           509         5         24         11" - 3"         3tr.         282           514         5         8         8" - 5"         120         4" - 5"         4" 11"         70           601         6         40         13" - 8"         104         11" - 2"         2" - 6"         821           602         6         14         7" - 0"         3tr.         360         604         6" - 0"         3tr.         360           604         6         4         11" - 0"         3tr.         2.255         360           901         9         45         24" - 9"         3tr.         3.787         2.255           903         9         11" - 9"         3tr.<		5	<del> </del>				2'-5"	
513         5         8         7' - 4"         104         4' - 11"         2'-5"         61           506         5         28         13" - 6"         Str.         394           507         5         28         12' - 9"         Str.         372           508         5         24         12' - 0"         Str.         282           509         5         24         11' - 3"         Str.         282           514         5         8         8' - 5"         120         4' - 5"         1-11"         70           601         6         40         13' - 8"         104         11' - 2"         2'-6"         821           602         6         14         7' - 0"         Str.         360         40         6' - 0"         Str.         360           604         6         4         11' - 0"         Str.         2.255         3787           902         9         39         17' - 0"         Str.         2.255         40           904         9         3         21' - 6"         Str.         219         313           907         9         8         11' - 0"         Str. <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>2'-5"</td><td></td></td<>							2'-5"	
506         5         28         13° - 6"         Str.         394           507         5         28         12° - 9"         Str.         372           508         5         24         12° - 0"         Str.         282           514         5         8         8° - 5"         120         4° - 5"         ½""         70           601         6         40         13° - 8"         104         11° - 2"         2"-6"         821           602         6         14         7° - 0"         Str.         360         604         6° - 0"         Str.         360           604         6         4         11° - 0"         Str.         3.787         902         9         39         17° - 0"         Str.         2.255         903         9         11° - 9"         Str.         2.168         2.255         906 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
508         5         24         12' - 0"         Str.         300           509         5         24         11' - 3"         Str.         282           514         5         8         8' - 5"         120         4' - 5"         1-11"         70           601         6         40         13' - 8"         104         11' - 2"         2'-6"         821           602         6         14         7' - 0"         Str.         147           603         6         40         6' - 0"         Str.         360           604         6         4         11' - 0"         Str.         66           901         9         45         24' - 9"         Str.         2.255           903         9         1         11' - 9"         Str.         2.255           903         9         1         11' - 9"         Str.         219           904         9         3         21' - 6"         Str.         219           905         9         8         11' - 0"         Str.         231           907         9         8         8' - 6"         Str.         231           101			$\overline{}$					-,
509       5       24       11' - 3"       Str.       282         514       5       8       8' - 5"       120       4' - 5"       ½-1½"       70         601       6       40       13' - 8"       104       11' - 2"       2'-6"       821         602       6       14       7' - 0"       Str.       147         603       6       40       6' - 0"       Str.       360         604       6       4       11' - 0"       Str.       65         901       9       45       24' - 9"       Str.       2.255         902       9       39       17' - 0"       Str.       2.255         903       9       1       11' - 9"       Str.       2.255         903       9       1       11' - 9"       Str.       2.19         904       9       3       21" - 6"       Str.       2.19         905       9       8       11' - 0"       Str.       2.99         906       9       16       5' - 9"       Str.       2.168         102       11       34       12' - 0"       321       2.168         102       11 </td <td></td> <td></td> <td></td> <td></td> <td>1 1</td> <td></td> <td></td> <td></td>					1 1			
514       5       8       8" - 5"       120       4" - 5"       \$\frac{1}{1}\text{"}\$       70         601       6       40       13" - 8"       104       11" - 2"       \$\frac{7}{2}\text{-6}"       821         602       6       14       7" - 0"       \$\frac{1}{2}\text{Tr.}\$       360         603       6       40       6" - 0"       \$\frac{1}{2}\text{Tr.}\$       360         604       6       4       11" - 0"       \$\frac{1}{2}\text{Tr.}\$       3.787         902       9       39       17" - 0"       \$\frac{1}{2}\text{Tr.}\$       2.255         903       9       1       11" - 9"       \$\frac{1}{2}\text{Tr.}\$       2.19         904       9       3       21" - 6"       \$\frac{1}{2}\text{Tr.}\$       219         905       9       8       11" - 0"       \$\frac{1}{2}\text{Tr.}\$       299         906       9       16       5" - 9"       \$\frac{1}{2}\text{Tr.}\$       2.168         102       11       20       19" - 0"       \$\frac{1}{2}\text{Tr.}\$       2.168         102       11       3       25" - 6"       \$\frac{1}{2}\text{Tr.}\$       7.181         104       11       3       21" - 9"								
602       6       i4       7' - 0"       Str.       147         603       6       40       6' - 0"       Str.       360         604       6       4       1i' - 0"       Str.       66         901       9       45       24' - 9"       Str.       2.255         902       9       39       i7' - 0"       Str.       2.255         903       9       i 11' - 9"       Str.       40         904       9       3       21' - 6"       Str.       219         905       9       8       11' - 0"       Str.       299         906       9       16       5' - 9"       Str.       23i         101       1i       34       12' - 0"       Str.       23i         102       1i       20       19' - 0"       32i       2,019         103       1i       53       25' - 6"       Str.       7,18i         104       1i       3       21' - 9"       Str.       347         105       1i       47       19' - 6"       Str.       4,870						41 - 5"	\$-11°	
602       6       i4       7' - 0"       Str.       147         603       6       40       6' - 0"       Str.       360         604       6       4       1i' - 0"       Str.       66         901       9       45       24' - 9"       Str.       2.255         902       9       39       i7' - 0"       Str.       2.255         903       9       i 11' - 9"       Str.       40         904       9       3       21' - 6"       Str.       219         905       9       8       11' - 0"       Str.       299         906       9       16       5' - 9"       Str.       23i         101       1i       34       12' - 0"       Str.       23i         102       1i       20       19' - 0"       32i       2,019         103       1i       53       25' - 6"       Str.       7,18i         104       1i       3       21' - 9"       Str.       347         105       1i       47       19' - 6"       Str.       4,870	601	£	ΠU	131 0#	I VB	111 - 2*	21 - 5 11	ווס
603 6 40 6' - 0" Str. 360 604 6 4 11' - 0" Str. 66  901 9 45 24' - 9" Str. 3.787 902 9 39 17' - 0" Str. 2.255 903 9 1 11' - 9" Str. 40 904 9 3 21' - 6" Str. 219 905 9 8 11' - 0" Str. 299 906 9 16 5' - 9" Str. 313 907 9 8 8' - 6" Str. 231  101 11 34 12' - 0" Str. 231  102 11 20 19' - 0" Str. 231  103 11 53 25' - 6" Str. 7.181 104 11 3 21' - 9" Str. 347 105 11 47 19' - 6" Str. 4,870				71 - 0"		14' - 4"	4-0	
901 9 45 24' - 9" Str. 3.787 902 9 39 17' - 0" Str. 2.255 903 9 1 11' - 9" Str. 40 904 9 3 21' - 6" Str. 219 905 9 8 11' - 0" Str. 299 906 9 16 5' - 9" Str. 313 907 9 8 8' - 6" Str. 231  101 11 34 12' - 0" Str. 231  102 11 20 19' - 0" \$21 2.019 103 11 53 25' - 6" Str. 7.181 104 11 3 21' - 9" Str. 347 165 11 47 19' - 6" Str. 4,870	603	6	40	61 - 0*	Str.		1	360
902       9       39       17" - 0"       Str.       2.255         903       9       1       11" - 9"       Str.       40         904       9       3       21" - 6"       Str.       219         905       9       8       11" - 0"       Str.       299         906       9       16       5" - 9"       Str.       313         907       9       8       8" - 6"       Str.       231         101       11       34       12" - 0"       Str.       2.168         102       11       20       19" - 0"       321       2.019         103       11       53       25" - 6"       Str.       7.181         104       11       3       21" - 9"       Str.       347         105       11       47       19" - 6"       Str.       4,870	004	6	4	11' - 0"	Str.			66
903 9 1 11' - 9" Str. 219 904 9 3 21' - 6" Str. 219 905 9 8 11' - 0" Str. 299 906 9 16 5' - 9" Str. 313 907 9 8 8' - 6" Str. 231  101 11 34 12' - 0" Str. 231  102 11 20 19' - 0" 321 2,019 103 11 53 25' - 6" Str. 7,181 104 11 3 21' - 9" Str. 347 105 11 47 19' - 6" Str. 4,870								3,787
904 9 3 21° - 6° Str. 219 905 9 8 11° - 0° Str. 299 906 9 16 5° - 9° Str. 313 907 9 8 8° - 6° Str. 231  101 11 34 12° - 0° Str. 231  102 11 20 19° - 0° 321 2,019 103 11 53 25° - 6° Str. 7,181 104 11 3 21° - 9° Str. 347 105 11 47 19° - 6° Str. 4,870	***************************************		39	······································			<del>  </del>	
905       9       8       11' - 0"       Str.       299         906       9       16       5' - 9"       Str.       313         907       9       8       8' - 6"       Str.       231         101       11       34       12' - 0"       Str.       2.168         102       11       20       19' - 0"       \$21       2.019         103       11       53       25' - 6"       Str.       7.181         104       11       3       21' - 9"       Str.       347         105       11       47       19' - 6"       Str.       4,870			3			•	+	
907 9 8 8 8 - 6 Str. 231  101 11 34 12 - 0 Str. 2.168  102 11 20 19 - 0 321 2.019  103 11 53 25 - 6 Str. 7.181  104 11 3 21 - 9 Str. 347  105 11 47 19 - 6 Str. 4.870		9	8	11' - 0"	Str.	***		299
101     11     34     12' - 0"     Str.     2.168       102     11     20     19' - 0"     \$21     2.019       103     11     53     25' - 6"     Str.     7.181       104     11     3     21' - 9"     Str.     347       105     11     47     19' - 6"     Str.     4,870			<del></del>			<del></del>	1	
102     11     20     19' - 0"     \$21     2.019       103     11     53     25' - 6"     \$tr.     7.181       104     11     3     21' - 9"     \$tr.     347       105     11     47     19' - 6"     \$tr.     4,870	906	Ω	Ø	o' • B	JEF.			431
102     11     20     19" - 0"     \$21     2,019       103     11     53     25' - 6"     \$tr.     7,181       104     11     3     21' - 9"     \$tr.     347       105     11     47     19' - 6"     \$tr.     4,870	906	9						
104     11     3     21' - 9"     Str.     347       105     11     47     19' - 6"     Str.     4870	906 907		34	12" - 0"	Str.			2,168
105   1   47   19' - 6"   Str.   4,870	906 907 101 102	l i	20	19" - 0"	321			2,019
	906 907 101 102 103	11	20 53	19" - 0" 251 - 6"	\$21 Str.			2,019 7,181
	906 907 101 102 103 104		20 53 3	19' - 0" 25' - 6" 21' - 9" 19' - 6"	<b>321</b> Str. Str.			2,019 7,181 347
	906		20 53 3 47	19' - 0" 25' - 6" 21' - 9" 19' - 6"	\$21 Str. Str. Str.			2,019 7,181 347 4,870
	906 907 101 102 103 104 185		20 53 3 47	19' - 0" 25' - 6" 21' - 9" 19' - 6"	\$21 Str. Str. Str.			2,019 7,181 347 4,870
	906 907 101 102 103 104 185		20 53 3 47	19' - 0" 25' - 6" 21' - 9" 19' - 6"	\$21 Str. Str. Str.			2,019 7,181 347 4,870
	906 907 101 102 103 104 185		20 53 3 47	19' - 0" 25' - 6" 21' - 9" 19' - 6"	\$21 Str. Str. Str.			2,019 7,181 347 4,870
	906 907 101 102 103 104 185		20 53 3 47	19' - 0" 25' - 6" 21' - 9" 19' - 6"	\$21 Str. Str. Str.			2,019 7,181 347 4,870
	906 907 101 102 103 104 105		20 53 3 47	19' - 0" 25' - 6" 21' - 9" 19' - 6"	\$21 Str. Str. Str.			2,019 7,181 347 4,870

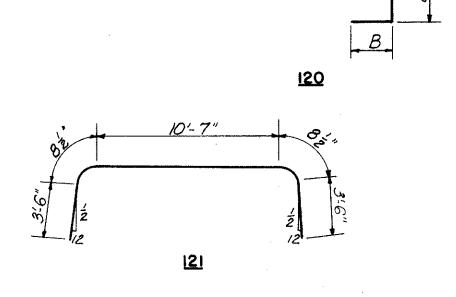
MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIO A	NS B	WEIGHT LBS.
			PIER S	SHAFT	7N		
401 402	4	718	3" - 3" 3" - 4"	100	1' 1i" 2' 0"		1,559
402	4	312	3 - 4	100	Z' + U'		695
501 502	5	28 28	17' - 11"	1.04	15" - 6"	2'- <b>5"</b> 2'- <b>5"</b>	523 5 <b>04</b>
503	5	28	16' - 6"	104	14" - 1"	2-5"	482
504	5	25	15' - 8"	104	13' - 3"	2-5"	409
505	5	28	14" - 10"	104	121 - 5"	2-5"	433
506	5	16	14' - 1"	1 04	11' - 8"	2'-5"	235
507 508	5	28	15° - 0"	Str.	·	-	438
509	5	28 28	14" - 3"	Str.			416 394
510	5	25	12" - 9"	Str.		<del>                                     </del>	332
511	5	28	121 - 0"	Str.			350
512	5	16	111 - 3"	Str.			188
513 514	5 5	6	7' - 9 "	104	5' - 4" 4' -   "	2 - 5"	48 56
<b>917</b>		<u> </u>	v - 11	120	7 -11	-	96
		<u></u>					
601	6	40	13' - 8"	104	11' - 2"	2"-6"	821
602	6	14	71 - 0"	Str.			147
603 604	6	40	6' - 0"	Str.		-	360 66
- VVT	0	7	11: <del>- V</del>	Jir.		+	00
					4"		
901	9	45	31' - 9"	Str.			4,858
902	9	3	28' - 6"	Str.			291
903 904	9	39	26' - 0" 20' - 9"	Str.		-	3,448
905	9	8	11' - 0"	Str.		-	70 299
906	9	16	5' - 9"	Str.			313
907	9	8	8' - 6"	Str.	-		231
1101							
1101	11	34	12' - 0"	Str.		1	2.168
1102 1103	11	20 53	19" - 0" 32" - 6"	121 Str.			2,019 9,152
1104	11	3	28' - 9"	Str.			458
105	11	47	28* - 3*	Str.			7,054
1106	11		23" - 3"	Str.			124
		<del>                                     </del>				1	
			PIER	SHAFT	7 S		
401	4	718	31 - 3"	100	11 - 11"		1 550
402	4	312	3' - 4"	100	2' - 0"		1,559 695
:							
501	5	28	17' - 11"	104	151 - 6*	2'-5"	<u>523</u>
502 503	5	28 28	17' - 3" 16' - 6"	104	14" - 10" 14" - 1"	2'-5" 2'-5"	504 482
504	5	25	15" 8"	104	13' - 3"	2'-5"	409
505	5	28	141 - 10"	104	12' - 5"	2'-5"	
506	5	16	141 - 17	1.04	111 - 8"	2'-5"	235
507	5	28	15' - 0"	Str.			438
508	5	28	14' - 3"	Str.		-	416
509 510	5	28 25	13' - 6" 12' - 9"	Str.	derman and a desired of the first of the fir		394 332
511	5	28	12' - 0"	Str.			350
512	5	16	111 - 3"	Str.			188
513	5	6	7" - 9 "	104	51 - 4"	2'-5"	48
514	5	6	8* - 11*	120	4, -1[,	P-11"	56
			THE RESERVE AND ADDRESS OF THE PROPERTY OF THE				
60 i	6	40	131 - 8"	1 04	11' - 2"	2 -6"	821
602	6	14	71 - 0"	Str.			147
603	6	40	6' - 0"	Str.			360
604	6	4	11' - 0"	Str.		-	66
	<del> </del>					<del>                                     </del>	
901	9	45	31' - 9"	Str.		<u> </u>	4,858
902	9	3	28" - 6"	Str.			291
903	9	39	26' - 0"	Str.		<del> </del>	3,448
904	9		201 - 9"	Str.		-	70
905 906	9	8	11' - 0" 5' - 9"	Str.			299
905	9	8	<u>5' - 9"</u> 8' - 6"	Str.	<u>.                                    </u>		313 231
JUI				J			431
1101	11	34	12' - 0"	Str.		-	2,168
1102	11	20	191 - 01	121	<u>, , , , , , , , , , , , , , , , , , , </u>	1	2,019
1103	11	53	32 * - 6 * 28 * - 9 *	Str.			9,152 458
1105		47	281 - 3"	Str.		1	7,054
	11	1	23' - 3"	Str.			124
1106							
1106		1		1	i		ı
1106						-	
1106							
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1106					1		
1106							

MARK	SIZE	NO.	LENGTH	TYPE	DIMENSION A	NS B	WEIGHT LBS.
		•	PIER	SHAFT	6N	**************************************	
401	ų,	718	3* - 3*	100	[1 -     "		1,559
402	4	312	3* - 4"	100	2' - 0"		695
501	5	28	18" - 1"	104		21-5"	528
502	5	28	17' - 4"	104	14" - 11"	21-5"	506
503 504	5	28 25	16* - 7" 15* - 9"	104	14" - 2"	21-5" 21-5"	484
505	5	28	15' - 0"	104	12' - 7"	2'-5"	438
506	5	16	14' - 2"	104	11' - 9"	21-5	236
5 <b>07</b> 508	<b>5</b>	28 28	15" - 0"	Str.			438 416
509	5	28	13' - 6"	Str.			394
510 511	5	25	12' - 9"	Str.			332
512	<u>5</u>	28 16	11' - 3"	Str.	.,		350 188
513	5	6	7' - 10"	104	5' - 5"	2'-5"	49
514	5	6	8' - IL"	120	41 - 11"	'-	5 <b>6</b>
601	6	40	13' - 8"	104	11' - 2"	2'-6"	821
602	6	14	71 - 0"	Str.			147
603	6	40	6' - 0"	Str.			360
604	6	4	11, - 0	Str.			66
901	9	45	31' - 9"	Str.			4.858
902	9	3	281 - 6"	Str.			291
903 904	9	39 I	27' - 0" 21' - 9"	Str.		<del>                                     </del>	3,5 <u>80</u> 74
905	9	8	11' - 0"	Str.			299
906	9	16	5' - 9" 8' - 6"	Str.			313
907	9	8	ð· - 6"	Str.			231
1101	11	34	12' - 0"	Str.			2,168
102	11	20	191 - 0"	121	- Markey (1997)		2,019
1103	11	53 3	32' - 6" 28' - 9"	Str.		<del>                                     </del>	9,152 458
105		47	29' - 3"	Str.			7,304
106	11	11_	241 - 3"	Str.			129
					<u>, , , , , , , , , , , , , , , , , , , </u>		· · ·
			PIER	SHAFT	6 <b>S</b>	•	
401 402	4	718 312	3! - 3" 3! - 4"	100	2' - 11"		1,559 695
402	1	312		100	2 - 0		095
501	5	28	18' - 1"	104	151 - 8"	245"	528
502	5	28	171 - 4"	104	14+ - 11"		506
503 504	5	28 25	161 - 7" 151 - 9"	104	14' - 2"	245	484 411
505	5	28	15' - 0"	104	12' - 7"	245"	411
506	5	16	14' - 2"	104	11' - 9"	2 - 5	236
<u>507</u> 508	5	28 28	151 - 0" 141 - 3"	Str. Str.		<del>  </del>	438 416
509	5	28	13' - 6"	Str.	-		394
510 511	5	25 28	12" - 9" 12" - 0"	Str. Str.			332
512	5	16	11' - 3"	Str.	nii anan. an. an. an. an. an. an. an. a		350 188
513	5	6	7" - 10"	104	5' - 5"	21-5	49
514	5	6	8" - 11"	120	4" -  { "	1-11.	56
	<u>L</u>			1		-	
601		πυ	131 - 2"	I Un	111 - 2*	216"	gήi
601 602	6	40 14	13" - 8" 7" - 0"	lo4 Str.	11* - 2*	216"	821 147
602 603	6	14 40	7' - 0" 6' - 0"	Str.	11* - 2*	216"	147 360
602	6	14	7' - 0"	Str.	11* - 2*	216"	147
602 603	6	14 40 4	7' - 0" 6' - 0" 11' - 0"	Str. Str. Str.	111 - 2"	216"	147 360
602 603 604 901 902	6 6 9 9	14 40 4 45 3	7! - 0" 6! - 0" 1!! - 0" 3!! - 9" 28! - 6"	Str. Str. Str. Str. Str.	11* - 2*	216"	147 360 66 4,858 291
602 603 604 901 902 903	6 6 9 9 9 9	14 40 4	7' - 0" 6' - 0" 11' - 0" 31' - 9" 28' - 6" 27' - 0"	Str. Str. Str. Str. Str. Str. Str.	11* - 2*	216"	147 360 66 4,858 291 3,580
602 603 604 901 902	6 6 6 9 9 9	14 40 45 3 39 1	7' - 0" 6' - 0" 11' - 0" 31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0"	Str. Str. Str. Str. Str. Str. Str. Str.	111 - 2	216"	147 360 66 4,858 291 3,580 74 299
901 902 903 904 905 906	9 9 9 9	14 40 4 45 3 39 1 8	7' - 0" 6' - 0" 11' - 0" 31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0"	Str. Str. Str. Str. Str. Str. Str. Str.	111 - 2	216"	147 360 66 4,858 291 3,580 74 299 313
901 902 903 904 905	6 6 6 9 9 9	14 40 45 3 39 1	7' - 0" 6' - 0" 11' - 0" 31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0"	Str. Str. Str. Str. Str. Str. Str. Str.	11* - 2*	216"	147 360 66 4,858 291 3,580 74 299
901 902 903 904 905 906	9 9 9 9	14 40 4 45 3 39 1 8	7' - 0" 6' - 0" 11' - 0" 31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0"	Str. Str. Str. Str. Str. Str. Str. Str.	11 - 2	216"	147 360 66 4,858 291 3,580 74 299 313
901 902 903 904 905 906 907	9 9 9 9 9 9	14 40 4 45 3 39 1 8 16 8	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"	Str. Str. Str. Str. Str. Str. Str. Str.	11* - 2*	216"	147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019
901 902 903 904 905 906 907	9 9 9 9 9 9	14 40 45 3 39 1 8 16 8 34 20 53	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"	Str. Str. Str. Str. Str. Str. Str. Str.		216"	147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152
901 902 903 904 905 906 907 1101 1102 1103 1104	9 9 9 9 9 9	14 40 4 45 3 39 1 8 16 8	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 29' - 3"	Str. Str. Str. Str. Str. Str. Str. Str.		216"	147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152 458 7,304
901 902 903 904 905 906 907 1101 1102 1103	9 9 9 9 9 9	14 40 45 3 39 1 8 16 8 34 20 53 3	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 28' - 6" 28' - 9"	Str. Str. Str. Str. Str. Str. Str. Str.		216"	147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152 458
901 902 903 904 905 906 907 1101 1102 1103 1104	9 9 9 9 9 9	14 40 45 3 39 1 8 16 8 34 20 53 3	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 29' - 3"	Str. Str. Str. Str. Str. Str. Str. Str.		216"	147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152 458 7,304
901 901 902 903 904 905 906 907 1101 1102 1104 1105	9 9 9 9 9 9	14 40 45 3 39 1 8 16 8 34 20 53 3	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 29' - 3"	Str. Str. Str. Str. Str. Str. Str. Str.			147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152 458 7,304
901 901 902 903 904 905 906 907 1101 1102 1104 1105	9 9 9 9 9 9	14 40 45 3 39 1 8 16 8 34 20 53 3	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 29' - 3"	Str. Str. Str. Str. Str. Str. Str. Str.		216"	147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152 458 7,304
901 902 903 904 905 906 907 1101 1102 1103 1104	9 9 9 9 9 9	14 40 45 3 39 1 8 16 8 34 20 53 3	7' - 0" 6' - 0" 11' - 0"  31' - 9" 28' - 6" 27' - 0" 21' - 9" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 29' - 3"	Str. Str. Str. Str. Str. Str. Str. Str.			147 360 66 4,858 291 3,580 74 299 313 231 2,168 2,019 9,152 458 7,304

FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	30
•	ОНЮ	UI 1057 (4)		43

CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT
CUY - 42 R - 17. 50





BENDING DIAGRAM

PART 2

U. S. ROUTE 42 RELOCATION
INNER BELT FREEWAY - CENTRAL VIADUCT

REINFORCEMENT SCHEDULE

CLEVELAND CUYAHOGA COUNTY

SCALE NO SCALE

MADE D. E. E. DATE 3-9-54

TRCD ELS: DATE 6-1-54

CKD JGS. DATE 6-23-54

KANSAS CITY

HOWARD, NEEDLES, TAMMEN & BERGENDOFF

CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK

914-1A SHEET- 1.30

and the same

MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIONS A B	WEIGHT LBS.	MARK	SIZE	NO.	LENGTH	TYPE	DIMENSION A	IS B	WEIGHT LBS.
			PIER S	HAFT	1 N					PIER S	HAFT	2N		,
401 402	ц Ц	489 208	3" - 4"	100	1! - 11" 2! - 0"	1,062 463	401 402	4	702 304	3" - 3" 3" - 4"	100	11 - 11" 21 - 0"		1.529 677
501		20	16' - 7"	100	14' 2" 2'-5		501	-	20	17' - 11"	Lou	15' - 6"	2'-5"	500
501 502	5 5	28 28	15' - 11"	104	14' - 2" 2'-5 13' - 6" 2'-5		501 502	5 5	28 28	17' - 2"	104		2'-5"	523 <b>50</b>
503	5	24	15" - 1"	104	12' - 8" 2'-5		503	5	28	16' - 5"	104	14' - 0"	2'-5"	*480
504 51 <i>3</i>	5 5	20 8	14" - 4" 7" - 4"	104	111 - 11" 21-5		504 505	5	25 28	15" - 8"	104		2'-5"	40! 430
506	5	28	13' - 6"	Str.		394	506	5	12	14* - 0*	104		2-5	17
507	5	28	121 - 9"	Str.		372	507	5	28	15' - 0"	Str.			438
508 509	5 5	24 20	12" - 0"	Str.		300 235	508 509	5	28 28	14" - 3"	Str.			416 391
14	5	8	8' - 5 "	120	4" - 5" 13- 1	***************************************	510	5	25	12' - 6"	Str.			326
							511	5 5	28	11' - 9"	Str.			343
601	6	40	131 - 8"	104	11' - 2" 25-6	821	513	5	6	7' - 9"	104	5" - 4"	2'-5"	138 48
502	6	14	7' - 0"	Str.		147	514	5	6	8" - 9"	120	41 - 9"	17-11	55
603 604	6	40	61 - 0"	Str.		360 66								
<b>FU</b>				00.			601	6	40	131 - 8"	104	11' - 2"	2'-6"	821
							602	6	14	7' - 0"	Str.			147
001	9	45	24' - 9"	Str.		2 707	603 604	6	40	6' - 0"      0"	Str.			360 66
901	9	39	15" - 6"	Str.	,	3,787 2,055	804	0	<u> </u>	11 0	JLT.			
03	9		10' - 3"	Str.		35			41.5					
904 905	9	3 8	21' - 6" 11' - 0"	Str.		219	901	9	45	31' - 9" 28' - 6"	Str.			4,8 <b>5</b> 8
06	9	16	5' - 9"	Str.		313	903	9	39	25* - 0*	Str.			3,315
907	9	8	8' - 6"	Str.		231	904	9	8	19' - 9"	Str.			67
			<u> </u>	<del> </del>	:		905 906	9	16	5' - 9"	Str.			299 313
							907	9	8	8' - 6"	Str.			23
01	11	34 20	12" - 0" 19" - 0"	Str.		2,168								
02	11	53	25' - 6"	Str.		7,181	1101	11	34	12" - 0"	Str.			2,168
04	11	3	21' - 9"	Str.		347	1102	11	20	19' - 0"	121			2.019
05	11	47	17" - 9" 12" - 9"	Str.		4,442	1103	11	53	32" - 6" 28" - 9"	Str.			9,152 458
06			12 3	, Str.		- 00	1105	11	47	27' - 3"	Str.			6,805
							1106	11		221 - 3"	Str.	, , , , , , , , , , , , , , , , , , , ,		118
						<u> </u>								
			<del></del>	SHAFT				·			HAFT		1 1	
101	4	489 208	3* - 3* 3* - 4*	100	2' - 0"	1,062	401	4	702 304	31 - 3" 31 - 4"	100	21 - 11"		1, <u>52</u> 67
501	.5	28	16" - 7"	104	14" - 2" 2'-5	4 484	501	.5	28	17" - 1 <u>[</u> "	104	15! - 64	2"-5"	52
02	5	28	15' - 11"	104	13' - 6" 2'-5	464	502	5	28	17' - 2"	104	14' - 9"	2'-5"	50
03	5	24	15" - 1"	104	12" - 8" 2"-5 11" - 11" 2-5		503 504	5 .5	28 25	161 - 5" 151 - 8"	104		2'-5" 2'-5"	48 40
13	5 5	8	71 - 4"	104	4' - 11" 2-5		505	5	28	141 - 11"	104		2'-5"	430
06	5	28	13' - 6"	.Str.		394	506	5	12	14" - 0"	104		24-5"	17
07 08	5 5	28	12" - 9"	Str.		372	507 508	<u>.5</u>	28 28	151 - 0"	Str.			438 416
09	.5	20	111 - 3"	Str.		235	509	5	28	13' - 6"	Str.			39
14	5	8	8' - 5"	120	4' - 5"  '-	71	510	5	25	12' - 6"	Str.			320
						-	511	5 5	28	11' - 9"	Str.			34: 131
01	6	40	13" - 8"	100	111 - 2 2 2 -6	821	513	5	6	7' - 9"	104	5' - 4"	2'-5'	48
02	6	14	7' - 0"	Str.		147	514	5	6	8* - 9*	120	4' - 9"	f M.	5!
03 04	6	40	6' - 0"	Str.		360 66						· · · · · · · · · · · · · · · · · · ·		
VT		7					601	6	40	131 - 8"	104	11' - 2"	2'-6"	
		,,	On the Car	84		2 70-	602	6	14	7' - 0"	Str.			147
01	9	45 39	24' - 9" 15' - 6"	Str.		3,787 2,055	603 604	6	40	11' - 0"	Str.			36
03	9	ī	10" - 3"	Str.		35								
04	9	3	21' - 6"	Str.		219					0.1	<b>MALORIE</b> 1000 1100 1100 1100 1100 1100 1100 11		
05 106	9	8 16	11' - 0"	Str.		299 313	901	9	45	31' - 9" 28' - 6"	Str.			4,85 29
07	9	8	8' - 6"	Str.		231	903	9	39	25' - 0"	Str.			3,31
			auto a versión de la companyo				904	9	1	19' - 9"	Str.			6
01	11	34	12" - 0"	Str.		2,168	905 906	9	8	11' - 0" 5' - 9"	Str.			29 31
02	11	20	19' - 0"	121		2,019	907	9	8	81 - 6"	Str.			23
03		53	25", - 6"	Str.		7,181	<u> </u>	ļ			<b> </b>			
04 05	11	3 47	21' - 9" 17' - 9"	Str.		4,442	1101	11	34	12* - 0*	Str.			2.16
06	11	1	12' - 9"	Str.		68	1102	11	20	19' - 0"	121			2,01
			ANA STATE OF THE S				1103	11	53	32" - 6" 28" - 9"	Str.			9,15 45
							1105	11	47	27° - 3 m	Str.			6,80
							1106	11	1	22" - 3"	Str.	.,		11
· · · · · · · · · · · · · · · · · · ·				<u> </u>		<u> </u>	<u> </u>				-			
	1	ı <b>I</b>		1		<u> </u>	<b>.</b>		1		<b> </b>		1	<u> </u>

MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIONS A	В	WEIGHT LBS.	MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIONS A B	WEIGI LBS
			PIER	SHAFT	3N					<u></u>	PIER S	HAFT	4N	
401 402	<b>4</b>	718 312	31 - 3"	100	1" - 11"		1,559 695	401 402	4	734 320	31 - 3" 31 - 4".	100	1" - 11"	1,5
- 402		3.2		100			035		<b>T</b>	320				
501	5	28	18" - 1"	104		'-5	528	501	5	28	18" - 2"	104	15' - 9" 2'-1	
502 503	.5 .5	28 28	161 - 7"	104	14" - 11" 2	-5	506 484	502 503	.5 .5	28 28	17! - 5* 16! - 7"	104	15' - 0" 2'-!	
504	5	25	15' - 9"	104	13' - 4" 2	-5"	411	504	5	25	15' - 10"	104	13' - 5" 2'-	," <b>4</b>
505 506	<u>5</u> 5	28 16	15" - 0" 14" - 2"	104		! -5" ! - 5"	438 236	505 506	5 5	28 20	15" - 0" 14" - 3"	104	12' - 7" 2'-!	
507	5	28	15' - C"	Str.			438	507	5	28	15' - 3"	Str.		4
508 509	. <u>5</u>	28 28	14" - 3"	Str.			416 394	508 509	.5	28 28	131 - 6"	Str.		3
510	5	25	12' - 9"	Str.			332	510	5	25	12! - 9"	Str.		3
511 512	<u>5</u> 5	28 16	12" - 0"	Str.	A14-47-14-4-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1		350 188	511 512	5 5	28 20	12' - 0"	Str.		3
513	5	6	7' - 10"	104		<b>L5"</b>	49	513	5	6	7' - 10"	104	5' - 5" 2'-9	
514	5	6	8' - 11"	120	4 - 11"	<u>-117</u>	56	514	5	6	8' - 11"	120	4 - 11" !!-	<u>r                                     </u>
C 0 1			101 01	1.00	111 08 0		001	601		" 0	101 08	1011	11' - 2" 2'-(	
601 602	6	40	13' - 8" 7' - 0"	104 Str.	11' - 2"  2	6"	821 147	601 602	6 6	40 14	13" - 8" 7" - 0"	104 Str.	111 - 2 2 - 6	) i
603	6	40	6' - 0"	Str.			360	603	6	40	6' - 0"	Str.		3
604	6	.4	111 - 0"	Str.			66	604	6	4	11' - 0"	Ştr.		
001		11.5	211 0#	242			II OE C	901	0	# 5	31' - 9"	Str.		H f
901	9	45 3	31' - 9" 28' - 6"	Str.			4,858 291	901	9	<b>45</b>	28' - 6"	Str.		4,8
903	9	39	26" - 6"	Str.			3,514	903	9	39	27' - 9"	Str.		3,6
904 905	9	8	21" - 3" 11" - 0"	Str.			72 299	904	9	8	22" - 9" 11" - 0"	Str.		
906	9	16	5' - 9"	Str.			313	906	9	16	.51 - 9"	Str.		
907	9	8	8' - 6"	Str.			231	907	9	8	8' - 6"	Str.		
1101	11	34	12" - 0"	Str.			2.168	1101	11	34	12" - 0"	Str.		2,1
1102	11	20	19' - 0"	121.			2.019	1102	11	20	19' - 0"	121.		2.0
1103	11	53	321 - 6"	Str.			9,152	1103	11	53	32" - 6"	Str.		9,1
1104	11	3 47	28" - 9" 28" - 9"	Str.			458 7,179	1104	11	47	28' - 9" 30' - 0"	Str.		7.4
1106		1	23' - 6"	Str.			125	1106	11	i	25' - 0"	Str.		
							,				<u> </u>			
		1	PIER	SHAFT	35						PIER	SHAFT	45	
401 402	4	718 312		100	2' - 0"		1,559 695	401 402		73 <b>4</b> 320	3' - 3" 3' - 4"	100	1' - 11"	1,5
501	5	28	18' - 1"	104	15' - 8" 2	<b>~5"</b>	528	501	.5	28	i8* - 2*	104	15' - 9" 2'-	
502 503	. <u>5</u>	28	171 - 4" 161 - 7"	104	141 - 117 2		506 484	502 503	<u>5</u>	28 28	17' - 5" 16' - 7"	104	15' - 0" 2'-!	." .
504	<u> </u>	28 25	15' - 9"	104		-5"	411	504	.5	25	15' - 10"	104	13" - 5" 2-	
505	5	28	15' - 0"	104	121 - 7" 2	<b>4.5</b> "	438	505	.5	28	15* - 0*	104	12' - 7" 2'-	
506 507	. <u>5</u>	16 28	14" - 2"	104 Str.	11' - 9" .2	2.45"	236 438	.506 .507	.5 .5	20 28	141 - 3"	Str.	11' - 10" 2-!	07 4
508	5	28											l I	
<i>509</i>	5 .5	1 20	141 - 3"	Str.			416	508	.5	28	14' - 3"	.Str.		i i
511		28 25	131 - 6"	Str.			3 94	508 509	.5 5	28	14" - 3" 13" - 6"	Str.		
,	5	25 28	13° - 6" 12° - 9" 12° - 0"	Str. Str.			394 332 350	508 509 510	.5 5 5	28 25 28	14' - 3" 13' - 6" 12' - 9" 12' - 0"	Str.		
512	5 5	25 28 16	13' - 6" 12' - 9" 12' - 0" 11' - 3"	Str. Str. Str.	51 - 54 2	N.S.	394 332 350 188	508 509 510 511 .512	5 5 5 5	28 25 28 20	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3"	.str. .str. .str.		-
,	5 5 5	25 28 16 6	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10"	Str. Str.	5' 5" 2 4' - 11" 1		394 332 350 188 49	508 509 510	.5 5 5	28 25 28	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10"	Str.	.5"5" 24: 4"11" (!-	
512 513	5 5 5	25 28 16 6	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10"	Str. Str. Str. Str.			394 332 350 188 49	508 509 510 511 .512	5 5 5 5 5	28 25 28 20 6	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10"	Str. Str. Str. 104	5' - 5" 24	
.512 513 514 601	5 5 5 5	25 28 16 6 6	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"	Str. Str. Str. 104 120	4" - 11"		394 332 350 188 49 56	508 509 510 511 .512 .513 514	5 5 5 5 5 5	28 25 28 20 6 6	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"	.str. .str. .str. .str. 104	5' - 5" 24	
512 513 514 601 602	5 5 5 5 6 6	25 28 16 6 6 40	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11" 13' - 8" 7' - 0"	Str. Str. Str. 104 120	4" - 11"	rll"	394 332 350 188 49 56 821	508 509 510 511 .512 .513 514 601 602	5 5 5 5 5 5 5	28 25 28 20 6 6 6 40	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11" 13' - 8" 7' - 0"	Str. Str. Str. 104 120 104 Str.	.5'5" 24! 4'11" 1'-	
.512 513 514 601	5 5 5 5 6 6	25 28 16 6 6	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11" 13' - 8" 7' - 0" 6' - 0"	Str. Str. Str. 104 120	4" - 11"	rll"	394 332 350 188 49 56	508 509 510 511 .512 .513 514	5 5 5 5 5 5	28 25 28 20 6 6	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"	.str. .str. .str. .str. 104	.5'5" 24! 4'11" 1'-	
512 513 514 601 602 603	5 5 5 5 6 6	25 28 16 6 6 40 14	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11" 13' - 8" 7' - 0" 6' - 0"	Str.   Str.   Str.   Str.	4" - 11"	rll"	394 332 350 188 49 56 821 147 360	508 509 510 511 .512 .513 514 601 602 603	.5 .5 .5 .5 .5 .5 .6 .6	28 25 28 20 6 6 6 40 14	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7" - 0" 6' - 0"	Str. Str. Str. 104 120 104 Str. Str.	.5'5" 24! 4'11" 1'-	
512 513 514 601 602 603 604	5 5 5 5 6 6 6 6	25 28 16 6 6 40 14 40	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11" 13' - 8" 7' - 0" 6' - 0" 11' - 0"	Str.   Str.   Str.   Str.	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66	508 509 510 511 .512 .513 514 601 602 603 604	.5 .5 .5 .5 .5 .5 .6 .6	28 25 28 20 6 6 6 40 14	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7" - 0" 6' - 0"	Str. Str. Str. 104 120 104 Str. Str.	.5'5" 24! 4'11" 1'-	3"
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512 513 514 601 602 603 604 901 902 903 904 905 906 907	5 5 5 5 6 6 6 6 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4,858 291 3,514 72 299 313 231	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907	5 5 5 5 5 5 5 6 6 6 6 6 9 .9 .9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 1 8 16 8	14' - 3"  13' - 6"  12' - 0"  11' - 3"  7' - 10"  8' - 11"  13' - 8"  7' - 0"  6' - 0"  11' - 0"  28' - 6"  27' - 3"  22' - 0"  11' - 0"  5' - 9"  8' - 6"	Str. Str. Str. 104 120 104 Str. Str. Str. Str. Str. Str. Str. Str.	11' 2" 2-9	4, 3, 2,
512 513 514 601 602 603 604 901 902 903 904 905 906 907	5 5 5 5 6 6 6 6 9 .9 .9 .9 .9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0"  28' - 6" 26' - 6" 21' - 3" 11' - 0"  5' - 9" 8' - 6"	Str.	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4.858 291 3,514 72 299 313 231	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102	5 5 5 5 5 5 5 6 6 6 6 6 9 .9 .9	28 25 28 20 6 6 40 14 40 45 .3 39 1 8 16 8	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 27' - 3" 22' - 0" 11' - 0" 5' - 9" 8' - 6"	Str. Str. Str. 104 120 104 Str. Str. Str. Str. Str. Str. Str. Str.	11' 2" 2-(	3, 1 3, 1 2, 2, 1
512 513 514 601 602 603 604 901 902 903 904 905 906 907	5 5 5 5 6 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8 34 20 53 3	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7" - 0" 6' - 0" 11' - 0"  28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28" - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4.858 291 3,514 72 299 313 231 2,168 2,019 9,152 458	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104	5 5 5 5 5 5 6 6 6 6 6 6 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 16 8 16 8	14' - 3"  13' - 6"  12' - 0"  11' - 3"  7' - 10"  8' - 11"  13' - 8"  7' - 0"  6' - 0"  11' - 0"  28' - 6"  22' - 0"  11' - 0"  5' - 9"  8' - 6"  12' - 0"  19' - 0"  28' - 6"  28' - 6"	Str.   Str.	11' - 2" 2-1	2, 2, 2,
512 513 514 601 602 603 604 901 902 903 904 905 906 907 1101 1102 1103 1104 1105	5 5 5 5 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 4 45 3 39 1 8 16 8	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 28' - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4,858 291 3,514 72 299 313 231 2,168 2,019 9,152 458 7,179	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104 .1105	5 5 5 5 5 5 6 6 6 6 6 9 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 39 1 8 16 8	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 27' - 3" 22' - 0" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 6" 28' - 9" 28' - 9"	Str.   Str.	5' - 5" 24! 4' - 11" !-	2, 2, 2,
512 513 514 601 602 603 604 901 902 903 904 905 906 907	5 5 5 5 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8 34 20 53 3	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7" - 0" 6' - 0" 11' - 0"  28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28" - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4.858 291 3,514 72 299 313 231 2,168 2,019 9,152 458	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104	5 5 5 5 5 5 6 6 6 6 6 6 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 16 8 16 8	14' - 3"  13' - 6"  12' - 0"  11' - 3"  7' - 10"  8' - 11"  13' - 8"  7' - 0"  6' - 0"  11' - 0"  28' - 6"  22' - 0"  11' - 0"  5' - 9"  8' - 6"  12' - 0"  19' - 0"  28' - 6"  28' - 6"	Str.   Str.	5' - 5" 24! 4' - 11" !-	
512 513 514 601 602 603 604 901 902 903 904 905 906 907 1101 1102 1103 1104 1105	5 5 5 5 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8 34 20 53 3	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 28' - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4,858 291 3,514 72 299 313 231 2,168 2,019 9,152 458 7,179	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104 .1105	5 5 5 5 5 5 6 6 6 6 6 9 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 16 8 16 8	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 27' - 3" 22' - 0" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 6" 28' - 9" 28' - 9"	Str.   Str.	5' - 5" 24! 4' - 11" !-	3, 6 3, 6 2, 1 2, 6 9, 1
512 513 514 601 602 603 604 901 902 903 904 905 906 907 1101 1102 1103 1104 1105	5 5 5 5 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8 34 20 53 3	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 28' - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4,858 291 3,514 72 299 313 231 2,168 2,019 9,152 458 7,179	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104 .1105	5 5 5 5 5 5 6 6 6 6 6 9 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 16 8 16 8	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 27' - 3" 22' - 0" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 6" 28' - 9" 28' - 9"	Str.   Str.	5' - 5" 24! 4' - 11" !-	3, 6 3, 6 2, 1 2, 6 9, 1
512 513 514 601 602 603 604 901 902 903 904 905 906 907	5 5 5 5 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8 34 20 53 3	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 28' - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4,858 291 3,514 72 299 313 231 2,168 2,019 9,152 458 7,179	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104 .1105	5 5 5 5 5 5 6 6 6 6 6 9 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 16 8 16 8	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 27' - 3" 22' - 0" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 6" 28' - 9" 28' - 9"	Str.   Str.	5' - 5" 24! 4' - 11" !-	3, 6 3, 6 2, 1 2, 6 9, 1
512 513 514 601 602 603 604 901 902 903 904 905 906 907	5 5 5 5 6 6 6 6 9 9 9 9 9 9	25 28 16 6 6 40 14 40 45 3 39 1 8 16 8 34 20 53 3	13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 26' - 6" 21' - 3" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 9" 28' - 9"	Str.   Str.   Str.   IO4   I20   IO4   Str.   Str	4" - 11"	rll"	394 332 350 188 49 56 821 147 360 66 4,858 291 3,514 72 299 313 231 2,168 2,019 9,152 458 7,179	508 509 510 511 .512 .513 514 601 602 603 604 .901 902 903 904 .905 906 907 .1101 .1102 .1103 .1104 .1105	5 5 5 5 5 5 6 6 6 6 6 9 9 9 9 9	28 25 28 20 6 6 6 40 14 40 45 3 3 9 16 8 16 8	14' - 3" 13' - 6" 12' - 9" 12' - 0" 11' - 3" 7' - 10" 8' - 11"  13' - 8" 7' - 0" 6' - 0" 11' - 0" 28' - 6" 27' - 3" 22' - 0" 11' - 0" 5' - 9" 8' - 6"  12' - 0" 19' - 0" 32' - 6" 28' - 6" 28' - 9" 28' - 9"	Str.   Str.	5' - 5" 24! 4' - 11" !-	2, 2, 2,

DIMENSIO	NS B	WEIGHT LBS.	MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIONS A	B WEIGHT
4N	•				<u></u>	PIER S	HAFT	5N	
1' - 11'		1,594	401	4	766	3' - 3"	100	[" - [["	1,663
2" - 0"		713	402	4	336	3' - 4"	100	2' - 0"	748
151 - 9"	2'-5"	531	501.	5	28	181 4"	104	15* - 11" 2	535
15' - 0"	2'-5"	509	.502	5	28	17" 7"	104	15' - 2" 2	·-5" 513
14' - 2"	2' 5"	413	503 504	5 5	28 25	16" - 9" 16" - 0"	104		'-5" 489 '-5" 417
12' - 7"	2'-5"	438	505	5	28	15' - 2"	104	12' - 9" 2	'-5" 443
11' - 10'	2'-5"	297 445	<u>506</u> 507	<u>5</u> 5	28 28	15" - 5"	104 Str.	12" - 0" 2	'-5" 421 445
		416	508	5	28	14" - 6"	Str.		423
		394 332	509 510	5	28 25	13' - 9" 13' - 0"	Str.		402 339
		350	511	5	28	121 - 3"	Str.		358
51 - 5"	2'-5"	235 49	.512 513	5 5	28 6	7' - 11"	Str. 104	5' - 6" 2	336 -5" 50
4' - 11'		56	514	5	6	8' - 11'	120		211 56
<del> </del>									
111 - 2"	2'-6"	821	601	6	40	13' - 8"	104	11' - 2" 2	'-6" 82 i
		147 360	602 603	6	14	7' - 0" 6' - 0"	Str.	·	147 360
		66	604	6	4	11' - 0"	Str.		66
	-					, 1800 and 1			
		4,858	901	9	45	31' - 9"	Str.		4,858
to the state of th	-	29i 3,680	902	9	3 39	28" - 6" 29" - 9"	Str.		291 3,945
		77	904	9	ı	24' - 9"	Str.		84 299
		299 313	905 906	9	8 16	5' - 9"	Str.		313
		231	907	9	8	8' - 6"	Str.		231
		2,168	1101	11	34 .20	12" - 0"	Str.		2,168
		2,019 9,152	1103	11	53	32' - 6"	Str.		2,019 9,152
		458	1104	11	3	28' - 9"	Str.		458
		7.491 133	1105	11	47	32' - 3" 27' - 3"	Str.		8.053 145
								* `	
					<u> </u>	0.50			
45							HAFT	55	1.000
2" - 0"	<b>'</b>	713	401	4	766 336	31 - 3" 31 - 4"	100	2* - 0"	1,663
15' - 9"	2'-5"	.531	501	5	28	184 4"	104	15' - 11" 2	
15" - 0"	2-5" 2-5"	509 484	502 503	5 5	28 28	17' - 7"	104		'-5" 513 '-5" 489
1315"	2-5"	413	504	5	25	16' - 0"	104	13' - 7" 2	-5" 417
12' - 7"	2'-5"	438 297	505 506	.5 5	28 28	(5' - 2"  4' - 5"	104	1 1	2-5" 443 2-5" 421
	7	445	507	.5	28	151 - 3"	Str.		445
		394	508 509	.5 .5	28 28	14" - 6" 13" - 9"	Str.		423 402
		332	510	5	25	13" - 0"	Str.		339
	1	_350 _235	511	5 5	28 28	12" 3"	Str.		358 336
5'5"		49	.513	5	6	7" 11"	104		?-5 <b>"</b> 50
41 11	1-15	56	514	5	6	81 - 11"	120	4'-!!"	56
111 2*	2-6"	921	601	6	40	131 - 8"	1.04	11' - 2" 2	r-6" 821
11. 2	2-0"	.821 147	602	6	14	71 - 0"	Str.	2	147
		360 66	603 604	6	40	6"0"      0"	Str.		360
		30			7	v			
		4,858	901	9	45	31, - 8,	Str.		4,858
		291	902	9	3	281 - 6"	Str.		291
		3,613 75	903 904	9	39	29" - 9" 24" - 9"	Str.		3,945 84
	1	299	905	9	8	11' - 0"	Str.		299 313
		313 231	906 907	9	8	8' - 6"	Str.		231
	1		1101	11	34	12' - 0"	Str.		2,168
		2,168	<b></b>	1		4			
		2,019	1102	11	20 .53	19" - 0"	Str.		2,019
		2,019 9,152 458	1102 1103 1104	11	53 3	32' - 6" 28' - 9"	Str.		2,019 9,152 458
		2,019 9,152 458 7,429	1102 1103 1104 1105	11	53	32' - 6"	Str. Str. Str.		2,019 9,152
		2,019 9,152 458	1102 1103 1104	11	53 3	32' - 6" 28' - 9" 32' - 3"	Str.		2,019 9,152 458 8,053
		2,019 9,152 458 7,429	1102 1103 1104 1105	11	53 3	32' - 6" 28' - 9" 32' - 3"	Str. Str. Str.		2,019 9,152 458 8,053
		2,019 9,152 458 7,429	1102 1103 1104 1105	11	53 3	32' - 6" 28' - 9" 32' - 3"	Str. Str. Str.		2,019 9,152 458 8,053
		2,019 9,152 458 7,429	1102 1103 1104 1105	11	53 3	32' - 6" 28' - 9" 32' - 3"	Str. Str. Str.		2,019 9,152 458 8,053
		2,019 9,152 458 7,429	1102 1103 1104 1105	11	53 3	32' - 6" 28' - 9" 32' - 3"	Str. Str. Str.		2,019 9,152 458 8,053

	FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	31	
·	2	оню	UI 1057 (4)		43	
	~	O YTK	OGA COUNTY OF CLEVELAN BELT FREEV	ID	· .	
		CENTR	AL VIADUC -42R-17.50	Г	4	

100

120

104

BENDING DIAGRAM

PART 2 U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

REINFORCEMENT SCHEDULE

CUYAHOGA COUNTY CLEVELAND

SCALE No Scale
MADE R K DATE 3-9-54 HOWARD, NEEDLES, TAMMEN & BERGENDOFF TRCD E.S. DATE 6-1-54 CKD J.G.S. DATE 6:23:54

KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET- 1.31

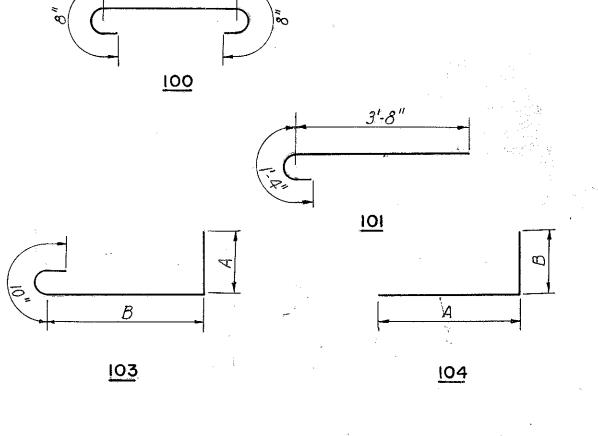
FEB 85 1987

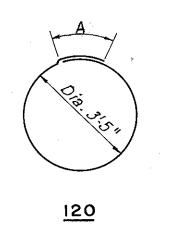
				<u> </u>				_ i			i		· · · · · · · · · · · · · · · · · · ·			· ·			1	- Distance	VO 1
MARK SIZE NO.	LENGTH	TYPE	DIMENSIONS WEIGHT A B LBS.	MARK SI	ZE NO.	LENGTH	TYPE	DIMENSION A	NS WEIGHT B LBS.		SIZE NO	LENG	гн тү	PE DIMENS	IONS WEIGHT B LBS.	MARK	SIZE NO	LENGTH	TYPE	DIMENSIO A	NS WEIGHT B LBS.
WES	ST END PI	R FOO	TING WN		WES	T END PIE	ER FOO	OTING W	S		Ε	AST END	PIER	FOOTING	EN		E	AST END	PIER F	OOTING E	S
601 6 29	23'-6"	Str.	1024		6 29	23'-6"	Str.		1024	601 602	6 2 6 2	9 23'-6 5 27'-6	й <b>51</b>	r.	1024	601	6 3	3 237-6"	Str.		1165
602 6 25	27'-6"	Str.	1033		6 25	27'-6"	Str.				8 6			r.	999	801 802			Str.		999 668
801 8 68 802 8 50	5'-6" 5'-0"	Str.	999 668		8 50	5'-6" 5'-0"	Str.	-	999 668		<del>                                     </del>			) i	668			-			
																1001	10 3	6 31'-6"	Str.		4880
				-																	
		Augustina de la companio del companio de la companio del companio de la companio del la companio de la companio																			
	WEST END	PIER S	SHAFT		٧	WEST END	PIER	SHAFT			. —	EAST.	END PI	ER SHAFT				EAST E	ND PIER	SHAFT	
401 4 280	21.3"	100	2'-11" 795	401	4 126	ુμ*-3"	100	2!+11"	358 234	401 402		8 41-3 4 31-3		00 2'-11" 00 1'-11"		401	4 37 4 32	8 <u>4!-3"</u> 4 3!-3"	100	2'-11"	1073 703
402         4         240           403         4         80	3'-2" 4'-9"	100	1'-11" 508 3'-5" 254	402 403	4 108 4 36	31-3" 4129"	100	3'-5"	114	403	4 10	8 46	9" 11	00 3'-5"	343	403	4 10	8 4'-9"	100	3'-5"	343
404 4 80 405 4 4	3'-7" 5'-3"	100 Str.	21-3" 192	404 405	4 36 4 4	3'-7" 5'-3"	100 Str.	21-3"	86			8 3!-7 4 5'-3		00 2!-3" tr.	259 14		4 10 4	8 3'-7" 4 5'-3"	100 Str.	<del></del>	259 14
									366										Str.		1141
501 5 40 502 5 40	121-9"	103	818 ['~5" 532	501	5 18 5 18	19!-6"	Str. 103	11-5"	239	502	5 5	4 131-6	6" I	tr. 03 2'-2"	760	501 502	5 5	4 137-6"	103	21-2"	760
503 5 40 504 5 4	15'-7"	105 1'	7-5"&2!-1"  2'-1"   650 	503 504	5 4	15!-7" 12!-8"		1!-5"&Z!-1"	2'-  " 293   1'-  " 53		5 5 5			05 2'-2"&2'- 04   11'-9"	5"   12±1" 939   1±9" 56	503 504		4 16%-8" 4 13'-6"	105 104	2'-2"&2'-5"	1211" 939 129?" 56
505 5 4	15'-0"	105 1	'-1"&2'-1"   11 <u>-10" 63</u>	505	5 4	15'-0"	105 I	11-1"&21-1"	11-10" 63	505	5	4 16'-0	)" [(	05 11-9"&2"-		505 506	5	4 16'-0" 2 15'-0"	105 Str.	1'-9"&2'-5"	II'-10" 67 31
506         5         2           507         5         2	15'-0" 17'-0"	Str.	31	506 507	5 2 5 2	15!-0" 17!-0"	Str.		31 35	507		2 17'-0	)" 5	tr.	35	507	5	2 17'-0"	Str.		35
508 5 8 509 5 8	16!-6" 15!-9"	Str.	138	508 509	5 9 5 18	151-6"  41-3"	Str.		145 268	<del></del>	5	7   17'-3 7   16'-6		tr.	126	508 509	<del> </del>	7 17'-3" 7 16'-6"	Str.		126
5 4	15'-6"	Str.	65	510	5 9	171-6"	Str.		164	510	5	7 16'-0	)" 51	tr.	117	510	5	7 16'-0"	Str.		117
511 5 8 512 5 8	18'-6" 17'-9"	Str.	154		6 50	4!-6"	str.		338		5 5	7 19!-3	3" S1	tr.	97	511 512	5	6 15'-6" 7 19'-3"	Str.		141
513 5 4 514 5 16	17"-6" 15!-0"	Str.	73 250	602	6 11	17'-6" 19'-6"	105		15'-0" 289 17-0" 264		5				135	513 514	<del>                                     </del>	7 18'-6" 7 18'-0"	Str.		135
515 5 16	14'-3"	Str.	238	604	6 2	141-6"	105	11-3"	12-0" 44	515	5	6 171-6	5" 5	tr.	110 266	515 516	5	6 17'-6" 4 18'-3"	Str.		110 266
516 5 8	14'-0"	Str.	1168	605 606	6 13 6 2	25'+0" 9!-9"	105	8'-6"	22'-6" 488   1-13" 29	517	5 1	4 171-9	3" S	tr.	259	517	5 i	4 17'-9"	Str.		259
601 6 50 602 6 11	4'-6" 17'-6"	Str. 105	338 1'-3"   15'-0" 289	607 608	6 2 6 1	11'-9"			123" 35 123" 15					tr.	256 207		5 I	<del></del>	Str.		256 207
603 6 9	19'-6"	105	17-3" 17-0" 264	609	6 1	121-1"	104	10'-10"	1-3" 18 1-3" 27								6 4		Str.		433
604 6 2 605 6 13	14'-6" 25'-0"	105	1'-3"   12'-0"   44 1'-3"   22'-6"   488	610	6 4	121-6"	104	111-3"	113" 38	602	6 I	1 19'-0	)" [(	tr. 05 2'-0"	433 15'-0" 314	602	6 1	1 - 19'=0."	105	2 0"	1540" 314
506 6 2	9'-9"	104	8'-6"   1±3"   29 10'-6"   1±3"   35	612	6 2 6 8	71-6"	104 Str.	10'-5"	1±3" 35 90		6			05 2'-0" 05 2'-0"	17'-0" 284 12'-0" 48	603 604	6	9 21'-0" 2 16'+0"	105	1	17 <sup>4</sup> 0" 284 12 <sup>4</sup> 0" 48
507 6 2 508 6 1	10'-1"	104	8'-10"   143"   15	614	6 6	91-6"	Str.	18 100	86	605	<del> </del>	3 261-6	5" 4 10	05 2'-0" 05 2'-0"	22'-6" 517 8±5" 38	605 606			105	2'-0"	22'-6" 517 845" 38
509 6 I 510 6 4	12'-1"	104	10'-10"   1±3"   18 3'-3"   1±3"   27		6 6	12'-0" 6'-3"	120 Str.	. l'−3"	108		7 - 6			05 21-0"	10'-5" 44	607		2 14'-5"	105	2'-0"	10-5" 44
6 2	12'-6"	104	11'-3" 113" 38			17'-0"			3087	608	6	1 12!-8		05 2'-0" 05 2'-0"	818" 19 10'-8" 22	608 609		1 12'-8"	105	<del></del>	818" 19 1018" 22
612     6     2       613     6     8	7'-6"	Str.	10'-5" 1+3" 35	802	8 68 8 50	13'-3"	Str.		1769	610	6	4 71-5	5" 10	05 2'-0"	315" 45	610	6	4 7'-5"	105	2'-0"	315" 45
14 6 6 15 6 6	91-6"	Str. 120	1'-3" 86 1'-3" 108		8 9 8 2	21!-3" 8!-0"	Str.		511 43	612	6	2	;" <u> </u>	05 2'-0" 05 2'-0"	11'-3" 46 10'-5" 44		6				10'-5" 44
16 6 24		Str.	225	805	8 2 8 1	101-9" 71-9"	Str.		57 21	613	6		3 tr S1	ir.	90	613 614	6	8 7'-6" 6 8'-6"	Str.		90
01 8 186	171-3"	Str.	8567	807	8 1	10!-6"	Str.		28	615	6	6 121-9	9" 13	20 2'- 0"	115	615	6	6 12"-9"	120	2'-0"	115
02 8 50 03 8 9	13!-3" 21!-3"	Str.	1769 511		8 73	51-0"	Str.		975	617				tr. 08	225 18		6 2		Str.   108		18
04 8 2 05 8 2	8'-0" 10'-9"	Str.	43 57	1101	11 23 11 2	15'-6"	Str.		1894		8 11	8 20'-0	)" S1	kr.	6301	801	8 11	8 20'-0"	Str.		6301
06 8 1	7'-9"	Str.	21	1103	11 2	3'-6"	Str.		37	802	8 6	8 24'-9	3" S1	tr.	4494 541		8 6	8 241-9"	Str.		4494 541
07 8 I 08 8 73	10'-6"	Str.	28 975	1104	11 1	9'-6" 3'-0"	Str.		50 16		8	2 8'-9	3" S1	tr.	47	804	8	2 8'-9"	Str.		47
	151-6"	Str.	1894							805 806			)" S1	r.	57 23	805 806			Str.		57 23
01 11 23	10'-0"	Str.	- 106							807	8	1 101-6	5" S1	ir.	28 921	807	8 8	1 10'-6"	Str.		28 921
03   1	3'-6" 9'-6"	Str.	37 50							808											
05 11 1	31-0"	Str.	16					· · · · · · · · · · · · · · · · · · ·			11 2			tr.	1864		11 2		Str.		1864 106
										1103	11	2 31-9	)" St	r.	40	1103	11	2 3'-9"	Str.		40
										1104				r.	50 19	1104	11	1 9'-6" 1 3'-6"	Str.		50 19
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FED. ROAD DIV. NO. STATE FEDERAL AID PROJECT NO. 
 32

 43
 UI 1057 (4)

CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT
CUY - 42 R - 17.50





105

BENDING DIAGRAM

PART 2

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

REINFORCEMENT SCHEDULE

CLEVELAND scale No scale

CUYAHOGA COUNTY

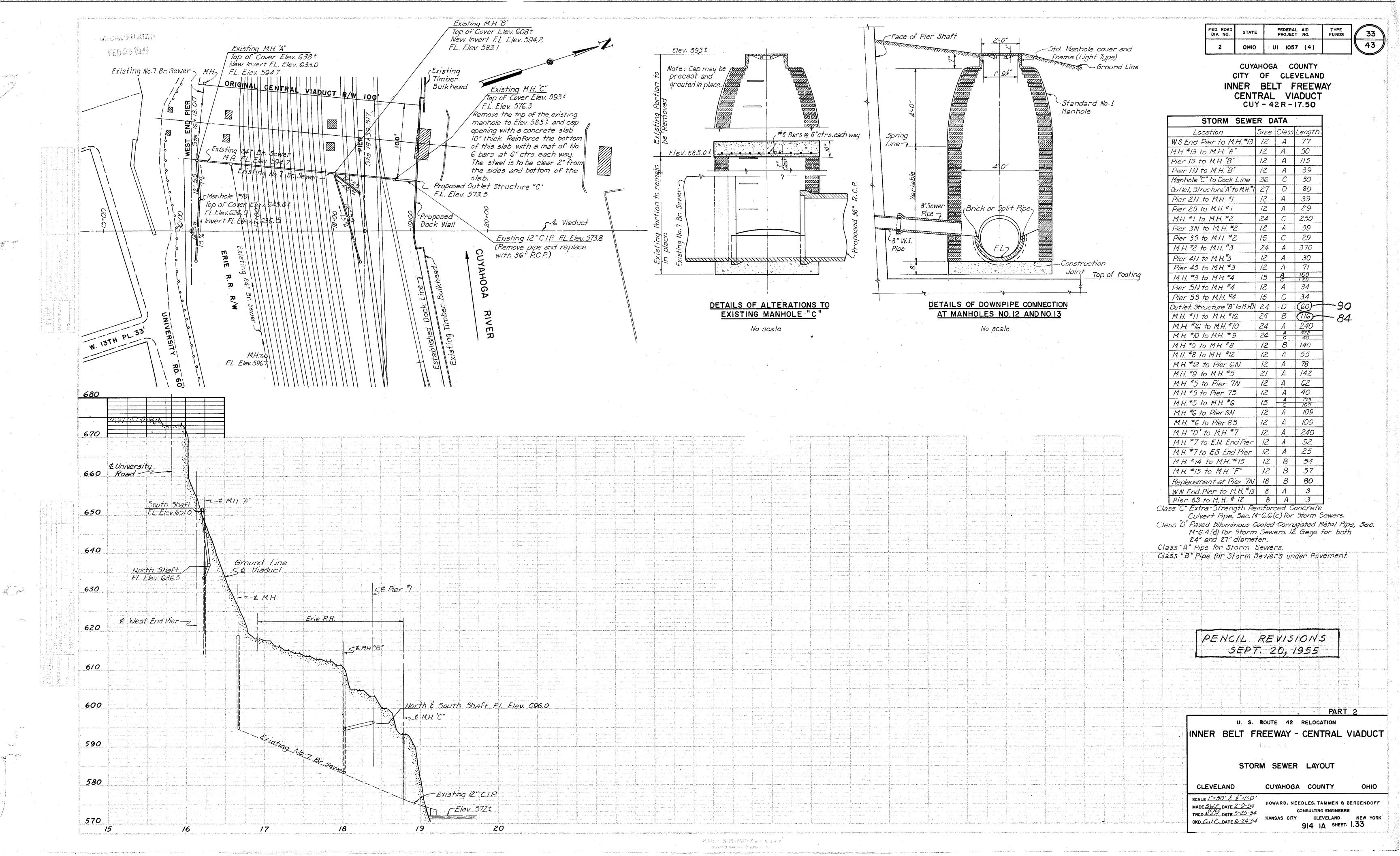
HOWARD, NEEDLES, TOWNSON, NEW YORK

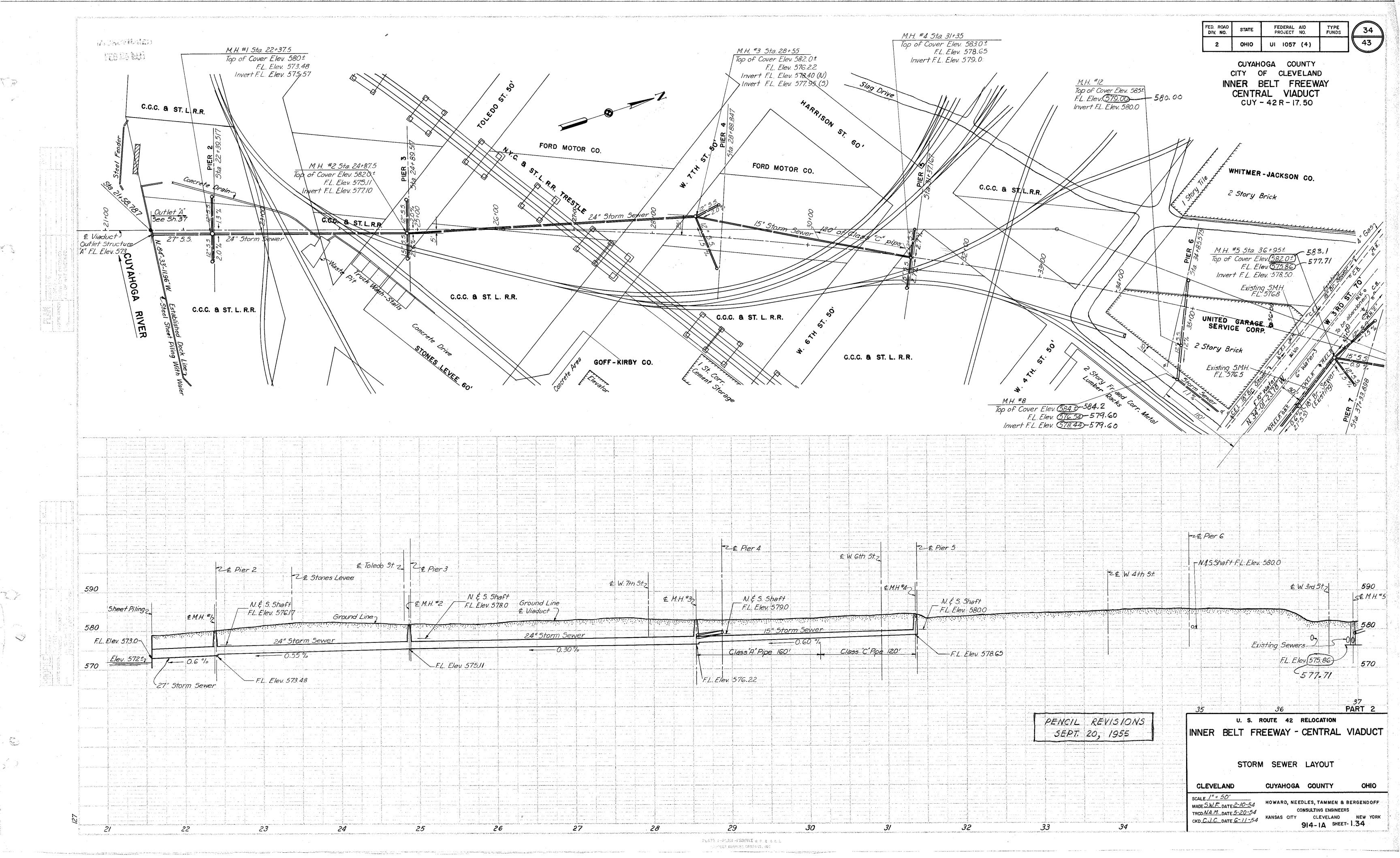
TRCDLCM DATE 8-24-54

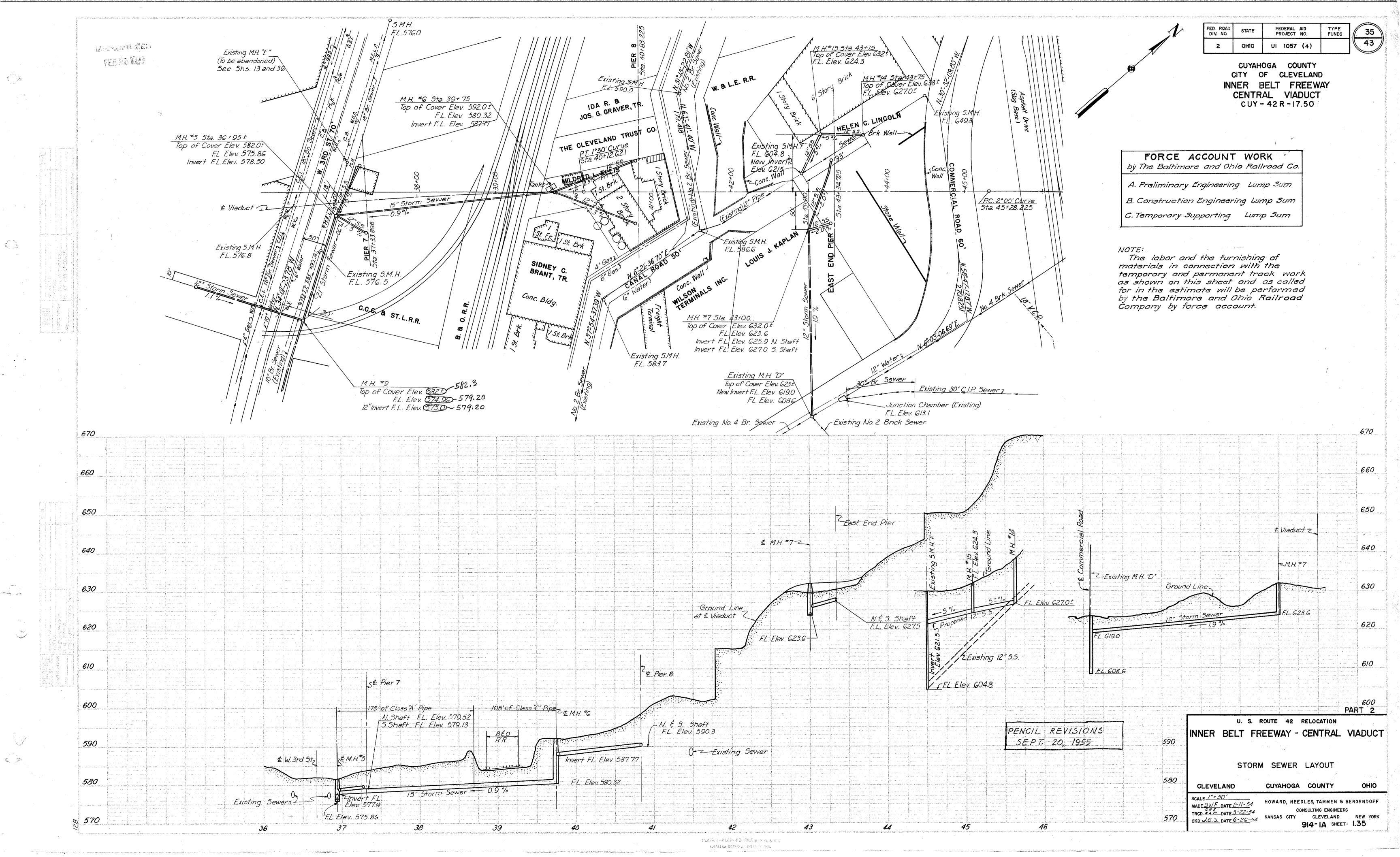
CKD.JGS DATE 8-24-54

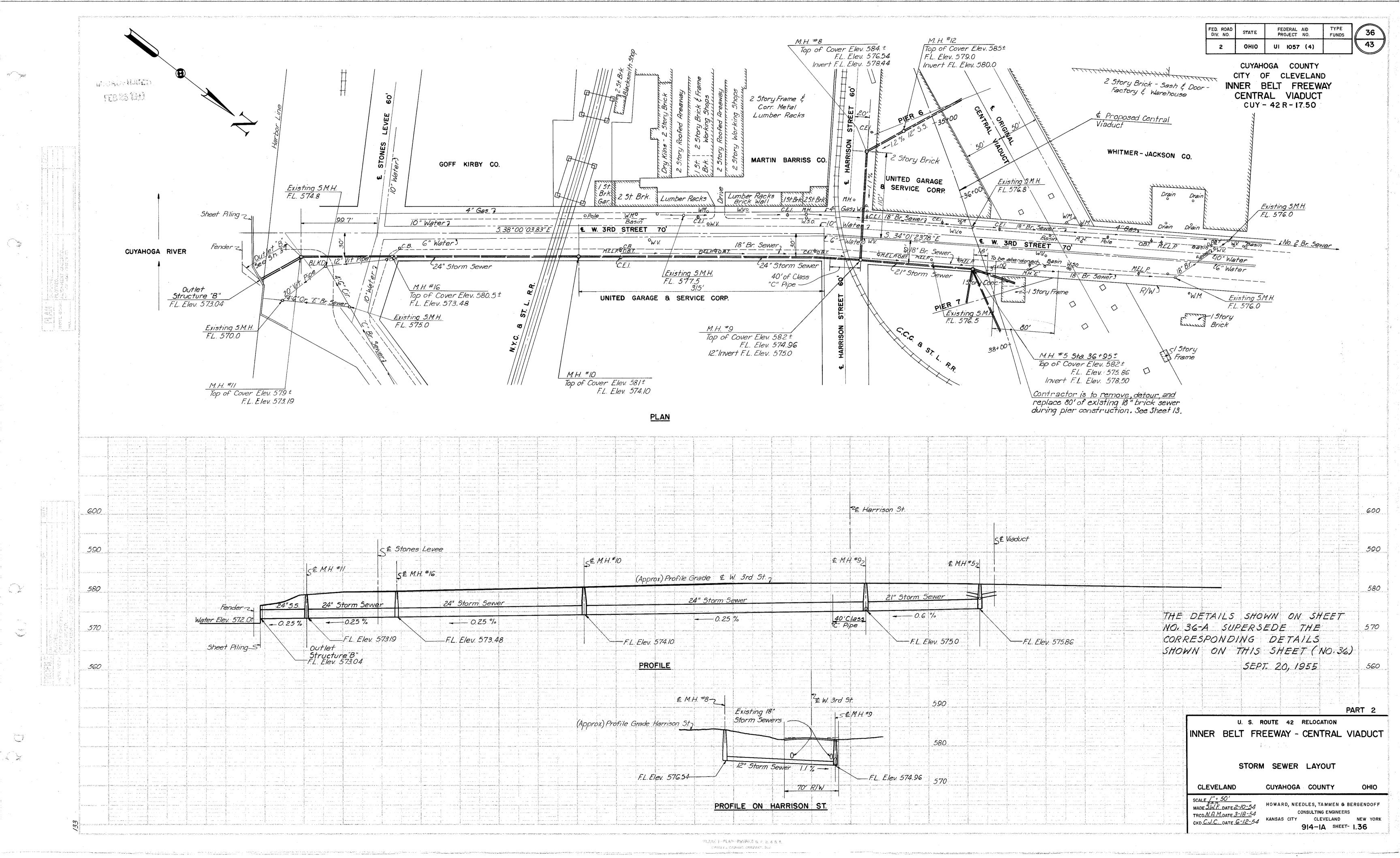
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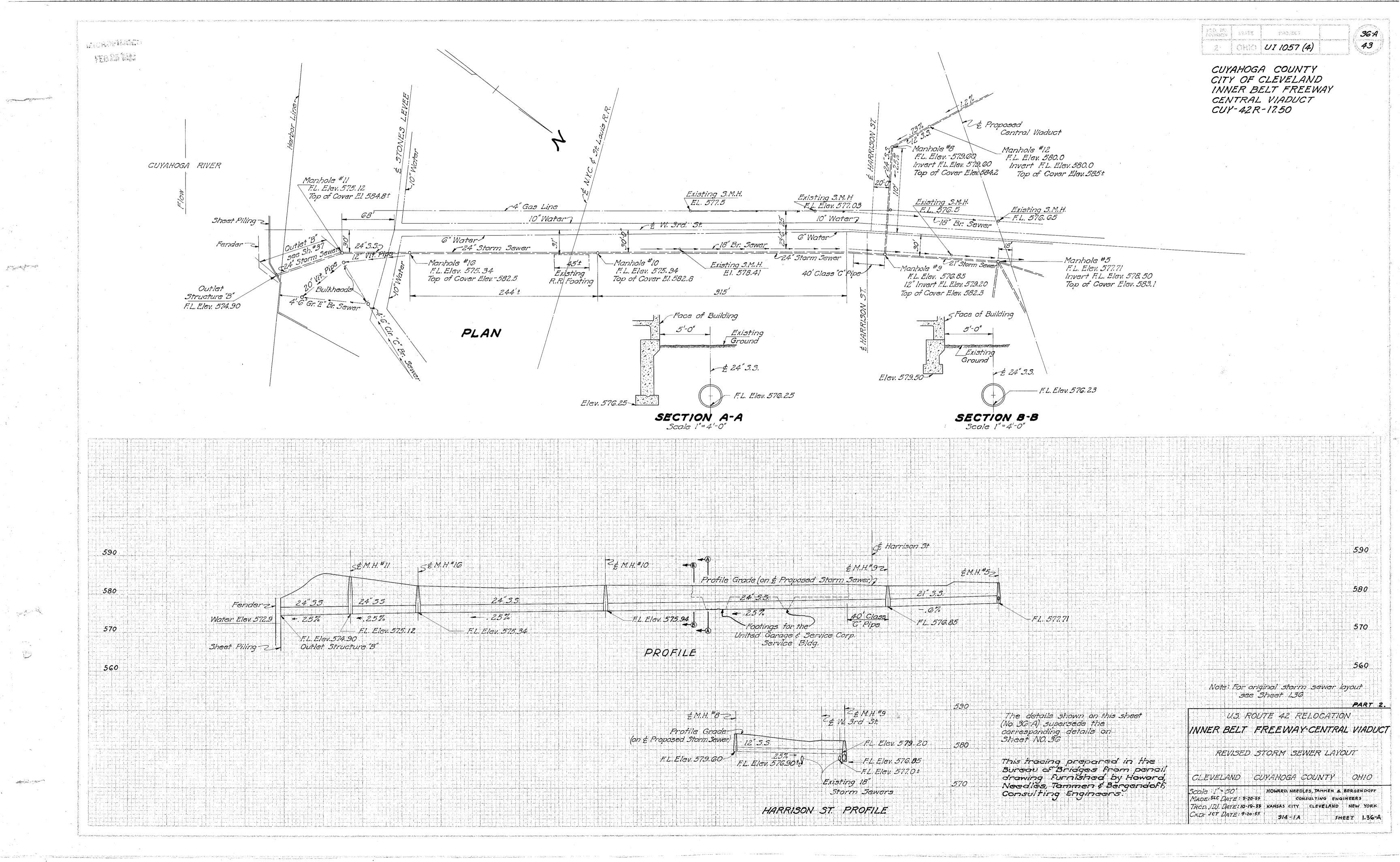
SHEET- 1.32

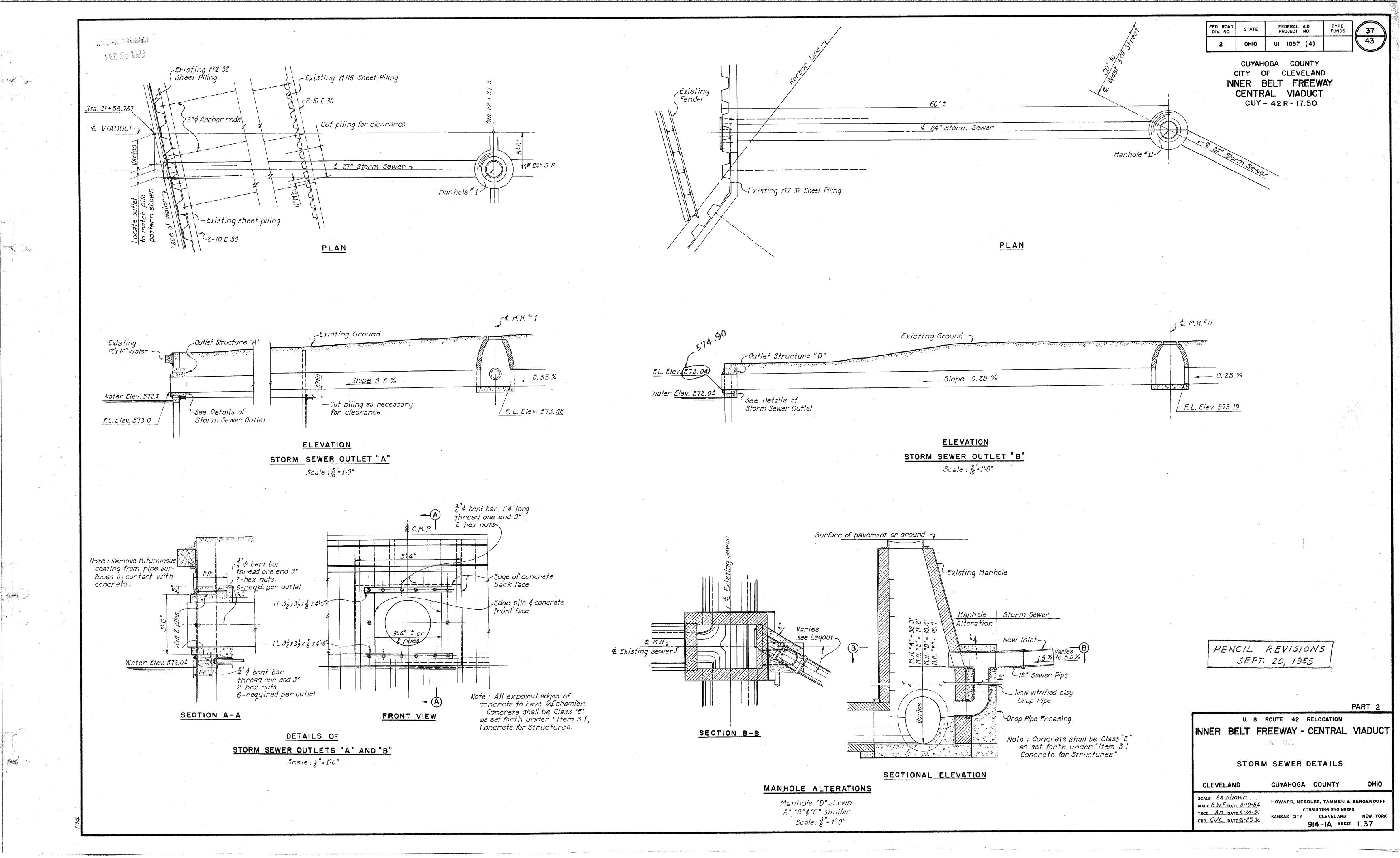


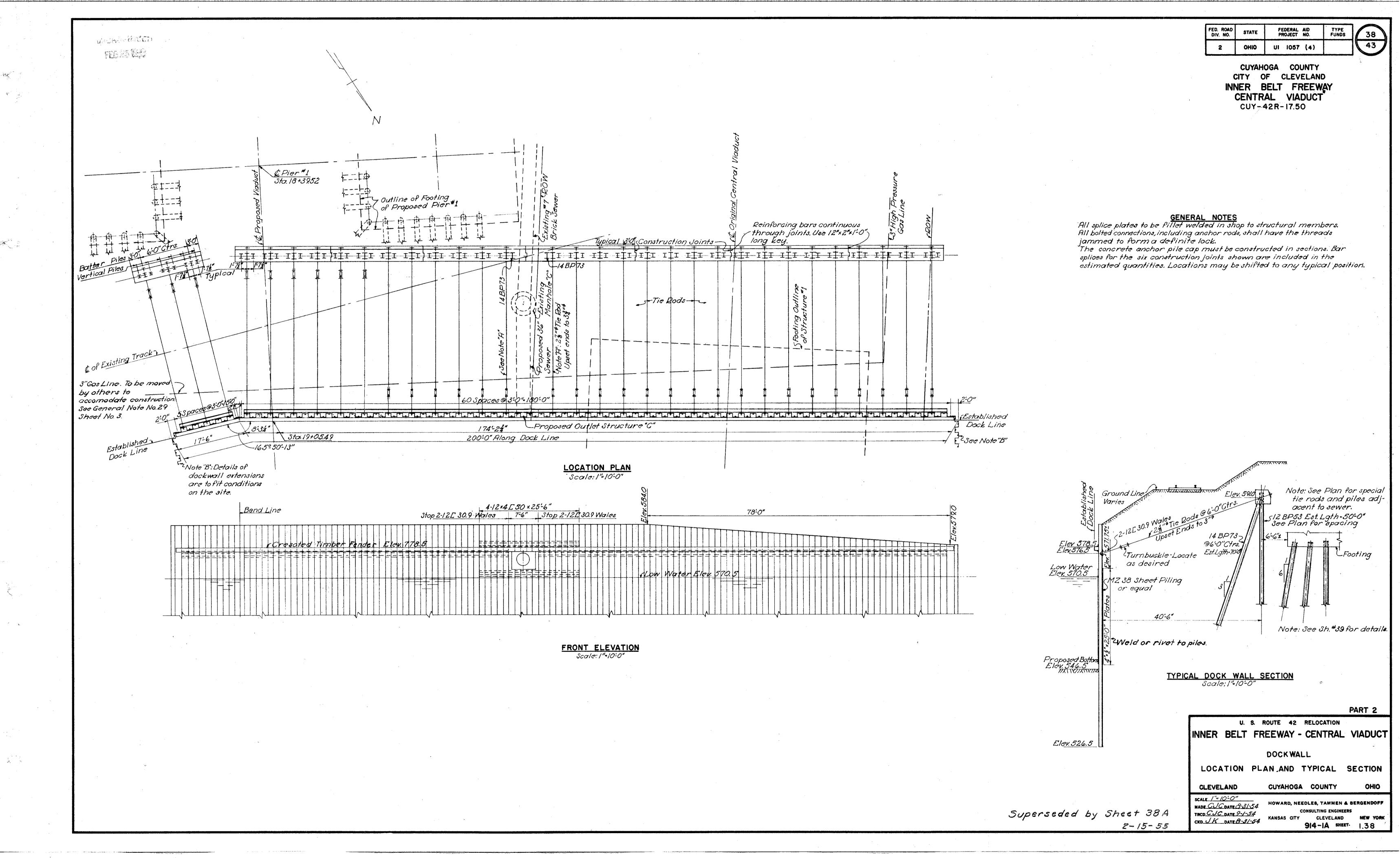












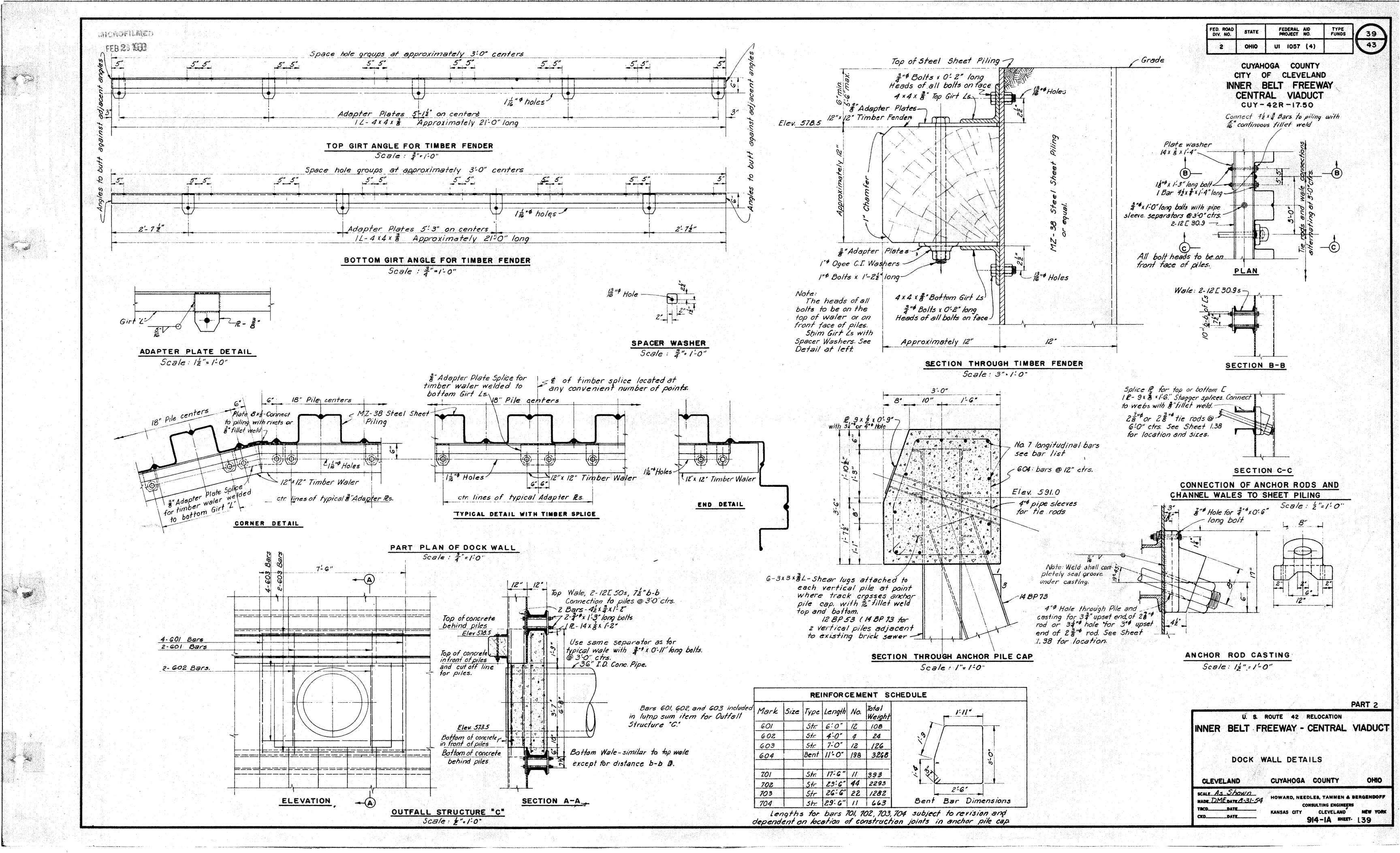
UI 1057 (A) MICROFILMED CUYAHOGÁ COUNTY CITY OF CLEVELAND FEB 28 1983 IMMER BELT FREEWAY CENTRAL VIADUCT CUY-42R-17.50 16 Spaces @ 5'93" = 93'-0" 5 Spaces @6'-0"= 30'-0" 6'-6" 5 Spaces@6'-6" = 32'-6" 12'-0" Anchor pile spacing as shown has been changed from the original spacing to concur with the actual field location of the existing # 1 brick sewer.

Tie rod spacing and other details at face of dockwall to remain the same. Note that some of the tie rods will not be perpendicular to the dockwall and will not be parallel to each other Piling driven prior to Feb. 15, 1955 & Pier \*1 5to 18+3952 GENERAL NOTES
All splice plates to be filler welded in shop to structural members Reinforcing bars continuous All bolted connections, including anchor rods, shall have the threads jammed to form a definite lock. / through joints. Use 12"x2"x1"-0"> Typical S'O Construction Joints The concrete anchor pile cap must be constructed in sections Box splices for the six construction joints shown are included in the estimated quantities. Locations may be shifted to any typical position, Ju Tio Bods ---\* Col Existing Tracks+ 3"Gos Line. To be moved by others to accomodate construction See General Note No. 29 Sheet No 3. Dock Line Sta. 19+0549 200-0" Along Dock Line -16.5° 50° 13" LOCATION PLAN Note B. Details of Scale: 1'410:0" dockwall extensions & Ground Line Letrenstates and month are to fit conditions on the site. Stop 2-12[ 30.9 Wales \_ 7-6" Stop 2-12[ 30.9 Wales 78:0" Band Line 14 BP 73 -96'0"Ctray Estloth-700 as desired Weld or rivet to piles TYPICAL DOCK WALL SECTION U. S. POUTE AZ PELOCATION Eler 526.5 DOCKWALL LOCATION PLAN, AND TYPICAL SECTION CUYAHOGA COUNTY CLEVELAND 568.5.1.5.10.00 9408.G.J.S. 8478.F.3.1.5.4 Supersedes Sheet 38 raceEdCoarrILIA caedKoarrAdist Revised anchor pile spacing - GA 2-15-55

PEDERAL AD PRIVICE NO

tie rode and piles asj-acent to sever. PART 2 INNER BELT FREEWAY - CENTRAL YEADUCT

Howard, Herdler, Trystem a Grademone?



GICTOFILMED FEB 20 Med

#### TIMBER CRIB WALL INSTALLATION

PREPARING BASE - The foundation or bed for the cribbing shall be firm and shall be approved by the Engineer before any cribbing is placed.

The foundation shall be sloped at right angles to the finished crib batter face.

FACE TIMBERS OR STRETCHERS - The timbers in the base tier and in alternate tiers above the base shall be as long as practicable. Preferably they shall have a minimum length of 8 feet. Joints in each tier shall stagger with joints in adjacent tiers.

Care shall be exercised in the erection of cribs to produce a true and even face built to line as shown on the plans. All face timbers shall be set parallel

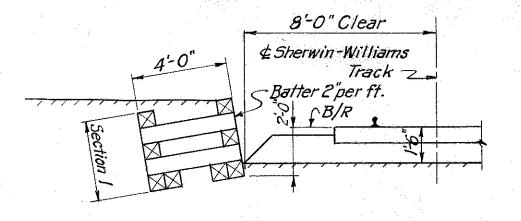
TIES OR HEADERS - Ties shall be anchored to the face by framing, drift bolting or other approved means.

Ties should be anchored in the fill to stretchers fastened to them at right angles by drift bolts or other suitable means.

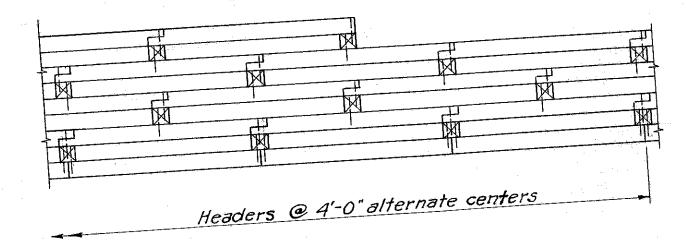
FASTENING - Each successive ther of open face cribbing shall be drift bolted together erateach tie, using one 34" drift bolt at each intersection where no splice occurs or at lap joints and two 3/4" drift bolts at butt joints. Drift bolts shall be long enough to extend through one tier and at least 3/4 of the distance into the next tier. Stagger drift bolts from tier to tier.

FILLING - The filling of the interior of the crib shall follow closely the erection of the successive tiers of units and at no time shall the wall be laid up higher than 3 feet above the back filled portion.

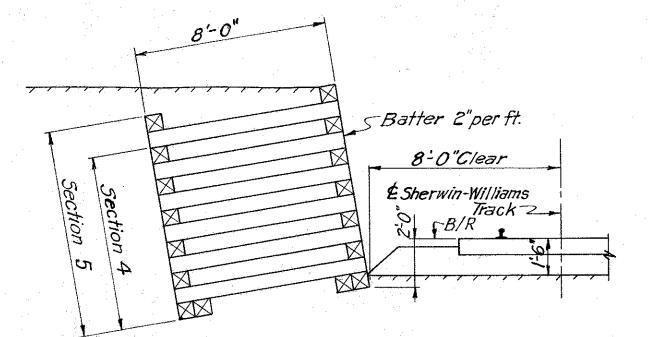
In open face cribbing a layer of hand-placed stone shall be placed in back of the front members of the cribbing to prevent loss of fill material through the openings.



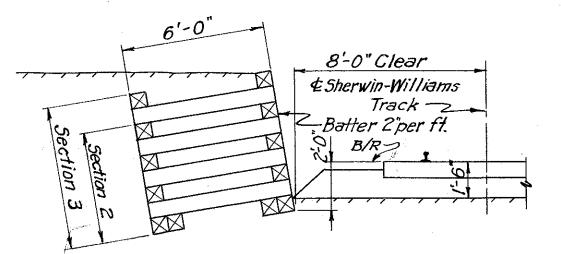
SECTION I Scale 14"=1"-0"



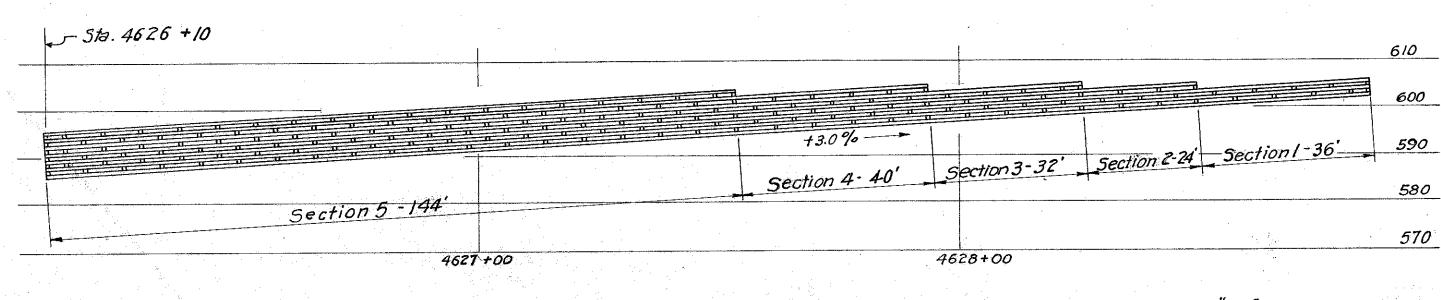
SPLICING DETAIL Scale 1/4"=1'-0"



SECTIONS 4 AND 5 Scale 1/4" = 1'-0"



SECTIONS 2 AND 3 Scale 1/4" = 1-0"



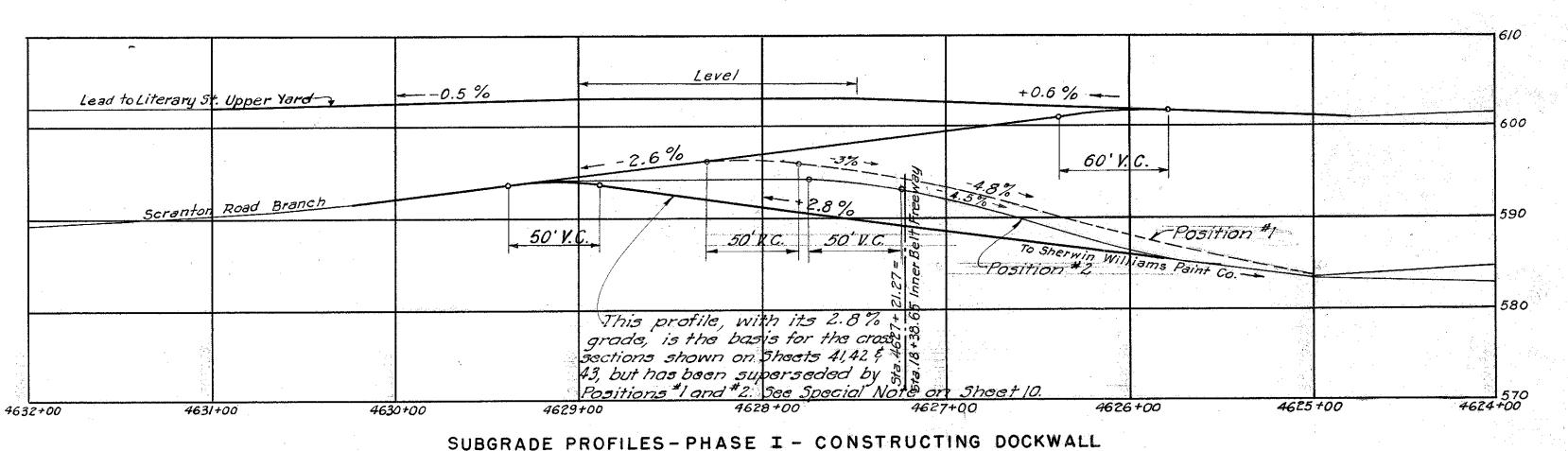
FRONT ELEVATION Scale | "=20'-0"

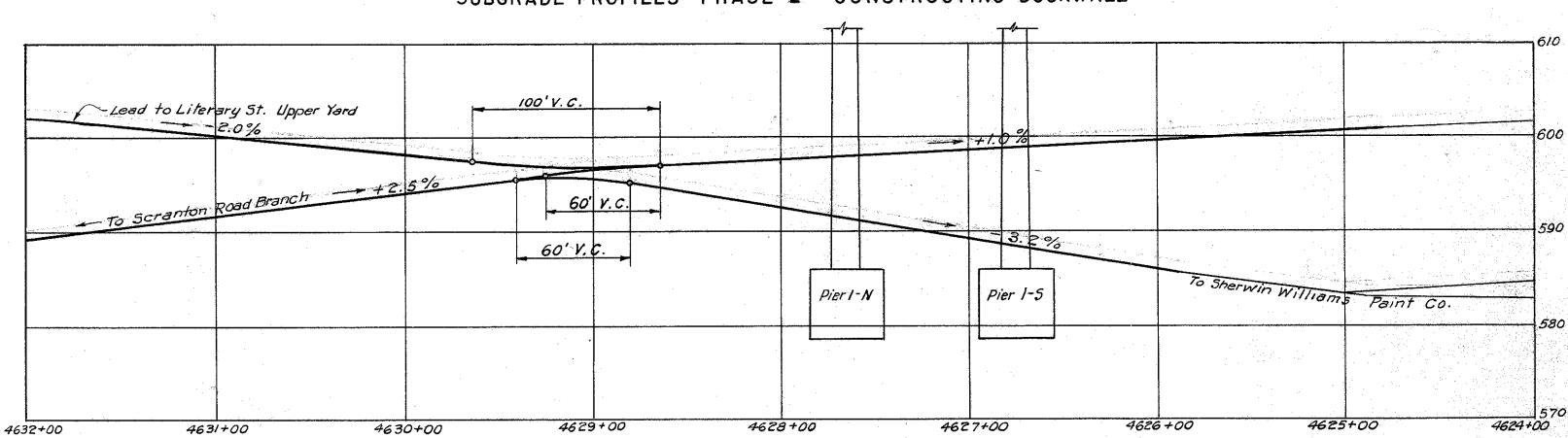
Note: All timbers are 8"x8"

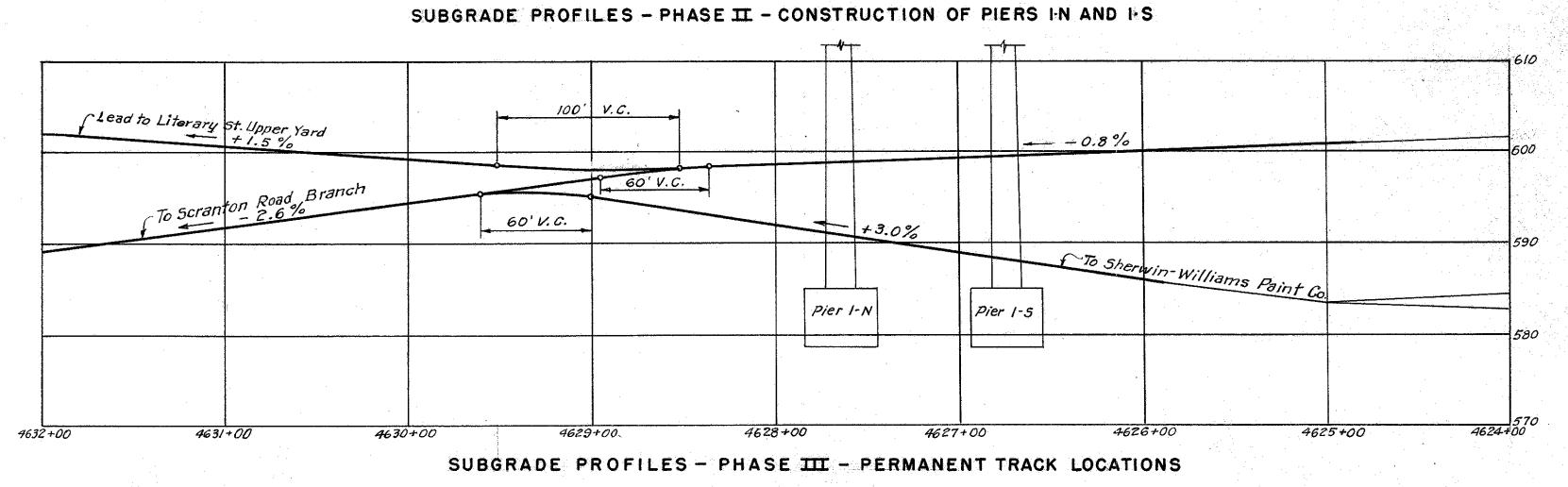
TEMPORARY TIMBER CRIB WALL For location of crib wall in plan, see Sheet 10.

FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	40
2	ОНЮ	UI 1057 (4)		43

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT CUY - 42R - 17.50







Subgrade profiles are shown 1'-0" below

base of rail elevations given on Erie Railroad

NOTE (Reference Phase I)

With tracks in position \*1, construct entire dockwall and westerly 150' to of anchor piles.

Install tie rods in easterly 50' to fackwall to within 10' to of track in position \*1. With tracks in position #2, install easterly 50't of anchor piles and complete tie rod connections. If necessary, support the easterly 50't of

dockwall by temporary shoring.

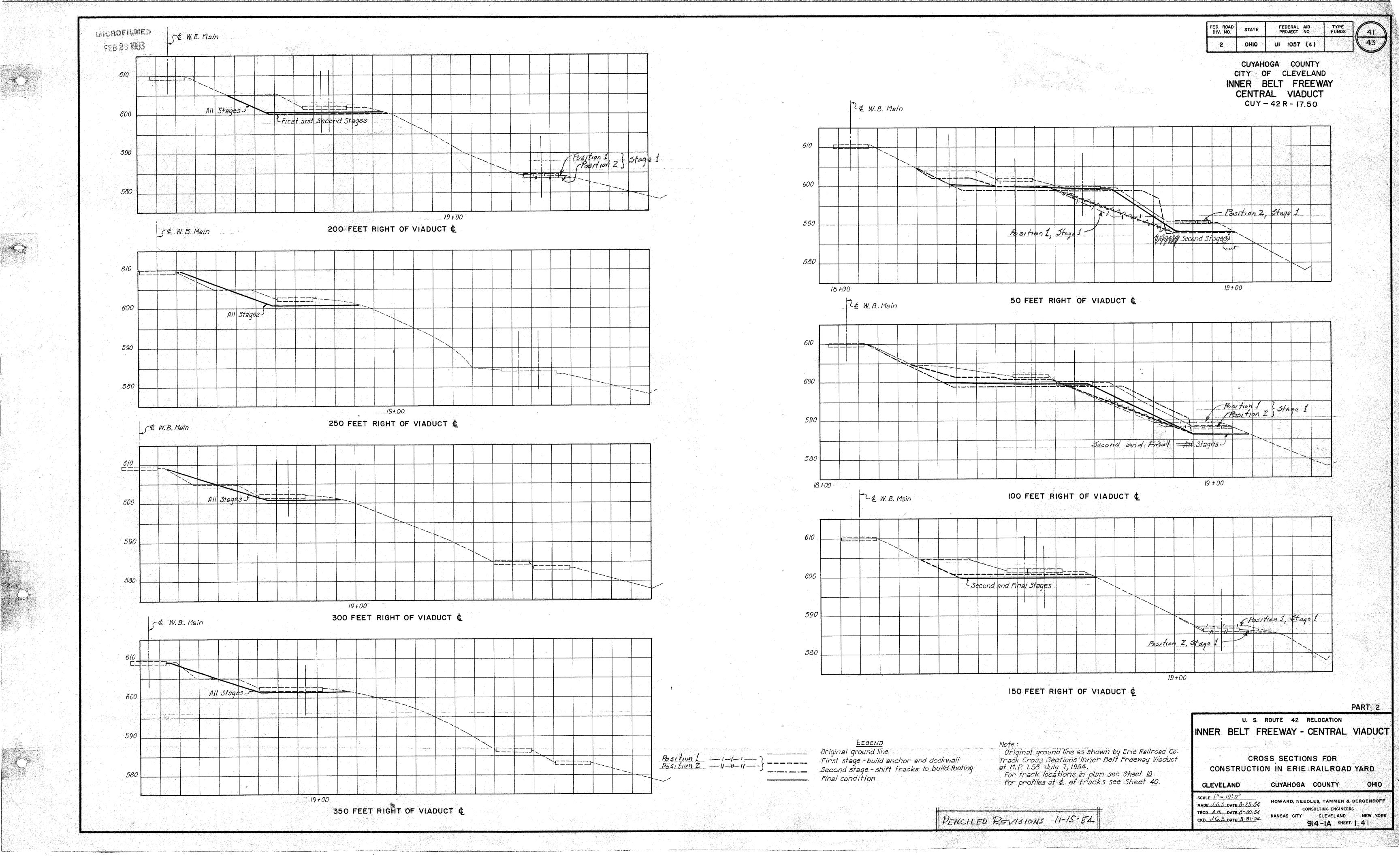
Company drawings D-194, D-195 and D-196
revised Aug. 13, 1954.
For track locations in plan see Sheet 10.
For cross sections parallel to & proposed Central Viaduct see Sheets 41, 42 and 43. Subgrade Profile Scale | Hor. |"= 50'-0" | Vert. |"= 10'-0"

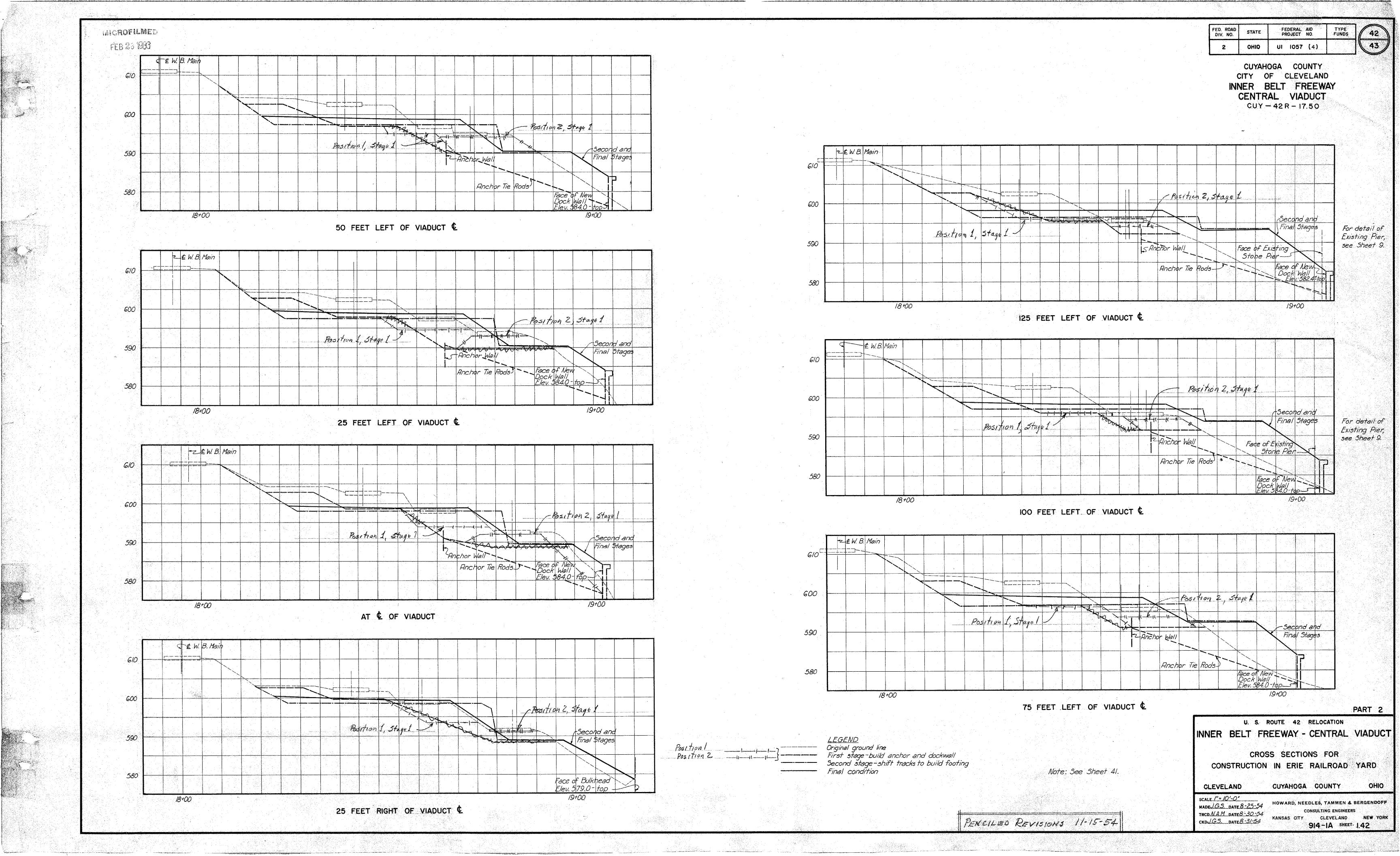
PART 2 U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO.

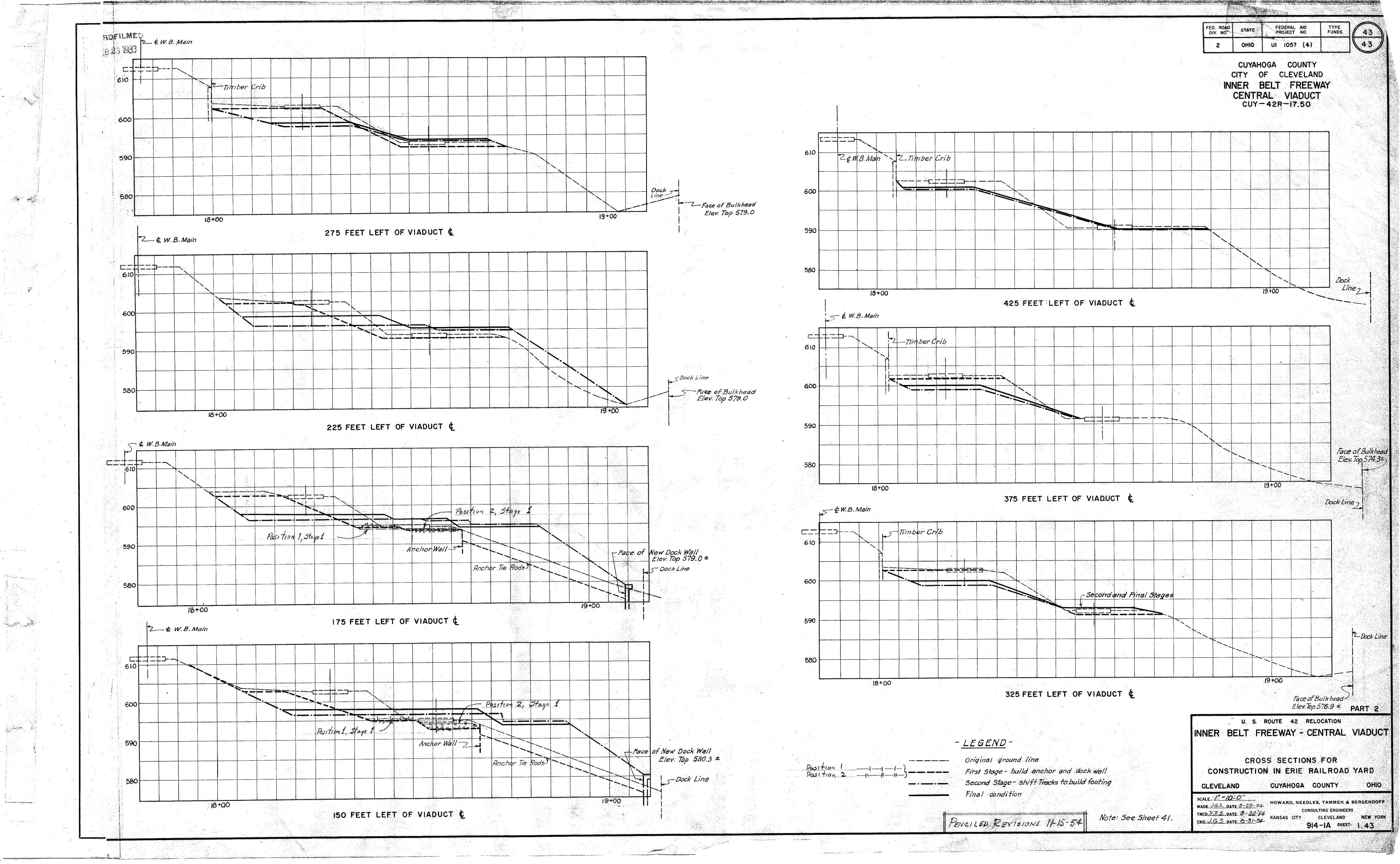
SUBGRADE PROFILES AND TEMPORARY TIMBER CRIB DETAILS

CUYAHOGA COUNTY CLEVELAND SCALE As Shown HOWARD, NEEDLES, TAMMEN & BERGENDOFF MADE D.L.C. DATE 8-30-54 TRCD 7/75 DATE 8-30-54 CKD JGS. DATE 9-1-54 CLEVELAND NEW YORK

914-1A SHEET- 1.40







### STATE OF CHID DEPARTMENT OF HIGHWAYS

MICROFILNIED FEB 15 BJ

CUX - 4212 - 17.50

FEDERAL AID PROJECT NO. 122

> CLYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT CUY-42R-17.50 PART 3

# INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42 R - 175 CUYAHOGA COUNTY CITY OF CLEVELAND

## PART 3 - SUPERSTRUCTURE

THIS IMPROVEMENT HAS BEEN DECLARED A LIMITED ACCESS HIGHWAY OR FREEWAY BY ACTION OF THE DIRECTOR OF HIGHWAYS IN ACCORDANCE WITH THE PROVISIONS OF SECTION 5511.02 REVISED CODE OF OHIO AND IS ESPECIALLY DESIGNED FOR THROUGH TRAFFIC.

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3 - 5 GENERAL NOTES

QUANTITIES

7-9 GENERAL LAYOUT, EXISTING CONDITIONS, TEST HOLE BORINGS

10 . II RAILROAD TRACK MODIFICATIONS

GRADES AND ELEVATIONS

13-17 GENERAL CROSS SECTIONS

18-26 FRAMING PLANS 27.28 FLOORBEAMS AND STRINGERS

29-34 FLOORBEAM TRUSSES

35-37 LATERAL BRAGING

38-43 TRUSS STRESSES AND DETAILS -UNIT I

44-46 TRUSS STRESSES AND DETAILS -UNIT 2

47-57 TRUSS STRESSES AND DETAILS-UNIT 3

80-87 TRUSS STRESSES AND DETAILS - UNIT 7 TRUSS STRESSES - UNIT 8 89-94 TRUSS STRESSES AND DETAILS - UNIT 9 ANCHOR BOLT PLAN AND DETAILS 96-98 SHOES 99,100 HANDRAIL , FASCIA , MEDIAN 101,102 LADDERS 103-109 ROADWAY DRAINAGE 110-113 ROADWAY EXPANSION JOINTS 114-119 ROADWAY SLAB DETAILS

120.121 REINFORCEMENT SCHEDULES

122 LIGHTING

58-62 TRUSS STRESSES AND DETAILS -UNIT 4

63-76 TRUSS STRESSES AND DETAILS - UNIT 5

77-79 TRUSS STRESSES AND DETAILS - UNIT 6

### LINE DATA

BEGIN PROJECT END PROJECT

NET LENGTH

STA. 16 + 13.02 STA 43 + 34.72

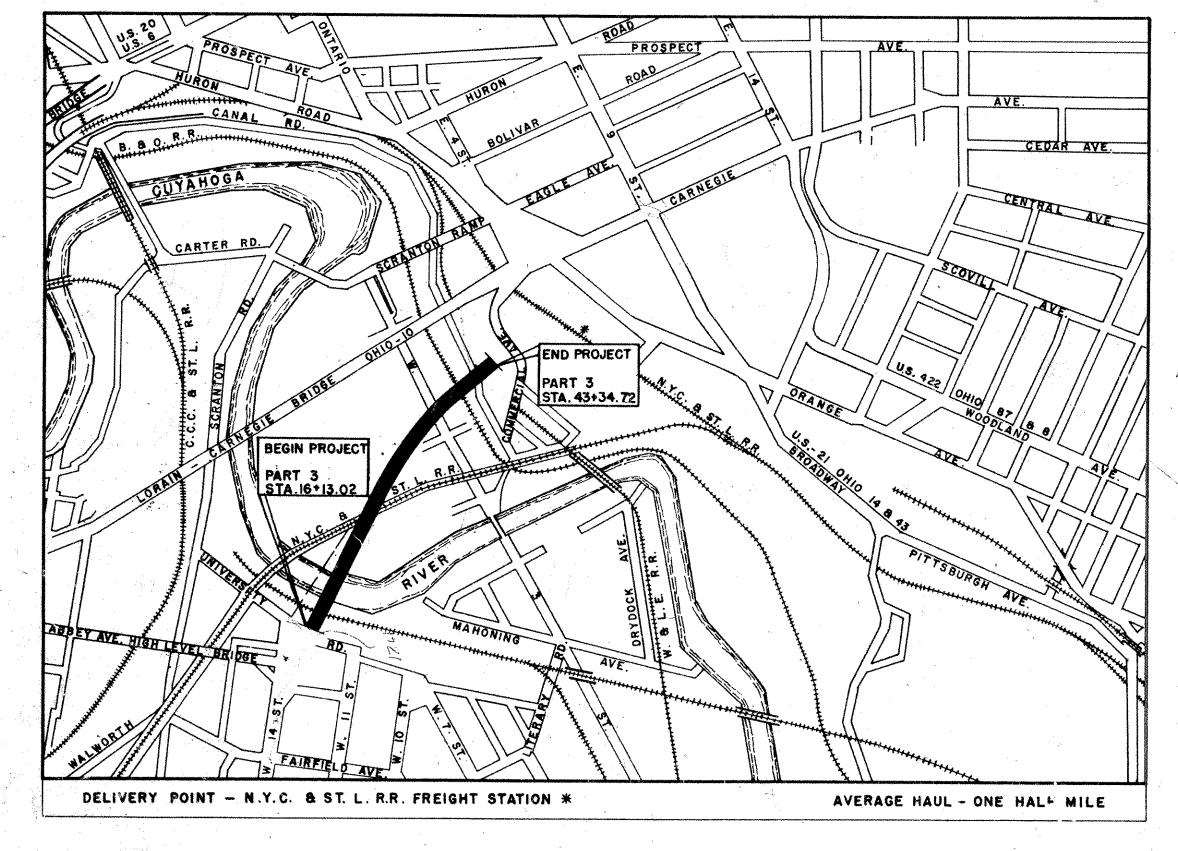
2,721.70 LIN. FT. OR 0.515 MILES

HOWARD NEEDLES TAMMEN & BERGENDOFF CONSULTING ENGINEERS

CLEVELAND NEW YORK KANSAS CITY

00078 FILE NO CUYAHOGA COUNTY DATE OF LETTING \_ CONTRACT NO.

H.G. SOURS ASSOCIATE COLUMBUS



THE STANDARD SPECIFICATIONS OF THE STATE OF OHIO DEPARTMENT OF HIGHWAYS INCLUDING CHANGES AND SUPPLEMENTAL SPECIFICATIONS LISTED IN THE PROPOSAL SHALL GOVERN THIS IMPROVEMENT.

I HEREBY APPROVE THESE PLANS AND DECLARE THAT THE MAKING OF THIS IMPROVEMENT WILL NOT REQUIRE THE CLOSING TO TRAFFIC OF THE HIGHWAY AND THAT PROVISIONS FOR THE MAINTENANCE AND SAFETY OF TRAFFIC WILL BE AS SET FORTH IN THE PLANS AND ESTIMATE.

THE RIGHT OF WAY FOR THIS IMPROVEMENT WILL BE PROVIDED BY THE STATE OF OHIO

DATE 5/11/55 DATE 6.2.55 DEPUTY DIRECTOR OF PLANNING AND PROGRAMMING APPROVED

DATE 5-10-5-5 ENGINEER OF BRIDGES APPR@VED ENGINEER OF LOCATION & DESIGN DATE\_\_\_\_ APPROVED DATE\_\_\_\_\_DEPUTY DIRECTOR OF DESIGN & CONSTRUCTION DATE 4-28-55 CHIEF ENGINEER, ERIE RAILROAD DATE 4-27-55 CHIEF ENGINEER, NEW YORK CENTRAL SYSTEM DATE 2-55 CHIEF ENGINEER, NEW YORK, CHICAGO AND SAINT LOUIS RAILROAD CO. DATE 5-11-55 CHIEF ENGINEER, BALTIMORE AND OHIO RAILROAD



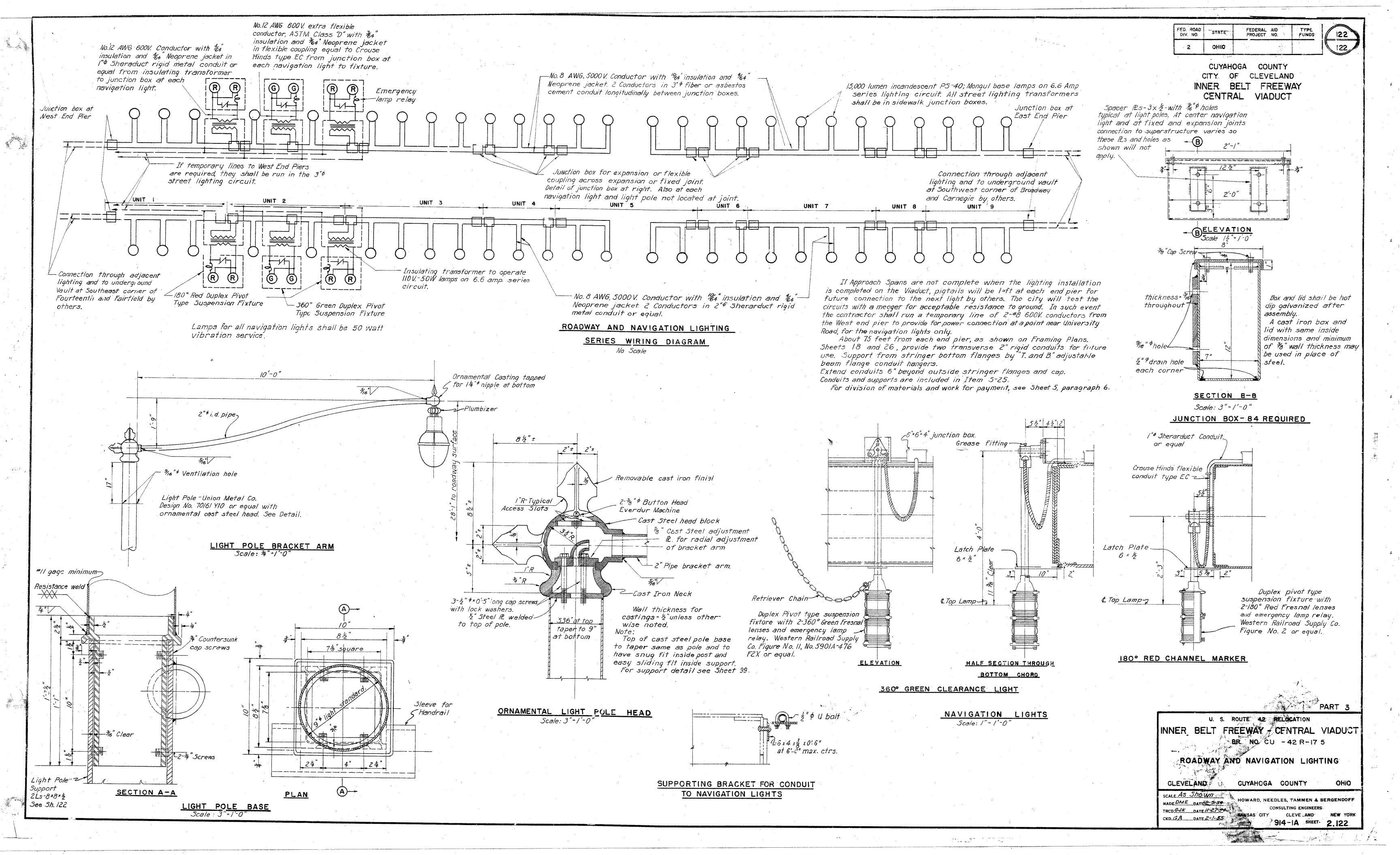


PORTION TO BE IMPROVED

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MARK	SIZE	NO.	LENGTH	TYPĘ	DIMENSION	NS B	WEIGHT LBS.
	<u></u>		UN	IF 6			
501	E	212		Str.			12 711
501 502	5 5	313 327	42"-0" 38*-6"	101	37'-8"	10"	13,711 13,131
503	5	140	35'-6"	Str.	<b>/</b>	•••	5,184
504	5	45	35'-0"	Str.			1,643
505	5	72	35'-3"	Str.			2,647
506	5	56	35'-9"	Str.			2,088
		109	381-6 "	101	38 -8"	10"	4,376
507	5 5	31	34*-0*	Str.	30 -0	10	1,099
508			331-9"	Str.			
509	5	64		<del>{</del>			2,253
510	5	84	33++6*	Str.			2,935
511	5	134	33 - 3 *	Str.			4,647
404	Ţ.	158	5'- 9"	120			607
401	4	10	38'-9"	Str.			259
402	14	. 10	38' -6"	Str.			257
			201 48				10 1100
601	6	288	38'-0"	Str.			16,438
602	6	313	50'-3"	Str.			23,624
603	6	31	301-3"	Str.			1,409
604	6	140	31!-9"	Str.			6,676
605	6	45	31'-3"	Str.			2,112
606	6	72	311-6"	Str.			3,407
607	6	56	32*-0*	Str.		,	2,692
608	6	96	38*-6*	Str.			5,551
609	. 6	64	301-0"	Str.			2,884
610	6	84	29*-9"	Str.			3,753
611	6	134	29*-6*	Štr.			5,937
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Total	Unit	6			,		- 129,320
Total	Unit	6	UN	IT 7	,		- 129,320
			UN				
501	5	908	42'-C"	Str.			39,776
501 502	5 5	908 63	42'-C" 36'-0"	Str.			39,776 2,366
501 502 503	5 5 5	908 63 115	42 *- C** 36 *- 0** 35 *- 6**	Str. Str.			39,776 2,366 4,258
501 502 503 504	5 5 5	908 63 115 59	42'-0" 36'-0" 35'-6" 35'-0"	Str. Str. Str.			39,776 2,366 4,258 2,154
501 502 503 504 505	5 5 5 5	908 63 115 59	42 1-0" 36 1-0" 35 1-6" 35 1-0" 34 1-9"	Str. Str. Str. Str.			39,776 2,366 4,258 2,154 3,624
501 502 503 504	5 5 5 5 5	908 63 115 59 100 40	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6"	Str. Str. Str. Str. Str. Str.			39,776 2,366 4,258 2,154 3,624 1,439
501 502 503 504 505 506 507	5 5 5 5 5 5	908 63 115 59 100 40	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6"	Str. Str. Str. Str. Str. 101	38'-7"	10"	39,776 2,366 4,258 2,154 3,624 1,439
501 502 503 504 505 506	5 5 5 5 5 5	908 63 115 59 100 40 434	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6"	Str. Str. Str. Str. Str. Str.	15-11"to 20!-6"	10"	39,776 2,366 4,258 2,154 3,624 1,439
501 502 503 504 505 506 507	5 5 5 5 5 5	908 63 115 59 100 40 434	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6"	Str. Str. Str. Str. Str. 101	<del></del>	10"	39,776 2,366 4,258
501 502 503 504 505 506 507 508 509	5 5 5 5 5 5	908 63 115 59 100 40	42'-C" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2"	Str. Str. Str. Str. Str. 101	15-11"to 20!-6"	10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197
501 502 503 504 505 506 507 508 509	5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 106 2 Ser 105	42'-C" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0"	Str. Str. Str. Str. Str. 101 100 101	15-11"to 20!-6" 33-11"to 38!-2"	10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077
501 502 503 504 505 506 507 508 509 510	5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 105	42'-C" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3"	Str. Str. Str. Str. Str. 101 100 101 101	15-11"to 20!-6" 33-11"to 38!-2" 17!-4" 50!-5"	10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077
501 502 503 504 505 506 507 508 509	5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 106 2 Ser 105	42'-C"  36'-0"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"	Str. Str. Str. Str. Str. 101 100 101	15-11"to 20!-6" 33-11"to 38!-2" 17!-4"	10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077
501 502 503 504 505 506 507 508 510 511 512 513	5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 106 2 Ser 105 1 Ser 106 1 Ser	42'-C"  36'-0"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"	Str. Str. Str. Str. Str. 101 100 101 101 100 100	15'-11"to 20'-6" 33'-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3"	10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 18
501 502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 56 7 1 05 1 218 1 Ser. 106 1	42'-C" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3" 17'-8" to 21'-11" 22'-2"	Str. Str. Str. Str. 101 100 101 101 100 100 100 100	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 19 11,653 2,181 23
501 502 503 504 505 506 507 508 509 510 511 512 513 514	5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 366 2 Ser 105 1 218 1 Ser. 106 1 22	42'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 100 101	15-11"to 20!-6" 33-11"to 38!-2" 17!-4" 50!-5" 16!-0" to 20!-3" 20!-6"	10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 23
501 502 503 504 505 506 507 508 510 511 512 513 514 515	5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 106 2 Ser 105 1 218 1 Ser. 106 1 2 2 2 74	42'-C"  36'-0"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 101 101 10	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 11,653 2,181 23 72 2,817
501 502 503 504 505 506 507 508 510 511 512 513 514 515 516	5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 105 1 218 1 Ser. 1 218 1 Ser. 2 74 78	42'-C"  36'-0"  35'-6"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 18 11,653 2,181 23 2,817 2,624
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517	5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 105 1 106 1 218 1 Ser. 106 1 2 74 78	42'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 101 Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,3 1,2 2,817 2,624
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518	5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 105 1 218 1 Ser 106 1 2 74 78 2	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3" 17'-8" to 21'-11" 22'-2" 5'-8" 34'-9" 36'-6" 32'-3" 17'-7" 34'-3"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 101 Str. Str. 100 Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 11,653 2,181 23 2,817 2,624 37 3,679
501 502 503 504 505 506 507 508 510 511 512 513 514 515 516 517 518	5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 1 05 1 (218 1 Ser. 106 1 Ser. 106 1 Ser. 106 1 Ser. 106 1 Ser. 106 1 Ser. 106 1 Ser. 106 106 106 106 106 106 106 106 106 106	42'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-3"  34'-0"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. 100 Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,3 12 7,2 2,624 3,679 1,454
501 502 503 504 505 506 507 508 510 511 512 513 514 515 516 517 518 519 520	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 ser 106 1 2 ser 106 1 2 74 78 2 103 41 247	42'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-0"  33'-9"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 11,653 2,188 23 12 2,624 37 2,624 3,675 1,454 8,695
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 106 2 Ser 106 1 218 1 Ser 106 1 22 74 78 2 103 41 247 57	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3" 17'-8" to 21'-11" 22'-2" 5'-8" 34'-9" 36'-6" 32'-3" 17'-7" 34'-3" 34'-0" 33'-9" 33'-6"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,3 1,2 2,817 2,624 3,679 1,454 8,695 1,992
501 502 503 504 505 506 507 508 510 511 512 513 514 515 516 517 518 519 520 521 522	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 105 1 218 1 Ser 106 1 2 2 74 78 2 103 41 247 57 145	#2'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-0"  33'-9"  33'-6"  33'-6"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,3 1,2 3,679 1,454 8,695 1,992 5,029
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 106 2 Ser 106 1 218 1 Ser 106 1 22 74 78 2 103 41 247 57	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3" 17'-8" to 21'-11" 22'-2" 5'-8" 34'-9" 36'-6" 32'-3" 17'-7" 34'-3" 34'-0" 33'-9" 33'-6" 33'-3" 33'-0"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,3 1,2 2,624 3,3 3,679 1,454 8,695 1,992 5,029
501 502 503 504 505 506 507 508 510 511 512 513 514 515 516 517 518 519 520 521 522	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 105 1 218 1 Ser 106 1 2 2 74 78 2 103 41 247 57 145	#2'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-0"  33'-9"  33'-6"  33'-6"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 11,653 2,18 23 17,2,624 33 3,679 1,454 8,695 1,992 5,029 2,409
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 105 1 218 1 Ser 106 1 2 74 78 2 103 41 247 57 145 70	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3" 17'-8" to 21'-11" 22'-2" 5'-8" 34'-9" 36'-6" 32'-3" 17'-7" 34'-3" 34'-0" 33'-9" 33'-6" 33'-3" 33'-0"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 13 11,653 2,181 2,624 37 2,817 2,624 37 1,454 8,695 1,992 5,029 2,409 2,699
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 106 1 2 74 78 2 74 78 2 103 41 247 57 145 70 79	#2'-C"  36'-0"  35'-6"  35'-6"  35'-6"  34'-9"  34'-6"  39'-5"  i7'-7" to 22'-2"  34'-9" to 39'-0"  i8'-2"  51'-3"  i7'-8" to 21'-i1"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  i7'-7"  34'-0"  33'-9"  33'-6"  32'-9"  32'-9"  32'-6"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 101 Str. Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 11,653 2,181 23 77 2,817 2,624 37 3,679 1,454 8,695 1,992 5,029 2,409 2,699 1,220
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 Ser 106 1 2 Ser 106 1 2 108 1 Ser 106 1 2 74 78 2 103 41 247 57 145 70 79 36 176	#2'-C"  36'-0"  35'-6"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-0"  33'-9"  33'-0"  32'-6"  32'-6"  35'-3"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,624 37 2,817 2,624 37 3,679 1,454 8,695 1,992 2,409 2,699 1,220 6,471
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 106 2 Ser 105 1 2 18 1 Ser 106 1 2 74 78 2 103 41 247 57 145 70 79 36 176 140	#2'-C"  36'-0"  35'-6"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  51'-3"  17'-8" to 21'-11"  22'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-3"  34'-0"  33'-9"  33'-6"  33'-9"  32'-6"  35'-3"  35'-3"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 Str. Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6" 33-11"to 38'-2" 17'-4" 50'-5" 16'-0" to 20'-3" 20'-6" 4'-10" 33'-11"	10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,624 3,675 1,454 8,695 1,992 2,409 2,699 1,220 6,471 5,220
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501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 532 533 534 535 536	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 106 2 Ser 105 106 1 218 1 Ser 106 1 2 74 78 2 103 41 247 57 145 70 79 36 176 140 40 41 41 247 57 145 70 79 36 176 176 176 176 176 176 176 176 176 17	#2'-C"  36'-0"  35'-6"  35'-0"  34'-9"  34'-6"  39'-5"  17'-7" to 22'-2"  34'-9" to 39'-0"  18'-2"  5'-8"  34'-9"  36'-6"  32'-3"  17'-7"  34'-3"  34'-0"  33'-9"  33'-6"  33'-9"  33'-6"  35'-3"  35'-3"  35'-3"  35'-9"  36'-6"  32'-9"  32'-6"  32'-9"  32'-6"  32'-9"  32'-6"  35'-3"  35'-9"  36'-6"  32'-9"  32'-6"  35'-3"  35'-9"  36'-6"  35'-3"  35'-9"  36'-6"  35'-3"  35'-9"  36'-6"  35'-3"  35'-9"  36'-6"  35'-8"  40'-4"  32'-0"  42'-8"  40'-4"  32'-0"  42'-8"	Str. Str. Str. Str. Str. 101 100 101 101 100 100 101 101 Str. Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6"  33-11"to 38'-2"  17'-4"  50'-5"  16'-0" to 20'-3"  20'-6"  4'-10"  33'-11"  15'-11"  15'-10"  39'-6"  24'-8"	10" 10" 10" 10" 10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,624 3,675 1,454 8,695 1,992 2,409 2,699 1,220 2,409 2,699 1,220 3,705 89 52 14 9,087 1,268 27 17 35 10
501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 36 1 2 2 3 6 7 1 06 1 2 2 7 4 7 8 2 103 41 247 57 145 70 79 36 176 140 64 96 2 2 1 2 1 2 1 2 1 3 1 1 2 1 3 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	#2'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 51'-3" 17'-8" to 21'-11" 22'-2" 5'-8" 34'-9" 36'-6" 32'-3" 17'-7" 34'-3" 34'-0" 33'-9" 33'-6" 33'-9" 33'-6" 35'-3" 35'-3" 35'-9" 36'-6" 35'-3" 37'-0" 42'-8" 25'-0" 13'-8" 40'-4" 32'-0" 25'-6" 16'-0" 12'-9" 16'-8" 33'-8"	Str. Str. Str. Str. 101 100 101 101 100 100 101 101 Str. Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6"  33-11"to 38'-2"  17'-4"  50'-5"  16'-0" to 20'-3"  20'-6"  4'-10"  33'-11"  15'-11"  12'-10"  39'-6"  24'-8"	10" 10" 10" 10" 10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 13,653 2,181 2,624 37 2,817 2,624 37 3,679 1,454 8,695 1,992 2,409 2,699 1,220 6,471 5,220 2,420 3,705 89 52 144 9,087 1,268 27 17 35 10 23
502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	908 63 115 59 100 40 434 1 36 1 2 2 3 6 7 1 06 1 2 2 7 4 7 8 2 103 41 247 57 145 70 79 36 176 140 64 96 2 2 1 2 1 2 1 2 1 3 1 1 2 1 3 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	#2'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 39'-5" 17'-7" to 22'-2" 34'-9" to 39'-0" 18'-2" 5'-8" 34'-9" 36'-6" 32'-2" 5'-8" 34'-0" 33'-9" 33'-6" 33'-9" 33'-6" 33'-9" 32'-6" 35'-3" 35'-3" 35'-3" 35'-3" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-3" 35'-9" 36'-6" 35'-9" 36'-6" 35'-9" 36'-6" 35'-9" 36'-8" 35'-9"	Str. Str. Str. Str. 101 100 101 101 100 100 101 101 Str. Str. Str. Str. Str. Str. Str. Str.	15-11"to 20'-6"  33-11"to 38'-2"  17'-4"  50'-5"  16'-0" to 20'-3"  20'-6"  4'-10"  33'-11"  15'-11"  15'-10"  39'-6"  24'-8"	10" 10" 10" 10" 10" 10" 10" 10" 10" 10"	39,776 2,366 4,258 2,154 3,624 1,439 17,844 2,197 8,077 1,653 2,181 2,624 37 2,817 2,624 37 3,675 1,454 8,695 1,992 5,029 2,409 2,699 1,220 6,471 5,220 2,420 3,705 89 52 14 9,087 1,268 27 13 17

MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIO A	В	WEIGHT LBS.
	• *		UNIT 7	CONT	INUED		
545	5	4	20'-9"	Str.			87
546	5	4	29*-9"	Str.	-	1	124
547	5	2	20 -8"	101	191-10"	10"	43
14.001	.,	11.00		120			
404	4	461	5'-9"	120			1771
401	4	30	33'-0"	Str.			661
402	4	20	37' <i>-</i> 6"	Str.		1	501
403	4	15	341+0"	Str.			341
		,				i.	
1				ì.			
							.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
601	6	644		101	21-6*	1'-0"	3,386
602	6	908		Str.			68,532
603 604	6	63 115		Str.			3,052 5,484
605	6	59		Str.	, , , , , , , , , , , , , , , , , , ,	<del> </del>	2,769
606	6	100	<del></del>	Str.			4,656
607	. 6	40	30*-9*	Str.			1,847
608	6	382 1 387	381-6"	Str.	· · · · · · · · · · · · · · · · · · ·		22,090
609	6	93 2 Ser.	16'-3" to 20'-9"	<del> </del>		· · · · · · · · · · · · · · · · · · ·	2,584
610	6	92	34'-3"to38'-6"	Str.		ļ	10,053
611	6	: 1	171-6"	Str.		<del> </del>	26
612	6	192 1 Ser. 93	50'-9"	Str.		<del>                                     </del>	14,635 2,567
613	6 6	93	16'-3"to20'-6" 20'-9"	Str.			2,567 31
615	6	2	34*-3"	Str.			103
616	6	103	30'-6"	Str.			4,719
617	6	2	42"-0"	Str.			126
618	6	74	32'-9"	Str.			3,640
619	6	78	28'-6"	Str.			3,339
620	6	2	16'-3"	Str.			45
621	6	41	301-3"	Str.			1,863
622	6	247	301-0"	Str.			11,130
623	. 6	57	291-9"	Str.			2,547
624	6	145	29!-6"	`Str.			6,429
625 626	6 6	70 78	29!-3" 29!-0"	Str.	r	<b> </b>	3,075 3,398
627	6	78 36	28'-9"	Str.		1	1,55
628	6	176	31'-6"	Str.	<u> </u>	<u> </u>	8,32
629	6	140	32'-0"	Str.			6,72
630	6	64	321-6"	Str.			3,12
63 l	6	96	33!-3"	Str.			4,79
632	6	2	33'-0"	Str.			9:
633	6	3 2	25*-0* 13*-0*	Str.			11:
634 635	6 6	190	401-0"	Str.			11,4]
636	6	38	281-311	Str.			1,612
637	6	2	161-0"	Str.			4.1
638	6	ı	81-6"	Str.			13
639	6	4 00-	201-6"	Str.			3
640	6	3 u e^-	4'-0" to 28'-0"	Str.			28
641	6	<b></b>	· · · · · · · · · · · · · · · · · · ·	Str.		-	63
642 643	6 6	4	17'-0" 26'-0"	Str.		-	10:
644	6	<del> </del>	5'-0"	Str.	<del></del>	<del>                                     </del>	13
645	6	2 2	20'-0"	Str.		1	61
*							
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	SIZE	NO.	LENGTH	TYPE	DIMENSIO A	NS B	WEIGHT LBS.
			UN	NIT 8			
501	5	309	421-0"	Str.	<u></u>		13,536
502	· 5	24	36"-0"	Str.			901
503	5	26	33"-3"	Str.			902
504	5	26	33"-0"	Str.			895
505	5	25	32'-9"	Str.	<del> </del>		854
506	5	51	32'-6"	Str.			1,729
507	5	26	35'-9"	Str.			969
508	5	23	36'-3"	Str.			870
509	5	80	37'-0"	Str.		!	3,087
510	5	106	36'-9"	Str.			4,063
511	5		24 1-9 "	Str.	FO. 107	:0#	26
512 513	5	20	131-8"	101	12'-10"	10"	14 968
514	5 5	29	32"-0" 38"-6"	Str.	37'-8"	IC"	8,714
515	5	218	381-2"	101	37'-4"	10"	8,678
516	5	50	36'-6"	Str.	V/ 1,	10	1.903
517	. 5	152	32'-3"	Str.			5.113
<u> </u>		132					
404	4	158	5'-9"	120			607
		`					
401	4	10	38' <b>-9</b> "	Str.			259
402	4	10	38'-6"	Str.			257
			•				
601	6	92	3*-6*	101	2'-6"	1'-0"	484
602	6	309	50'-3"	Str.			23,322
603	6	24	321-3"	Str.			1,163
604	6	26	291-6"	Str.	·		1,152
605	6.	26	291-3"	Str.	· · · · · · · · · · · · · · · · · · ·		1,142
606	6	25	29'-0"	Str.			1,089
607	6	51	281-9"	Str.			2,202
608	6	26	32'-0"	Str.			1,250
609	6	23	321-6"	Str.			1,123
610	6	80	331-3"	Str.			3.995
611	6	106	33'-0"	Str.		<del> </del>	5,254
612	6.	1	25'-0"	Str.			38
613	6	1	13'-0"	Str.			20
614	6	29	28 f = 3 H 38 f = 0 H	Str.			1,231
615		191		Str.			10,902
616	6	152	28!-6" 37!-9"	Str.			6,507
617 618	6	192 50	321-9"	Str.		`	10,886 2,460
****							,†
				<u> </u>	· · · · · · · · · · · · · · · · · · ·		
[otal	Unit	8					128,565
[otal	Unit	8	·	NIT 9			128,565
501	5	720	42°-0"	Str.			31,540
501 502	5 5	720	42'-0" 36'-0"	Str.			31,540
501 502 503	5 5 5	720 29 22	42'-0" 36'-0" 35'-6"	Str. Str.			31,540 1,089 815
501 502 503 504	5 5 5	720 29 22 19	42'-0" 36'-0" 35'-6" 35'-0"	Str. Str. Str.			31,540 1,089 819 694
501 502 503 504 505	5 5 5	720 29 22 19	42'-0" 36'-0" 35'-6" 35'-0" 34'-9"	Str. Str.			31,540 1,089 815 694 761
501 502 503 504	5 5 5 5 5	720 29 22 19	42'-0" 36'-0" 35'-6" 35'-0" 34'-9"	Str. Str. Str. Str. Str.	35*-2**	10"	31,540 1,089 815 694 761 38,430
501 502 503 504 505 506	5 5 5 5 5	720 29 22 19 21 1068	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0"	Str. Str. Str. Str. Str. Str.	35*-2**	,	31,540 1,089 815 694 761 38,430 8,185 4,121
501 502 503 504 505 506 507	5 5 5 5 5 5	720 29 22 19 21 1068 218	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6"	Str. Str. Str. Str. Str. Str.	35'-2"	10"	31,540 1,089 815 694 761 38,430 8,185 4,121
501 502 503 504 505 506 507	5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0"	Str. Str. Str. Str. Str. Ioi Str.		,	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932
501 502 503 504 505 506 507 508 509	5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3"	Str. Str. Str. Str. Str. Str. IOI Str. IOO	19'-0"	10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270
501 502 503 504 505 506 507 508 509 510 511	5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8"	Str. Str. Str. Str. Str. ioi Str. ioi	19'-0" 43'-5" 43'-8" 39'-10"	10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270
501 502 503 504 505 506 507 508 509 510	5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8"	Str. Str. Str. Str. Str. Str. 101 Str. 100 100	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284
501 502 503 504 505 506 507 508 509 510 511	5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4"	Str. Str. Str. Str. Str. ioi Str. ioo ioo ioo	19'-0" 43'-5" 43'-8" 39'-10"	10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284
501 502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 218 27	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 45'-7"	Str. Str. Str. Str. Str. ioi Str. ioi ioo ioo ioo ioo ioo	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291
501 502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 218	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8"	Str. Str. Str. Str. Str. ioi Str. ioo ioo ioo ioo	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 76) 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291
501 502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 218 27	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 45'-7"	Str. Str. Str. Str. Str. ioi Str. ioi ioo ioo ioo ioo ioo	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291
501 502 503 504 505 506 507 508 509 510 511 512 513 514	5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-10"	Str. Str. Str. Str. Str. ioi Str. ioi str. ioo ioo ioo ioi str. str.	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291
501 502 503 504 505 506 507 508 509 510 511 512 513 514 516	5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-10"	Str. Str. Str. Str. Str. ioi Str. ioo ioo ioo ioo str. str.	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291 609
501 502 503 504 505 506 507 508 509 510 511 512 513 514 516	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27 16	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-10" 36'-6"	Str. Str. Str. Str. Str. ioi Str. ioi str. ioo ioo ioi str. str. str. str.	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291 609
501 502 503 504 505 506 507 508 509 510 511 512 513 514 516 519 520 521 522 523	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27 16	42'-0" 36'-0" 35'-6" 35'-0" 34'-9" 34'-6" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-10" 36'-6" 34'-0" 33'-6" 33'-6"	Str.   Str.   Str.   Str.   IOO   Str.   Str	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291 609 965 461 880 874 867
501 502 503 504 505 506 507 508 509 510 511 512 513 514 516 520 521 522 523 524	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27 16 27 27 27 27 27 27 27	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-10" 36'-6" 34'-0" 33'-9" 33'-6" 33'-3" 33'-0"	Str.   Str.   Str.   Str.   IOI   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   Str.   Str	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291 609 965 461 880 874 867 757
501 502 503 504 505 506 507 508 509 510 511 512 513 514 516 516 520 521 522 523 524 525	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27 16 27 25 25 25 25 22	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-7" 45'-10" 36'-6" 33'-6" 33'-6" 33'-6" 33'-9" 32'-9"	Str.   Str.   Str.   Str.   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   Str.   St	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291 609 965 461 880 874 867 757
501 502 503 504 505 506 507 508 510 511 512 513 514 516 519 520 521 522 523 524 525 526	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27 16 27 27 27 27 27 27 27 27 27 27 27 27 27	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 36'-3" 20'-8" 45'-1" 45'-1" 45'-1" 45'-10" 36'-6" 34'-3" 34'-0" 33'-9" 33'-6" 32'-9" 32'-6"	Str.   Str.   Str.   Str.   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   Str.   S	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,291 609 461 880 874 867 757 922
502 503 504 505 506 507 508 509 510 511 512 513 514 516 519 520 521 522 523 524 525	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	720 29 22 19 21 1068 218 109 136 27 28 218 27 27 16 27 25 25 25 25 22	42'-0" 36'-0" 35'-6" 35'-6" 35'-0" 34'-9" 34'-6" 36'-0" 36'-3" 20'-8" 45'-1" 45'-4" 40'-8" 45'-7" 45'-7" 45'-10" 36'-6" 33'-6" 33'-6" 33'-6" 33'-9" 32'-9"	Str.   Str.   Str.   Str.   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   IOO   Str.   St	19'-0" 43'-5" 43'-8" 39'-10" 43'-11"	10" 10" 10" 10"	31,540 1,089 815 694 761 38,430 8,185 4,121 2,932 1,270 1,324 9,247 1,284 1,291 609

UNIT 9 CONTINUED  530 5 28 20'-1" 100 18'-5" 10" 531 5 27 20'-4" 100 19'-3" 10" 532 5 26 20'-11" 100 19'-3" 10" 533 5 1 21'-3" 100 19'-7" 10" 515 5 216 40'-4" 101 39'-6" 10" 517 5 11 29'-5" 101 28'-7" 10" 518 5 1 9'-9" Str.  404 4 30 42'-9" Str.  401 4 30 42'-9" Str.  601 6 644 3'-6" 101 2'-6" 1'-0" 602 6 720 50'-3" Str. 603 6 29 32'-3" Str. 604 6 22 31'-9" Str. 605 6 19 31'-3' Str. 606 6 21 31'-0" Str. 607 6 1068 30'-9" Str. 608 6 189 35'-6" Str. 609 6 94 36'-6" Str. 609 6 94 36'-6" Str. 610 6 118 19'-3" Str. 611 6 23 43'-9" Str. 612 6 24 44'-0" Str.	587 573 567 22 9,087 34 10	10" 10" 10"	INUED  18'-5" 18'-8"	100	201-1"	<del> </del>	5	
531   5   27   20'-4"   100   18'-8"   10"     532   5   26   20'-11"   100   19'-3"   10"     533   5   1   21'-3"   100   19'-7"   10"     515   5   216   40'-4"   101   39'-6"   10"     517   5   1   29'-5"   101   28'-7"   10"     518   5   1   9'-9"   Str.     404   4   363   5 -9"   120     401   4   30   42'-9"   Str.     402   4   15   34'-0"   Str.     601   6   644   3'-6"   101   2'-6"   1'-0"     602   6   720   50'-3"   Str.     603   6   29   32'-3"   Str.     604   6   22   31'-9"   Str.     605   6   19   31'-3'   Str.     606   6   21   31'-0"   Str.     607   6   1068   30'-9"   Str.     608   6   189   35'-6"   Str.     609   6   94   36'-6"   Str.     610   6   118   19'-3"   Str.     611   6   23   43'-9"   Str.     612   6   24   44'-0"   Str.     613   612   6   24   44'-0"   Str.     614   612   614   614   614   614   614   615	573 567 22 9,087 34 10	10"	18"-8"			<del> </del>	5	
531         5         27         20'-4"         100         18'-8"         10"           532         5         26         20'-11"         100         19'-3"         10"           533         5         1         21'-3"         100         19'-7"         10"           515         5         216         40'-4"         101         39'-6"         10"           517         5         1         29'-5"         101         28'-7"         10"           518         5         1         9'-9"         Str.           404         4         363         5-9"         120           404         4         30         42'-9"         Str.           404         4         30         42'-9"         Str.           601         6         644         3'-6"         101         2'-6"         1'-0"           602         6         720         50'-3"         Str.         604         6         22         31'-9"         Str.           604         6         22         31'-9"         Str.         606         21         31'-0"         Str.           605         6         19         31'-3' </td <td>567 22 9,087 31 10</td> <td>10"</td> <td></td> <td>100</td> <td>201-119</td> <td>27</td> <td></td> <td>530</td>	567 22 9,087 31 10	10"		100	201-119	27		530
100	22 9,087 34 10 1394				204			531
515         5         216         40'-4"         101         39'-6"         10"           517         5         1         29'-5"         101         28'-7"         10"           518         5         1         9'-9"         Str.         10"           404         4         363         5 - 9"         \$20         \$20           401         4         30         42'-9"         \$tr.         \$tr.           601         6         644         3'-6"         101         2'-6"         1'-0"           602         6         720         50'-3"         \$tr.         \$tr.         603         6         29         32'-3"         \$tr.           603         6         29         32'-3"         \$tr.         \$tr.         605         6         19         31'-9"         \$tr.           605         6         19         31'-3"         \$tr.         \$tr.         606         6         21         31'-0"         \$tr.           607         6         1068         30'-9"         \$tr.         \$tr.         609         6         94         36'-6"         \$tr.           609         6         94         36'	9,087 34 10 1394 857	1 8 2 ** 1	191-3"			26	<u> </u>	
517       5       1       29'-5"       101       28'-7"       10"         518       5       1       9'-9"       Str.       120         401       4       363       5 - 9"       120         401       4       30       42'-9"       Str.         402       4       15       34'-0"       Str.         601       6       644       3'-6"       101       2'-6"       1'-0"         602       6       720       50'-3"       Str.       60'       60'       60'-3"       Str.       604'-6"       Str.       604'-9"       Str.       605'-6"       Str.       606'-6"       Str.       606'-6"       Str.       608'-6"       Str.       608'-6"       Str.       609'-6"       Str.       609'-3"       Str.       609'-6"       Str.       610'-6"       Str.       610'-6"       Str.       610'-6"       Str.       611'-6"       612'-6"       Str.       612'-6"       612'-6"       Str.       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"       612'-6"	1394					216		
518       5       1       9'-9"       Str.         404       4       363       5-9"       f20         401       4       30       42'-9"       Str.         402       4       15       34'-0"       Str.         601       6       644       3'-6"       101       2'-6"       1'-0"         602       6       720       50'-3"       Str.       5tr.       603       6       29       32'-3"       Str.       5tr.       604       6       22       31'-9"       Str.       605       6       19       31'-3'       Str.       606       6       21       31'-0"       Str.       607       6       1068       30'-9"       Str.       608       6       189       35'-6"       Str.       609       6       94       36'-6"       Str.       610       6       118       19'-3"       Str.       611       6       23       43'-9"       Str.       612       6       24       44'-9"       Str.       612       6       24       44'-0"       Str.       612       6       24       44'-0"       Str.       612       6       24       44'-0"       5tr.       612	1394			<del></del>		<del></del>		
404       4       363       5 - 9"       f20         401       4       30       42' - 9"       Str.         402       4       15       34' - 0"       Str.         601       6       644       3' - 6"       101       2' - 6"       i' - 0"         602       6       720       50' - 3"       Str.       603       6       29       32' - 3"       Str.         603       6       29       32' - 3"       Str.       5tr.       604       6       22       31' - 9"       Str.       605       6       19       31' - 3"       Str.       606       6       21       31' - 9"       Str.       607       6       1068       30' - 9"       Str.       608       6       189       35' - 6"       Str.       609       6       94       36' - 6"       Str.       606       6       118       19' - 3"       Str.       606       6       189       35' - 6"       Str.       609       6       94       36' - 6"       Str.       606       6       23       43' - 9"       Str.       606       6       24       44' - 0"       5tr.       606       606       6       94       36' - 6"	857		•	<b>+</b>		-	<b></b>	
401       4       30       42'-9"       5tr.         402       4       15       34'-0"       5tr.         601       6       644       3'-6"       101       2'-6"       1'-0"         602       6       720       50'-3"       Str.       603       6       29       32'-3"       Str.       604       6       22       31'-9"       Str.       605       6       19       31'-3'       Str.       606       6       21       31'-0"       Str.       607       6       1068       30'-9"       Str.       608       6       189       35'-6"       Str.       609       6       94       36'-6"       Str.       610       6       118       19'-3"       Str.       611       6       23       43'-9"       Str.       612       6       24       44'-0"       Str.       612       6       24       44'-0"       5tr.       6	857			1				
402       4       15       34'-0"       5tr.         601       6       644       3'-6"       101       2'-6"       1'-0"         602       6       720       50'-3"       5tr.         603       6       29       32'-3"       5tr.         604       6       22       31'-9"       5tr.         605       6       19       31'-3'       5tr.         606       6       21       31'-0"       5tr.         607       6       1068       30'-9"       5tr.         608       6       189       35'-6"       5tr.         609       6       94       36'-6"       5tr.         610       6       118       19'-3"       5tr.         611       6       23       43'-9"       5tr.         612       6       24       44'-0"       5tr.				120	5 - 9"	363	ц	404
402       4       15       34'-0"       5tr.         601       6       644       3'-6"       101       2'-6"       1'-0"         602       6       720       50'-3"       5tr.         603       6       29       32'-3"       5tr.         604       6       22       31'-9"       5tr.         605       6       19       31'-3'       5tr.         606       6       21       31'-0"       5tr.         607       6       1068       30'-9"       5tr.         608       6       189       35'-6"       5tr.         609       6       94       36'-6"       5tr.         610       6       118       19'-3"       5tr.         611       6       23       43'-9"       5tr.         612       6       24       44'-0"       5tr.								
601 6 644 3'-6" 101 2'-6" 1'-0" 602 6 720 50'-3" Str. 603 6 29 32'-3" Str. 604 6 22 31'-9" Str. 605 6 19 31'-3' Str. 606 6 21 31'-0" Str. 607 6 1068 30'-9" Str. 608 6 189 35'-6" Str. 609 6 94 36'-6" Str. 610 6 118 19'-3" Str. 611 6 23 43'-9" Str.	341						<b></b>	
602       6       720       50'-3"       Str.         603       6       29       32'-3"       Str.         604       6       22       31'-9"       Str.         605       6       19       31'-3'       Str.         606       6       21       31'-0"       Str.         607       6       1068       30'-9"       Str.         608       6       189       35'-6"       Str.         609       6       94       36'-6"       Str.         610       6       118       19'-3"       Str.         611       6       23       43'-9"       Str.         612       6       24       44'-0"       Str.				Str.	34'-0"	15	4	402
602       6       720       50'-3"       Str.         603       6       29       32'-3"       Str.         604       6       22       31'-9"       Str.         605       6       19       31'-3'       Str.         606       6       21       31'-0"       Str.         607       6       1068       30'-9"       Str.         608       6       189       35'-6"       Str.         609       6       94       36'-6"       Str.         610       6       118       19'-3"       Str.         611       6       23       43'-9"       Str.         612       6       24       44'-0"       Str.								
603         6         29         32'-3"         Str.           604         6         22         31'-9"         Str.           605         6         19         31'-3'         Str.           606         6         21         31'-0"         Str.           607         6         1068         30'-9"         Str.           608         6         189         35'-6"         Str.           609         6         94         36'-6"         Str.           610         6         118         19'-3"         Str.           611         6         23         43'-9"         Str.           612         6         24         44'-0"         Str.	3,386	1'-0"	2'-6"		3'-6"			
604       6       22       31'-9"       Str.         605       6       19       31'-3'       Str.         606       6       21       31'-0"       Str.         607       6       1068       30'-9"       Str.         608       6       189       35'-6"       Str.         609       6       94       36'-6"       Str.         610       6       118       19'-3"       Str.         611       6       23       43'-9"       Str.         612       6       24       44'-0"       Str.	54,342 1,404						<del> </del>	
605       6       19       31'-3'       Str.         606       6       21       31'-0"       Str.         607       6       1068       30'-9"       Str.         608       6       189       35'-6"       Str.         609       6       94       36'-6"       Str.         610       6       118       19'-3"       Str.         611       6       23       43'-9"       Str.         612       6       24       44'-0"       Str.	1,048							
606 6 21 31'-0" Str. 607 6 1068 30'-9" Str. 608 6 189 35'-6" Str. 609 6 94 36'-6" Str. 610 6 118 19'-3" Str. 611 6 23 43'-9" Str. 612 6 24 44'-0" Str.	892			1		<del></del>	t	
607       6       1068       30*-9"       Str.         608       6       189       35'-6"       Str.         609       6       94       36'-6"       Str.         610       6       118       19'-3"       Str.         611       6       23       43'-9"       Str.         612       6       24       44'-0"       Str.	978				31'-0"	· · · · · · · · · · · · · · · · · · ·		
609 6 94 36'-6" Str. 610 6 118 19'-3" Str. 611 6 23 43'-9" Str. 612 6 24 44'-0" Str.	49,327	•		Str.	301-9"	1068	<del></del>	607
610 6 118 19'-3" Str. 611 6 23 43'-9" Str. 612 6 24 44'-0" Str.	10,078	,		Str.	35'-6"	189	6	608
611 6 23 43'-9" Str 612 6 24 44'-0" Str.	5,153				361-6"	94	6	609
612 6 24 44°-0" Str.	3,412			<del>}</del>		+		
	1,511	•	1.	· · · · · · · · · · · · · · · · · · ·		<del> </del>	<del></del>	
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613 6 24 44'-3" Str.	1,595							
614 6 188 40'-3" Str.	11,366			<del></del>		<del>}</del>		
615 6 23 44'-6" Str. 616 6 27 30'-6" Str.	1,537 1,237					4		·
616 6 27 30'-6" Str.	1,43/			sir.	30'-0"	21	D	010
618 6 16 32'-9" Str.	787		, , , , , , , , , , , , , , , , , , ,	S+-	221_QN	ie	2	£10
618 6 16 32'-9" Str.	101			olf.	94 - B	10	, D	OIQ
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621 6 13 30'-3" Str.	591	T	, , , , , , , , , , , , , , , , , , ,	Str.	30'-3"	13	6	621
622 6 25 30'-C" Str.	1,127		:					
623 6 25 29'-9" Str.	1,117			·				
624 6 25 - 29'-6" Str.	1,108					· · · · · · ·	<del> </del>	
625 6 22 29'-3" Str.	967			<del>                                     </del>		<del> </del>	<del> </del>	
626 6 28 29'-0" Str.	1,220							626
627 6 25 28'-9" Str.	1,080	a		Str.	28.1-9"	25	6	627
628 6 21 31'-6" Str.	994							
629 6 26 32'-0" Str.	1,250				32'-0"			
630 6 29 32'-6" Str.	1,416			<del></del>	32'-6"			
631 6 24 18'-9" Str. 632 6 24 19'-0" Str.	676 685				187-9"	<del></del>	<del>•</del>	
633 6 23 19'-6" Str.	674				19'-6"			
617 6 1 19'-9" Str.	30				191-9"	·····	<del> </del>	
619 6 190 40'-0" Str.	11,415	-	,				<del></del>	
620 6 1 10'-0" Str.	15			Str.	10'-0"	1	6	620
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Total Unit 9

ED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	121	
2	оню	•		122	

CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT

PART 3

U. S. ROUTE 42 RELOCATION
INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU -42R-175

REINFORCEMENT SCHEDULE

CLEVELAND CUYAHOGA COUNTY

SCALE None

MADE R.K. DATE 2-25-54

TRCD DATE CKD DER. DATE 9-10-54

CKD DER. DATE 9-10-54

SCALE NONE

HOWARD, NEEDLES, TAMMEN & BERGENDOFF

CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK

914-14 SHEET. 2.121

FEB 16 1830

MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIO A	NS B	WEIGHT LBS.
,		<u> </u>	UN	<u> </u>   T			
<b>.</b>	5	669	421-0"	Str.			29,306
501 502	5	218	20' - 8"	100	19'-0"	10"	4,700
503	5	218	28' - 2"	101	27'-0"	10*	6,405
504	5	109	45' - 8"	100	44'-O"	10"	5,192
5 <b>0</b> 5	5	218	46'-0"	101	39'-2"	10"	9,095
506	5	133.8	34'~6"	Str.			48,146
507	5	812	36'-0"	101	35'-2"	10"	8,185
508	5	109	36'-3"	Str.		,	4,121
				100			. = 2.4
HOH	4	339	5'-8"	:20.			1,302
(1.7)	3.2	1 100	Lee' O B	C4	<u> </u>		428
401	14. . H	15	11/2". 9 "	Str.	<u> </u>		681
-402	4	30	34-0*	SCF.			.001
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60 I	6	644	31 - 6"	101	21-6"	19-0"	3,386
602	6	669	50' - 3"	Str.			50,493
603	6	188	27-9	Str.	-		7,836
604	6	94	44-6	Str.			6,283
605	6	188	39'-9"	Str.			11,224
606	6	188	191-3"	Str.			5,436
607	6	1338	30"-9"	Str.	•		61,796
608	6	188		Str.	,	·	10,024
609	6	94	36¹ -6 "	Str.			5,153
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Total	Unit	1					279,192
,	1.0	<u> </u>		<u> </u>		<u> </u>	
			UN	IT 2			
501	5	414	42'-0"	Str.			18,136
502	5	218	50'-7"	101	491-9"	10"	11,501
503	5	218	* 511-0"	101	501-9 <sup>n</sup>	10"	11,596
504	5	828		Str.			29,794
404	ų.	209	5'+9"	120			803
1101	100	-	pal as		NAME AND ADDRESS OF THE PARTY O		~=-
401	4	20	50'-9"	Str.			678
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COL	6	92	31-6"	101	2'-6"	18-0"	484
יוומ	6	602	50'-3"	Str.	- V		45,436
601	<u> </u>	188		Str.		<u> </u>	14,260
602	<u> </u>	828	301-9"	Str.		<b></b>	38,242
602 603	. 6	,	30 -3				,
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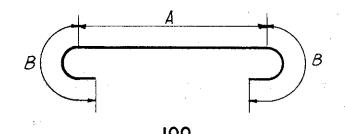
	SIZE	NO.	LENGTH	TYPE	DIMENSIO	B B	WEIGHT LBS.
			UI	VIT 3			,
501	5	922	42*-C*	St.			40,389
502	5	218	391-0"	101	38 ' - 2 "	10"	8,868
503	5	136	201-6"	100	18*-10"	10"	2,908
504	5	328	381-3"	101	371-5"	10"	13,085
505	5	218	51'-3"	101	501-5"	10"	11,653
506	5	108	38'-6"	101	37'-8"	10"	4,337
507	5	42	341-9"	Str.			1,522
508	5	28	201-0*	100	18*-4*	10"	584
509	5	54	35*-3*	Str.			1,985
510	5	56	35'-9"	Str.			2,088
511	5	54	36'-3"	Str.		<del> </del>	2,042
512	5	54 56	341-0" 331-6"	Str.	7-2-7-2-7-1	<u> </u>	1,915
513 514	5	56 54	331-0"	Str.			1,957
		34	<del></del>		121 5#	10"	
515 516	5	216	14'-3" 40'-0"	101	13'-5" 39'-2"	IC"	9,012
517	5	2.0	29'-3"	Str.	03 -2		31
518	5	1	17'-6"	Str.			18
519	5	1474	34*-6*	Str.			53,040
520	5	26	201-9"	100	19'-1"	10"	563
521	5	27	201-3"	100	18'-7"	10"	570
522	5	1	21*-0"	100	19'-4"	10"	22
722	-	•					
404	4	468	5' - 9"	120			1798
401	4	15	33'-3"	Str.			333
402	4	20	38' ~ <b>6</b> "	Str.		<b>†</b>	514
403	4	30	34 -0"	Str.			681
601	6	922	50'-3"	Str.			69,588
602	6	188	38*-6*	Str.		<del>                                     </del>	10,872
603	6	118	191-3*	Str.			3,412
604	6	282	37'-9"	Str.		<u> </u>	15,990
605	6	188	50'-9"	Str.			14,331
606	6	94	38'-0"	Str.			5,365
607	6	42	31'-0"	Str.			1,956
608	6	24	18'-9"	Str.			676
609	6	54	311-6"	Str.			2,555
6-10	6	56	321-0"	Str.			2,692
611	6	54	32'-6"	Str.			2,636
612	6	54	30'-3"	Str.			2,454
613	6	56	291-9"	Str.			2,502
614	6	54	291-3"	Str.			2,372
615	6		13'-6"	Str.			20
616	6	190	391-6"	Str.		,	11,273
617	6	130	29'-6"	Str.			44
618	6	i	17'-9"	Str.			27
619	6	1474	30'-9"	Str.			68,079
620	6	644	31-6"	101	2'-6"	1'-0"	3,386
621	6	23	191-6"	Str.			674
622	6	24	19'-0"	Str.			685
623	6	1	19*-9*	Str.			30
	ļ					-	
-							
			- - - A				
Total	Unit	3					383,408
	- * * -			NIT 4			
	T _						
	5	414	42"-0"	Str.		<del> </del>	18,136
501	<del></del>	<del> </del>	201 24				. K K 7
502	5	173	361-9"	Str.			
502 503	5 5	173	32'-6"	Str.			5,864
502 503 504	5 5 5	173 173 172	32*-6* 37*-3*	Str. Str.			5,864 6,683
502 503 504 505	5 5 5 5	173 173 172 172	32 1 - 6 " 37 1 - 3 " 32 1 - 0 "	Str. Str. Str.			6,63 5,864 6,683 5,74 2,609
502 503 504 505 506	5 5 5 5 5	173 173 172 172 69	32'-6" 37'-3" 32'-0" 36'-3"	Str. Str. Str. Str. Str.			5,864 6,683 5,74 2,609
502 503 504 505 506 507	5 5 5 5 5	173 173 172 172 69 69	32'-6" 37'-3" 32'-0" 36'-3" 33'-0"	Str. Str. Str. Str. Str. Str.	HO! _ iOn	107	5,864 6,683 5,74 2,609 2,378
502 503 504 505 506 507 508	5 5 5 5 5 5	173 173 172 172 69 69 218	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8"	Str. Str. Str. Str. Str. Str. 101	49*-10" 50*-2*	10"	5,864 6,683 5,74 2,609 2,379
502 503 504 505 506 507 508 509	5 5 5 5 5 5 5	173 173 172 172 69 69 218 216	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0"	Str. Str. Str. Str. Str. Str. 101	501-2"	10"	5,864 6,683 5,74 2,609 2,375 11,520
502 503 504 505 506 507 508 509 510	5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0"	Str. Str. Str. Str. Str. Str. 101 101		ļ	5,864 6,683 5,74 2,609 2,375 11,520 11,490
502 503 504 505 506 507 508 509 510	5 5 5 5 5 5 5 5 5	173 173 172 172 69 218 216 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0"	Str. Str. Str. Str. Str. 101 101 101 Str.	501-2"	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23
502 503 504 505 506 507 508 509 510 511	5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9"	Str. Str. Str. Str. Str. 101 101 101 Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23
502 503 504 505 506 507 508 509 510	5 5 5 5 5 5 5 5 5	173 173 172 172 69 218 216 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0"	Str. Str. Str. Str. Str. 101 101 101 Str.	501-2"	10"	5,864 6,683
502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 218 216 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9"	Str. Str. Str. Str. Str. 101 101 101 Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 22 41
502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9"	Str. Str. Str. Str. Str. 101 101 101 Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23
502 503 504 505 506 507 508 509 510 511 512 513	5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"	Str. Str. Str. Str. Str. 101 101 101 Str. Str. 101 101 101	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 22 4
502 503 504 505 506 507 508 509 510 511 512 513 404 404	5 5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1 1 1 209	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"	Str. Str. Str. Str. Str. Str. 101 101 101 101 Str. Str. 101 120	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 22 41 10
502 503 504 505 506 507 508 509 510 511 512 513 404	5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1 1	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"	Str. Str. Str. Str. Str. 101 101 101 Str. Str. 101 101 101	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 44 10
502 503 504 505 506 507 508 509 510 511 512 513 404 404	5 5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1 1 1 209	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"	Str. Str. Str. Str. Str. Str. 101 101 101 101 Str. Str. 101 120	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 44 10
502 503 504 505 506 507 508 509 510 511 512 513 404 404 402	5 5 5 5 5 5 5 5 5 5	173 173 172 172 69 69 218 216 1 1 1 209	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9"	Str. Str. Str. Str. Str. Str. 101 101 101 101 Str. Str. 5tr. 5tr. 5tr.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 22 4 10
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402	5 5 5 5 5 5 5 5 5 5 5 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9"	Str. Str. Str. Str. Str. 101 101 101 101 Str. Str. 5tr. 5tr.  Str. Str. Str. Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 44 10 803 344 344
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402	5 5 5 5 5 5 5 5 5 5 5 4 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15 15	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9"  50'-3" 33'-0"	Str. Str. Str. Str. Str. Str. 101 101 101 101 120  Str. Str. Str. Str. Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 24 10 803 344 345 31,247 8,575
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402 601 602 603	5 5 5 5 5 5 5 5 5 5 5 4 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15 15	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  50'-3" 34'-3" 33'-0" 28'-9"	Str. Str. Str. Str. Str. Str. 101 101 101 101 Str. Str. Str. 101  120  Str. Str. Str. Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 22 41 10 803 34 34,345 31,247 8,575 7,471
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402 601 602 603 604	5 5 5 5 5 5 5 5 5 5 5 4 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15 15 173 173	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9"  50'-3" 33'-0" 28'-9" 33'-6"	Str. Str. Str. Str. Str. Str. 101 101 101 101 Str. Str. 101 120 Str. Str. Str. Str. Str. Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 24 4 10 803 344 31,247 8,575 7,471 8,655
502 503 504 505 506 507 508 509 510 511 512 513 404 401 401 402 601 602 603 604 605	5 5 5 5 5 5 5 5 5 5 5 4 4 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15 15 414 173 173 173 172	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9" 34'-0" 34'-3" 33'-0" 28'-9" 33'-6" 28'-3"	Str. Str. Str. Str. Str. Str. 101 101 101 101 120 Str. Str. Str. Str. Str. Str. Str. Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,379 11,520 11,490 23 24 4 10 803 34 34 34,579 7,471 8,655 7,298
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402 601 602 603 604 605 606	5 5 5 5 5 5 5 5 5 5 5 4 4 4 4 4 6 6 6 6	173 173 172 172 69 69 218 216 1 1 1 209 15 15 173 173 173 172 172 69	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9" 34'-0" 34'-3" 33'-0" 28'-9" 33'-6" 28'-3" 32'-6"	Str. Str. Str. Str. Str. Str. 101 101 101 Str. Str. 101  120  Str. Str. Str. Str. Str. Str. Str. Str	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 22 4,10 803 34,345 3,247 8,575 7,471 8,655 7,298 3,368
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402 601 602 603 604 605 606 607	5 5 5 5 5 5 5 5 5 5 5 5 4 4 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15 15 173 173 172 172 69 69	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9" 34'-3" 33'-6" 28'-9" 33'-6" 28'-3" 32'-6" 29'-3"	Str.   Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,375 11,520 11,490 23 24 4 10 803 344 345 31,247 8,575 7,471 8,655 7,298 3,368 3,031
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402 601 602 603 604 605 606 607 608	5 5 5 5 5 5 5 5 5 5 5 4 4 4 4 4 6 6 6 6	173 173 172 172 69 69 218 216 1 1 1 209 15 15 173 173 173 172 172 69 69	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9" 34'-0" 34'-3" 33'-0" 28'-9" 33'-6" 28'-3" 32'-6" 29'-3" 50'-0"	Str. Str. Str. Str. Str. Str.  101 101 101 101 120  Str. Str. Str. Str. Str. Str. Str. Str	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,379 11,520 11,490 23 24 10 803 34 31,247 8,575 7,471 8,655 7,298 3,368 3,031 14,419
502 503 504 505 506 507 508 509 510 511 512 513 404 401 402 601 602 603 604 605 606 607	5 5 5 5 5 5 5 5 5 5 5 5 4 4 4 4	173 173 172 172 69 69 218 216 1 1 1 209 15 15 173 173 172 172 69 69	32'-6" 37'-3" 32'-0" 36'-3" 33'-0" 50'-8" 51'-0" 22'-0" 21'-3" 39'-9" 9'-8"  5'-9" 34'-3" 33'-6" 28'-9" 33'-6" 28'-3" 32'-6" 29'-3"	Str.   Str.	50*-2* 21*-2*	10"	5,864 6,683 5,74 2,609 2,379 11,520 11,490 23 24 10 803 34 31,247 8,575 7,471 8,655 7,298 3,368 3,031

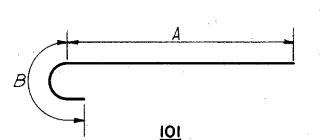
MARK	SIZE	NO.	LENGTH	TYPE	DIMENSIOI A	В	WEIGHT LBS.
,			UNIT 4	CONT	TINUED		
612	6	·l	9'-0"	Str.			[1
613	6	92	3'-6"	101	2*-6*	1'-0"	481
							· · · · · · · · · · · · · · · · · · ·
						_	
Tatal	باد: سال	11					171 730
Total	Unit	4	1 10 11	<b>+</b> 6			171,73 <b>0</b>
	_		UNI				
501 502	5 5	903 74	42°-0" 36°-0"	Str. Str.			39,557 2,779
503	5	89	351-6"	Str.			3,29
504	5	43	35'-0"	Str.			1,570
505 506	5 5	78 67	34*-9* 34*-6*	Str. Str.			2,827 2,411
507	5	429	38'-11"	101	381-1"	10*	17,413
508	5	Ser.	17'-7"to21'-10"		15'-11"to20'-2"	10"	2,179
509 510	5 5	1	21'-10" 17'-7"	100	20'-2" 	10"	23
511	5	218	51'-3"	101	50'-5"	10"	11,653
512	5	ı	131-8"	101	12'-10"	10*	į ų
513 514	5 5	216	36'-2" 38'-6"	101	35'-4" 37'-8"	10"	38 8,674
515	5	-10	29*-0"	Str.			30
516	5	77	36'-6"	Str.			2,931
517 518	5 5	36 2	32"-3"	Str.	331-10"	104	1,211 72
519	5	64	34'-3"	Str.	30 - 10		2,286
520	5	60	34'-0"	Str.			2,128
521 522	5 5	178 158	33'-9" 33'-6"	Str.			6,266 5,52
523	5	110	33'-3"	Str.			3,815
524	5	56	33'-0"	Str.			1,927
525	5	40	32*-9*	Str.			1,366
526 527	5 5	81 188	32"-6" 35*-3"	Str.			2,746 6,912
528	5	140	35'-9"	Str.			5,220
529	5	69	361-3 <sup>H</sup>	Str.		:	2,609
530 531	5 5	75 _ 36	37*-0" 36*-9"	Str.			2,894 1,380
532	5	2 Ser.	4'-0" to 42'-0"	Str.			192
533	5	2	11'-0"	Str.			23
534 535	5	2 95	23'-0" 32'-0"	Str.	<u> </u>		3,17
536	5 5	95 2	141-0"	Str.			29
537	5	2	26'-0"	Str.	001 107	i e P	54
538 539	5	2	39'-8"	101	38"-10" 20"-4"	10"	124
540	5	2	28*-2"	101	27'-4"	10"	59
541	5		34'-10"to39'-1"	101	34'-0"to38'-3"	10"	4,047
542 543	5 5	- 1	34'-10"	101	34'-10" 38'-3"	10"	36 41
544	5	î Ser.	34'-7" to 39'-4"		331-9"to381-6"	10"	4,047
545	5	2	10*-0"	Str.			21
546 547	5	2 Seg.	21'-0"	Str.		<u> </u>	44 15(
547 548	5 5	2	13'-0" to 35'-0"	Str.			33
549	5	2	271-0"	Str.	and a second second		56
550 551	5	1 Ser. 106		į.	15'-8" 15'-8"	10"	2,174
551 552	5 5	1	17'-4" 22'-1"	100	20'-5"	10"	23
553	5	i	16'-2"	101 -	151-4"	10"	17
554	5	1	71-6"	Str.	101 .	10=	3
;555 556	5 5	1	18"-11" 31"-2"	101	18'-1" 30'-4"	10"	20 33
557	5	1	17'-9"	Str.	-		15
404	ų	457	51'-9"	150			158
401	4	30	33'-0"	Str.			661
402	4	20	37'-6"	Str.			501
403	4	15	341-0"	Str.			344
601	6	552	31-6"	101	2*-6*	1'-0"	2,902
6 C 2	6	903	501-3"	Str.			68,15 <sup>1</sup>
603	6	74	32+-3"	Str.			3,585
604 605	6	88 43	31'-9"	Str.			4,197 2,018
606	6	78	31'-0"	Str.			3,632
607	6	67	30'-9"	Str.			3,09
608	6	377 1 Seg.	38'-6" 16'-3" to 20'-6'	Str.			21,80
600		, 50			<b></b>	ļ	
609 610	6	3	20'-6"	Str.			92

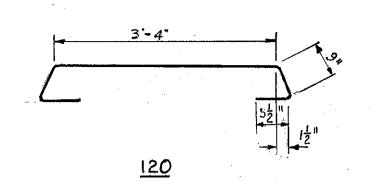
614 6 2 35'-6" Str. 10,88 615 6 190 38'-0" Str. 2,97 616 6 65 30'-6" Str. 2,97 617 6 1 17'-9" Str. 3,72 618 6 77 32'-9" Str. 3,72 619 6 36 28'-6" Str. 1,54 620 6 3 34'-0" Str. 2,66 621 6 59 30'-3" Str. 2,66 622 6 178 30'-0" Str. 8,02 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,67 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 3,49 627 6 81 28'-9" Str. 8,88 629 6 140 32'-0" Str. 8,38 629 6 140 32'-0" Str. 8,38 629 6 140 32'-0" Str. 8,38 631 6 75 33'-3" Str. 8,78 633 6 2 8 8 31'-6" Str. 3,36 631 6 75 33'-3" Str. 3,78 632 6 36 33'-0" Str. 3,38 633 6 2 8 8 10'-0" Str. 3,38 634 6 2 11'-0" Str. 3,78 635 6 4 2 11'-0" Str. 32 636 6 95 28'-3" Str. 66 637 6 4 10'-0" Str. 66 638 6 2 2 22'-0" Str. 66 639 6 3 39'-0" Str. 66 644 6 2 27'-6" Str. 66 650 6 1 88 34'-3" Str. 66 644 6 2 27'-6" Str. 66 656 6 95 28'-3" Str. 66 664 6 2 27'-6" Str. 66 665 6 95 28'-3" Str. 66 667 668 6 22'-0" Str. 66 668 6 2 2 22'-0" Str. 66 668 6 2 2 22'-0" Str. 66 669 6 2 27'-6" Str. 66 669 6 2 27'-6" Str. 66 669 6 1 188 34'-3" Str. 66 669 6 2 27'-6" Str. 66 669 6 1 188 34'-3" Str. 65 664 6 1 188 34'-3" Str. 65 665 6 1 1 16'-0" Str. 66 665 6 1 1 16'-0" Str. 66 669 6 1 16'-0" Str. 65 669 6 1 16'-0" Str. 65 669 6 1 1 16'-0" Str. 65 670 6 1 1	MARK	SIZE	NO.	LENGTH	TYPE	DIMENSION A	8 B	WEIGHT LBS.
614 6 2 35'-6" Str. 10,84 616 6 190 38'-0" Str. 2,97 617 6 1 17'-9" Str. 2,97 618 6 77 32'-9" Str. 3,78 619 6 36 28'-6" Str. 1,54 620 6 3 34'-0" Str. 2,66 620 6 3 34'-0" Str. 2,66 621 6 59 30'-3" Str. 2,66 622 6 178 30'-0" Str. 3,00 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,67 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 3,49 627 6 81 28'-9" Str. 3,49 628 6 188 31'-6" Str. 6,77 630 6 69 32'-6" Str. 3,38 631 6 75 33'-3" Str. 3,78 632 6 36 33'-0" Str. 3,38 631 6 75 33'-3" Str. 3,78 633 6 2 864 81'-0" Str. 3,38 634 6 2 11'-0" Str. 3,78 635 6 4 23'-0" Str. 3,78 636 6 95 28'-3" Str. 3,78 637 6 4 10'-0" Str. 32 647 6 14 10'-0" Str. 32 648 6 188 6 2 22'-0" Str. 32 659 6 14 23'-0" Str. 32 659 6 14 23'-0" Str. 32 650 6 14 23'-0" Str. 32 651 6 75 33'-3" Str. 3,78 652 6 16 16 29'-3" Str. 32 653 6 17 5 33'-3" Str. 3,78 654 6 2 22'-0" Str. 32 655 6 17 5 33'-3" Str. 32 657 6 17 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5				UNIT 5	CON	<b>FINUED</b>		,
614 6 2 35'-6" Str. 10,84 616 6 190 38'-0" Str. 2,97 617 6 1 17'-9" Str. 2,97 618 6 77 32'-9" Str. 3,78 619 6 36 28'-6" Str. 1,54 620 6 3 34'-0" Str. 2,66 620 6 3 34'-0" Str. 2,66 621 6 59 30'-3" Str. 2,66 622 6 178 30'-0" Str. 3,00 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,67 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 3,49 627 6 81 28'-9" Str. 3,49 628 6 188 31'-6" Str. 6,77 630 6 69 32'-6" Str. 3,38 631 6 75 33'-3" Str. 3,78 632 6 36 33'-0" Str. 3,38 631 6 75 33'-3" Str. 3,78 633 6 2 864 81'-0" Str. 3,38 634 6 2 11'-0" Str. 3,78 635 6 4 23'-0" Str. 3,78 636 6 95 28'-3" Str. 3,78 637 6 4 10'-0" Str. 32 647 6 14 10'-0" Str. 32 648 6 188 6 2 22'-0" Str. 32 659 6 14 23'-0" Str. 32 659 6 14 23'-0" Str. 32 650 6 14 23'-0" Str. 32 651 6 75 33'-3" Str. 3,78 652 6 16 16 29'-3" Str. 32 653 6 17 5 33'-3" Str. 3,78 654 6 2 22'-0" Str. 32 655 6 17 5 33'-3" Str. 32 657 6 17 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	613	6		131-0"	Str.			20
616 6 65 30'-6" Str. 2,97 617 6 1 17'-9" Str. 2 618 6 77 32'-9" Str. 3,78 619 6 36 28'-6" Str. 1,59 620 6 3 34'-0" Str. 2,66 621 6 59 30'-3" Str. 2,66 622 6 178 30'-0" Str. 3,78 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,87 625 6, 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,78 627 6 81 28'-9" Str. 3,44 628 6 188 31'-6" Str. 6,73 630 6 69 32'-6" Str. 3,34 633 6 2 36' 8'-0" Str. 3,34 633 6 2 36' 8'-0" Str. 3,37 634 6 2 11'-0" Str. 3,37 635 6 4 23'-0" Str. 3,37 636 6 95 28'-3" Str. 3,78 637 6 4 10'-0" Str. 33 638 6 2 22'-0" Str. 33 640 6 2 11'-0" Str. 33 651 6 75 33'-3" Str. 3,78 652 6 36 33'-0" Str. 3,78 653 6 4 23'-0" Str. 3,78 654 6 5 5 8 8 8 39'-0" Str. 3,78 655 6 95 28'-3" Str. 3,78 656 6 95 28'-3" Str. 3,78 657 6 4 10'-0" Str. 3,78 658 6 95 28'-3" Str. 4,03 659 6 3 39'-0" Str. 66 659 6 1 38'-0" Str. 66 659 6 1 38'-0" Str. 66 659 6 2 22'-0" Str. 66 659 6 1 38'-0" Str. 66 669 6 2 22'-0" Str. 66 669 6 1 38'-0" Str. 55 669 6 1 38'-3" Str. 55 679 679 679 570 670 570 670 670 670 670 670 670 670 670 670 6	614				1			107
617 6 1 17'-9" Str. 3.78 618 6 77 32'-9" Str. 3.78 620 6 36 28'-6" Str. 15' 621 6 59 30'-3" Str. 2.66 622 6 178 30'-0" Str. 8.00 623 6 158 29'-9" Str. 7.06 624 6 110 29'-6" Str. 1.78 625 6 56 56 29'-3" Str. 2.46 626 6 411 29'-0" Str. 3.44 627 6 81 28'-9" Str. 3.44 628 6 188 31'-6" Str. 8.89 629 6 140 32'-0" Str. 8.89 630 6 69 32'-6" Str. 3.34 631 6 75 33'-3" Str. 3.34 632 6 36 33'-0" Str. 3.34 633 6 2 58' 8'-0" to 46'-0" Str. 32 633 6 2 8 11'-0" Str. 32 635 6 4 23'-0" Str. 32 636 6 95 28'-3" Str. 32 637 6 4 10'-0" Str. 66 638 6 2 22'-0" Str. 66 639 6 3 39'-0" Str. 66 640 6 2 27'-6" Str. 82 644 6 1 88'-3" to 38'-6" Str. 66 645 6 2 21'-0" Str. 66 646 6 2 38'-4" to 46'-5" Str. 66 647 6 1 38'-5" Str. 66 648 6 1 38'-3" to 38'-6" Str. 66 649 6 2 27'-6" Str. 66 649 6 2 27'-6" Str. 66 650 6 1 38'-3" to 38'-6" Str. 65 644 6 1 38'-3" to 38'-6" Str. 65 655 6 1 1 38'-3" Str. 65 656 6 1 1 38'-3" Str. 65 657 6 1 1 18'-3" Str. 65 659 6 1 1 16'-0" Str. 66 659 6 1 1 16'-0" Str. 65 659 6 1 1 18'-3" Str. 12.56	615	6	190	38'-0"	Str.			10,844
618 6 77 32'-9" Str. 3,78 619 6 36 28'-6" Str. 1,59 620 6 3 34'-0" Str. 2,68 621 6 59 30'-3" Str. 2,68 622 6 178 30'-0" Str. 3,02 623 6 158 29'-9" Str. 7,00 624 6 110 29'-6" Str. 4,88 625 6 56 29'-3" Str. 2,48 626 6 41 29'-0" Str. 1,78 627 6 81 28'-9" Str. 8,88 629 6 140 32'-6" Str. 6,74 630 6 69 32'-6" Str. 3,34 631 6 75 33'-3" Str. 3,34 633 6 2 58' 8'-0" Str. 3,34 633 6 2 58' 8'-0" Str. 3,74 634 6 2 11'-0" Str. 32 635 6 4 23'-0" Str. 33 637 6 4 10'-0" Str. 32 640 6 2 27'-6" Str. 66 638 6 2 22'-0" Str. 66 639 6 3 39'-0" Str. 13 640 6 2 27'-6" Str. 33 640 6 95 28'-3" Str. 13 640 6 2 27'-6" Str. 13 640 6 2 27'-6" Str. 15 640 6 2 27'-6" Str. 17 640 6 1 38'-6" Str. 17 640 6 2 27'-6" Str. 17 640 6 1 38'-6" Str. 17 640 6 1 38'-6" Str. 17 640 6 2 27'-6" Str. 17 640 6 1 38'-6" Str. 17 640 6 1 38'-6" Str. 18 640 6 1 38'-6" Str. 17 640 6 1 38'-6" Str. 17 640 6 2 27'-6" Str. 17 640 6 1 38'-6"	616	6	65	301-6"	Str.	•		2,978
619 6 36 28'-6" Str. 1,54 620 6 3 34'-0" Str. 15 621 6 59 30'-3" Str. 2,66 622 6 178 30'-0" Str. 8,02 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 2,46 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,75 627 6 81 28'-9" Str. 6,77 630 6 69 32'-6" Str. 6,77 631 6 75 33'-3" Str. 3,34 632 6 36 33'-0" Str. 3,36 633 6 2 56' 8'-0" to 46'-0" Str. 3,36 634 6 2 11'-0" Str. 33 635 6 4 23'-0" Str. 33 637 6 4 23'-0" Str. 33 638 6 2 22'-0" Str. 66 639 6 3 39'-0" Str. 66 639 6 3 39'-0" Str. 66 639 6 3 39'-0" Str. 7 644 6 1 38'-3" Str. 66 645 6 1 4 38'-3" Str. 56 656 6 1 5 6 5 6 5 6 5 6 5 6 6 5 6 6 6 6	617	6	l		Str.			27
620 6 3 34'-0" Str. 2,66 621 6 59 30'-3" Str. 2,66 622 6 178 30'-0" Str. 8,06 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,87 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,78 627 6 81 28'-9" Str. 8,49 628 6 188 31'-6" Str. 8,88 629 6 140 32'-0" Str. 6,77 630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 3,79 632 6 36 33'-0" Str. 3,79 633 6 2 56' 8'-0" to 46'-0" Str. 32 633 6 2 56' 8'-0" to 46'-0" Str. 32 634 6 2 11'-0" Str. 32 635 6 4 10'-0" Str. 6 636 6 95 28'-3" Str. 6 637 6 4 10'-0" Str. 6 638 6 2 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 6 640 6 2 22'-0" Str. 5 641 6 1 38'-3" Str. 5 642 6 1 38'-6" Str. 6 643 6 5 2 22'-0" Str. 6 644 6 5 2 22'-0" Str. 5 645 6 4 10'-0" Str. 6 646 6 95 38'-3" Str. 9 647 6 1 10'-0" Str. 9 648 6 1 1 34'-3" Str. 17 649 6 2 21'-0" Str. 17 649 6 1 1 34'-3" Str. 17 649 6 2 12'-0" Str. 17 649 6 1 1 16'-0" Str. 15 650 6 1 1 20'-9" Str. 17 651 6 1 15'-6" Str. 17 652 6 1 1 18'-3" Str. 17 653 6 1 1 18'-3" Str. 17 654 6 1 1 18'-3" Str. 17 655 6 1 1 18'-3" Str. 17 656 6 1 1 18'-3" Str. 17 657 6 1 1 18'-3" Str. 17 658 6 1 1 18'-3" Str. 19 659 6 1 1 18'-3" Str. 19 650 6 1 1 18'-3" Str. 19 651 6 1 118'-3" Str. 19 652 6 1 1 18'-3" Str. 19 653 6 1 1 18'-3" Str. 19 654 6 1 18'-3" Str. 19 655 6 1 18'-3" Str. 19 655 6 1 18'-3" Str. 19 656 6 1 18'-3" Str. 19 657 6 1 18'-3" Str. 19 658 6 1 18'-3" Str. 19 659 6 1 18'-3" Str. 19 650 6 1 18'-3" Str.	618	6	77	32'-9"	Str.			3,788
621 6 59 30'-3" Str. 2,68 622 6 178 30'-0" Str. 8,02 623 6 158 29'-9" Str. 7,00 624 6 110 29'-6" Str. 4,87 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,78 627 6 81 28'-9" Str. 8,88 628 6 188 31'-6" Str. 6,77 630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 3,37 632 6 36 33'-0" Str. 3,78 633 6 2 86 8 11'-0" Str. 32 633 6 2 86 8 11'-0" Str. 32 633 6 2 86 8 11'-0" Str. 32 634 6 2 11'-0" Str. 32 635 6 4 22'-0" Str. 6 636 6 95 28'-3" Str. 6 637 6 4 10'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 5 640 6 2 27'-6" Str. 8 641 6 1 88 6 2 22'-0" Str. 6 653 6 6 2 22'-0" Str. 6 646 6 2 86 34'-3" Str. 8 647 6 1 38'-6" Str. 8 648 6 1 1 38'-3" Str. 5 649 6 1 1 38'-6" Str. 8 649 6 1 1 6'-0" Str. 6 649 6 1 16'-0" Str. 6 649 6 1 16'-0" Str. 5 650 6 1 10'-0" Str. 6 651 6 1 15'-6" Str. 32 652 6 1 17'-6" Str. 32 653 6 1 15'-6" Str. 32 653 6 1 16'-0" Str. 32 654 6 1 16'-0" Str. 32 655 6 1 16'-0" Str. 32 656 6 1 16'-0" Str. 32 657 6 1 16'-0" Str. 32 658 6 1 16'-0" Str. 32 659 6 1 16'-0" Str. 32 650 6 1 16'-0" Str. 32 651 6 1 16'-0" Str. 32 652 6 1 7'-6" Str. 32 653 6 1 18'-3" Str. 32 653 6 1 18'-3" Str. 32 654 6 1 18'-3" Str. 32 655 6 1 18'-3" Str. 32	619	6	36	28'-6"	···			1,54
622 6 178 30'-0" Str. 7,06 623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,87 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,77 627 6 81 28'-9" Str. 8,88 629 6 140 32'-0" Str. 6,77 630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 3,74 632 6 36 33'-0" Str. 1,78 633 6 2 S	620	6			Str.			153
623 6 158 29'-9" Str. 7,06 624 6 110 29'-6" Str. 4,87 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,78 626 6 81 28'-9" Str. 3,44 628 6 188 31'-6" Str. 8,88 629 6 140 32'-0" Str. 6,72 630 6 69 32'-6" Str. 3,38 631 6 75 33'-3" Str. 3,74 632 6 36 33'-0" Str. 3,74 633 6 2 Set 8'-0" to 46'-0" Str. 32 633 6 2 Set 8'-0" to 46'-0" Str. 32 634 6 2 11'-0" Str. 32 635 6 4 23'-0" Str. 4,03 636 6 95 28'-3" Str. 4,03 637 6 4 10'-0" Str. 66 638 6 2 22'-0" Str. 66 639 6 3 39'-0" Str. 66 639 6 3 39'-0" Str. 5tr. 66 640 6 2 22'-6" Str. 5tr. 5,02 641 6 1 38'-3" Str. 5tr. 66 642 6 1 38'-3" Str. 5tr. 66 644 6 1 Set 34'-3" Str. 5tr. 66 645 6 1 38'-6" Str. 5tr. 5,02 646 6 1 Set 34'-0" to 38'-9" Str. 66 647 6 2 21'-0" Str. 5tr. 66 648 6 1 Set 34'-0" to 38'-9" Str. 66 649 6 1 16'-0" Str. 66 649 6 1 16'-0" Str. 66 650 6 1 120'-9" Str. 27 651 6 1 15'-6" Str. 27 652 6 1 7'-6" Str. 27 653 6 1 188'-3" Str. 22 655 6 1 18'-3" Str. 22	621	6	59		<del> </del>			2,68
624 6 110 29'-6" Str. 4,87 625 6 56 29'-3" Str. 2,46 626 6 41 29'-0" Str. 1,78 627 6 81 28'-9" Str. 3,49 628 6 188 31'-6" Str. 6,77 630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 3,79 632 6 36 33'-0" Str. 3,79 633 6 2 Seq. 8'-0" Str. 3,79 634 6 2 11'-0" Str. 32 635 6 4 23'-0" Str. 1,78 636 6 95 28'-3" Str. 13 637 6 4 10'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 5 640 6 2 27'-6" Str. 5 640 6 2 27'-6" Str. 6 641 6 1 Seq. 34'-3" Str. 5 642 6 1 38'-6" Str. 5 644 6 1 Seq. 34'-3" Str. 5 645 6 2 21'-0" Str. 6 646 6 2 Seq. 6" Str. 5 647 6 1 38'-6" Str. 5 648 6 1 Seq. 34'-3" Str. 5 649 6 1 38'-6" Str. 5 640 6 2 Seq. 6" Str. 6 641 6 1 Seq. 34'-3" Str. 5 642 6 1 38'-6" Str. 5 643 6 1 34'-3" Str. 5 644 6 1 Seq. 34'-0" Str. 6 645 6 2 12'-0" Str. 6 646 6 1 Seq. 34'-0" Str. 6 647 6 2 12'-0" Str. 6 648 6 1 Seq. 34'-0" Str. 6 649 6 1 16'-0" Str. 3 651 6 1 16'-0" Str. 3 652 6 1 7'-6" Str. 3 653 6 1 18'-3" Str. 2		i			i			8,02
625 6 56 29'-3" Str. 2.46 626 6 41 29'-0" Str. 1.78 627 6 81 28'-9" Str. 3.45 628 6 188 31'-6" Str. 6.72 630 6 69 32'-6" Str. 3.35 631 6 75 33'-3" Str. 3.74 632 6 36 33'-0" Str. 3.74 633 6 2 564 8'-0" to 46'-0" Str. 32 634 6 2 11'-0" Str. 32 635 6 4 23'-0" Str. 32 636 6 95 28'-3" Str. 4,03 637 6 4 10'-0" Str. 63 638 6 2 22'-0" Str. 63 639 6 3 39'-0" Str. 63 640 6 2 27'-6" Str. 66 640 6 2 27'-6" Str. 50 641 6 1 562 34'-3" Str. 50 642 6 1 38'-6" Str. 66 644 6 1 562 34'-3" Str. 66 645 6 2 21'-0" Str. 66 646 6 2 564 6'-0" Str. 66 647 6 1 562 34'-3" Str. 65 648 6 1 562 34'-3" Str. 65 649 6 1 1 6'-0" Str. 66 649 6 1 1 6'-0" Str. 66 649 6 1 1 6'-0" Str. 66 649 6 1 1 16'-0" Str. 66 650 6 1 1 16'-0" Str. 27 6650 6 1 1 16'-0" Str. 32 6651 6 1 16'-0" Str. 32 6652 6 1 7'-6" Str. 32 6653 6 1 18'-3" Str. 32 6654 6 1 16'-0" Str. 32 6655 6 1 18'-3" Str. 32 6656 6 1 18'-3" Str. 32 6656 6 1 18'-3" Str. 32 6657 6 1 18'-3" Str. 32 6658 6 1 18'-3" Str. 32 6659 6 1 18'-3" Str. 32 670 670 670 570 570 570 570 570 570 570 570 570 5	623	6	158	29'-9"	Str.			7,060
626 6 41 29'-0" Str. 1.78 627 6 81 28'-9" Str. 3.45 628 6 188 31'-6" Str. 6.72 630 6 69 32'-6" Str. 6.72 631 6 75 33'-3" Str. 3.79 632 6 36 33'-0" Str. 3.79 633 6 2 Seq. 8'-0" to 46'-0" Str. 3.6 634 6 2 11'-0" Str. 3.6 635 6 4 23'-0" Str. 13 636 6 95 28'-3" Str. 4.03 637 6 4 10'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 5 640 6 2 27'-6" Str. 8 641 6 1 Seg. 34'-3" to 38'-6" Str. 5 642 6 1 38'-6" Str. 5 644 6 1 Seg. 34'-3" Str. 6 645 6 1 38'-6" Str. 6 646 6 2 Seq. 6'-0" Str. 6 647 6 1 Seg. 34'-3" Str. 6 648 6 1 Seg. 34'-0" Str. 6 649 6 1 Seg. 34'-0" Str. 6 640 6 1 Seg. 34'-0" Str. 6 641 6 1 Seg. 34'-0" Str. 6 642 6 1 38'-6" Str. 5 643 6 1 38'-6" Str. 5 644 6 1 Seg. 34'-0" to 39'-0" Str. 6 645 6 2 12'-0" Str. 6 646 6 1 Seg. 36'-0" Str. 6 647 6 2 12'-0" Str. 6 648 6 1 Seg. 36'-0" Str. 6 649 6 1 16'-0" Str. 6 650 6 1 16'-0" Str. 32' 650 6 1 16'-0" Str. 32' 650 6 1 18'-3" Str. 32'	624	6	110	291-6"	Str.			4,874
627 6 81 28'-9" Str. 8.85 628 6 188 31'-6" Str. 6.85 629 6 140 32'-0" Str. 6.72 630 6 69 32'-6" Str. 3.36 631 6 75 33'-3" Str. 3.74 632 6 36 33'-0" Str. 3.75 633 6 2 Seq. 8'-0" to 46'-0" Str. 32 633 6 2 Seq. 8'-0" to 46'-0" Str. 32 635 6 4 23'-0" Str. 13 636 6 95 28'-3" Str. 63 637 6 4 10'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 6 640 6 2 27'-6" Str. 5 641 6 1 38'-6" Str. 5 642 6 1 38'-6" Str. 5 644 6 1 38'-3" Str. 6 644 6 1 38'-3" Str. 6 645 6 2 2 2'-0" Str. 6 646 6 2 Seq. 6'-0" to 39'-0" Str. 6 646 6 2 Seq. 6'-0" to 39'-0" Str. 6 647 6 2 12'-0" Str. 6 648 6 1 Seq. 16'-0" to 39'-0" Str. 6 649 6 1 16'-0" Str. 6 650 6 1 16'-0" Str. 22 6550 6 1 16'-0" Str. 25 6551 6 1 18'-3" Str. 22 6553 6 1 18'-3" Str. 3 6551 6 1 18'-3" Str. 3 6551 6 1 18'-3" Str. 3 6552 6 1 7'-6" Str. 3 6553 6 1 18'-3" Str. 3 6553 6 1 18'-3" Str. 3 6554 6 1 18'-3" Str. 3 6555 6 1 18'-3" Str. 3 6556 6 1 18'-3" Str. 3 657 6 1 18'-3" Str. 3 657 657 657 657 657 657 657 657 657 657	625	6	56	29'-3"	Str.			2,460
628 6 188 31'-6" Str. 6,886 629 6 140 32'-0" Str. 6,77 630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 3,74 632 6 36 33'-0" Str. 3,74 633 6 2 Set 8'-0" to 46'-0" Str. 32 633 6 2 Set 8'-3" Str. 33 635 6 4 23'-0" Str. 33 636 6 95 28'-3" Str. 4,03 637 6 4 10'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 5 640 6 2 27'-6" Str. 5 641 6 1 Set 34'-3" Str. 5 642 6 1 38'-6" Str. 5 644 6 1 38'-6" Str. 6 645 6 2 21'-0" Str. 6 646 6 2 Set 6'-0" to 39'-0" Str. 6 646 6 1 Set 6'-0" to 39'-0" Str. 6 647 6 1 Set 7'-6" Str. 3 648 6 1 Set 7'-6" Str. 3 649 6 1 16'-0" Str. 6 650 6 1 10'-0" Str. 6 651 6 1 15'-6" Str. 3 652 6 1 18'-3" Str. 3 653 6 1 18'-3" Str. 3 654 6 655 6 1 18'-6" Str. 3 655 6 1 18'-6" Str. 3 656 6 1 18'-6" Str. 3 657 657 658 6 1 18'-6" Str. 3 658 6 1 18'-6" Str. 3 659 6 1 18'-6" Str. 3 659 6 1 18'-8" Str. 3 659 6 1 18'-9" Str. 3 659 6 18'-9" Str. 3	626	6	41	29"-0"	Str.			1,786
629 6 140 32'-0" Str. 6,72 630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 1,78 632 6 36 33'-0" Str. 3,74 632 6 36 33'-0" Str. 3,24 633 6 2 Set 8'-0" to 46'-0" Str. 3,24 634 6 2 11'-0" Str. 3,24 635 6 4 23'-0" Str. 6,35 636 6 95 28'-3" Str. 6,33 637 6 4 10'-0" Str. 6,33 638 6 2 22'-0" Str. 6,33 640 6 2 22'-0" Str. 6,33 640 6 2 22'-0" Str. 6,33 640 6 2 27'-6" Str. 5,02 641 6 1 38'-6" Str. 5,02 642 6 1 38'-6" Str. 5,02 644 6 2 21'-0" Str. 6,04 645 6 2 21'-0" Str. 6,04 646 6 2 21'-0" Str. 5,02 647 6 2 21'-0" Str. 6,04 648 6 1 38'-6" Str. 2,7 649 6 1 16'-0" Str. 2,7 649 6 1 16'-0" Str. 3,7 649 6 1 16'-0" Str. 3,7 649 6 1 16'-0" Str. 3,7 655 6 1 15'-6" Str. 2,7 655 6 1 15'-6" Str. 2,7 655 6 1 18'-3" Str. 2,7 655 6 1 18'-3" Str. 2,7 655 6 1 18'-3" Str. 3,7 655 6 1 18'-3" Str. 2,7 655 6 1 18'-3" Str. 3,7 657 6 1 18'-3" Str. 3,7 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	627	6	81	28'-9"	Str.			3,498
630 6 69 32'-6" Str. 3,36 631 6 75 33'-3" Str. 3,74 632 6 36 33'-0" Str. 1,78 633 6 2 set 8'-0" to 46'-0" Str. 32 634 6 2 11'-0" Str. 32 635 6 4 23'-0" Str. 13 636 6 95 28'-3" Str. 4,03 637 6 4 1C'-0" Str. 66 638 6 2 22'-0" Str. 66 639 6 3 39'-0" Str. 66 639 6 3 39'-0" Str. 8 640 6 2 27'-6" Str. 8 641 6 1 38'-6" Str. 5 642 6 1 38'-6" Str. 5 644 6 1 34'-3" Str. 5 644 6 1 set 34'-3" Str. 64 645 6 2 2 1'-0" Str. 5 646 6 2 1'-0" Str. 5 647 6 2 12'-0" Str. 5 648 6 1 34'-3" Str. 66 649 6 1 16'-0" Str. 32 649 6 1 16'-0" Str. 32 650 6 1 15'-6" Str. 32 651 6 1 15'-6" Str. 32 653 6 1 18'-3" Str. 32 653 6 1 18'-3" Str. 32 655 6 1 7'-6" Str. 32 655 6 1 18'-3" Str. 32 655 6 1 18'-3" Str. 32 655 6 1 18'-3" Str. 32	628	6	188					8,895
631 6 75 33'-3" Str. 3,74 632 6 36 36 33'-0" Str. 1,78 633 6 2 Seq. 8'-0" to 46'-0" Str. 32 634 6 2 11'-0" Str. 33 635 6 4 23'-0" Str. 4,03 636 6 95 28'-3" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 6 639 6 3 39'-0" Str. 6 640 6 2 27'-6" Str. 38'-6" Str. 5 642 6 1 38'-3" Str. 5 644 6 1 Seq. 34'-3" Str. 5 644 6 1 Seq. 34'-3" Str. 5 644 6 1 Seq. 34'-0" Str. 6 645 6 2 21'-0" Str. 6 646 6 2 Seq. 6'-0" to 39'-0" Str. 6 647 6 2 12'-0" Str. 3 648 6 1 Seq. 31'-3" Str. 3 649 6 1 16'-0" Str. 3 650 6 1 20'-9" Str. 3 651 6 1 15'-6" Str. 3 652 6 1 7'-6" Str. 3 653 6 1 18'-3" Str. 2	629	6	140	32'-0"	Str.			6,729
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633	63 I	6	75	33'-3"	Str.			3,74€
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635 6 4 23'-0" Str. 13 636 6 95 28'-3" Str. 4,03 637 6 4 1C'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 17 640 6 2 27'-6" Str. 8 4	634							33
636 6 95 28'-3" Str. 4,03 637 6 4 1C'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 17 640 6 2 27'-6" Str. 8 41 6 Ser 34'-3" to 36'-6' Str. 5,02 642 6 1 38'-6" Str. 5 644 6 Ser 34'-0" to 38'-9" Str. 5 644 6 Ser 34'-0" to 38'-9" Str. 6 645 6 2 21'-0" Str. 6 646 6 Ser 6'-0" to 39'-0" Str. 6 647 6 2 12'-0" Str. 27 648 6 Ser 6'-0" to 39'-0" Str. 3 648 6 Ser 6'-0" to 39'-0" Str. 3 648 6 Ser 6'-0" to 39'-0" Str. 3 650 6 I Ser 6'-0" Str. 2 650 6 I Ser 6'-0" Str. 2 651 6 I Ser 6'-0" Str. 3 652 6 I 7'-6" Str. 2 653 6 I 18'-3" Str. 2								138
637 6 4 10'-0" Str. 6 638 6 2 22'-0" Str. 6 639 6 3 39'-0" Str. 17 640 6 2 27'-6" Str. 8 44 6 Str. 8 644 6 Str. 8 642 6 I 38'-3" to 38'-6' Str. 5 643 6 I 34'-3" Str. 5 644 6 Str. 5 644 6 Str. 6'-0" Str. 6 645 6 2 21'-0" Str. 6 646 6 Str. 6'-0" Str. 6 647 6 2 Str. 6'-0" Str. 6 648 6 Str. 8 649 6 I 16'-0" Str. 27 650 6 I 20'-9" Str. 3 651 6 I 15'-6" Str. 3 652 6 I 7'-6" Str. 2 653 6 I 18'-3" Str. 2			<del> </del>					4,031
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639 6 3 39'-0" Str. 17 640 6 2 27'-6" Str. 8  41 6 Sec 34'-3" to 38'-6 Str. 5,02  642 6 1 38'-6" Str. 5  643 6 1 34'-3" Str. 5  644 6 Sec 34'-0"to 38'-9" Str. 6  645 6 2 Sec 4 6'-0" to 39'-0" Str. 6  646 6 Sec 16'-0" to 39'-0" Str. 3  648 6 Sec 16'-0"to 20'-9" Str. 2,56  649 6 1 16'-0" Str. 2  650 6 1 20'-9" Str. 3  651 6 1 15'-6" Str. 3  653 6 1 18'-3" Str. 2		<del>                                     </del>	<del>                                     </del>					66
640 6 2 27'-6" Str. 88  44 6 Sec 34'-3" to 38'-6" Str. 5,02  642 6 1 38'-6" Str. 5  643 6 1 34'-3" Str. 5  644 6 Sec 34'-0"to 38'-9" Str. 6  645 6 2 21'-0" Str. 6  646 6 2 Sec 6'-0" to 39'-0" Str. 27  647 6 2 12'-0" Str. 3  648 6 Sec 3 16'-0"to 20'-9" Str. 2,56  649 6 1 16'-0" Str. 2  650 6 1 20'-9" Str. 2  652 6 1 7'-6" Str. 2  653 6 1 18'-3" Str. 2								176
41       6         Sec   34   -3" to 38   -6"   Str.         5,02         642       6       1       38   -6"   Str.         5         643       6       1       34   -3"   Str.         5         644       6         Sec   34   -0" to 38   -9"   Str.         5,02         645       6       2       2   1   -0"   Str.         6         645       6       2       2   1   -0"   Str.         27         646       6       2   2   -0"   Str.         27         647       6       2       12   -0"   Str.         3         648       6         Sec   16   -0"   Str.         2,56         649       6       1       16   -0"   Str.         2         650       6       1       20   -9"   Str.         3         651       6       1       15   -6"   Str.         2         652       6       1       7   -6"   Str.         1         653       6       1       18   -3"   Str.         2		1			1			83
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646 6 2 Set 6'-C" to 39'-O" Str. 27 647 6 2 12'-O" Str. 3 648 6   Set   16'-C"to 20'-9" Str. 2,56 649 6   16'-O" Str. 2 650 6   120'-9" Str. 3 651 6   15'-6" Str. 2 652 6   7'-6" Str. 1 653 6   18'-3" Str. 2			92	34'-0"to38'-9"	Str.			
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648 6   Ser   16'-C"to2C'-9"   Str.   2,56 649 6   16'-0"   Str.   2 650 6   120'-9"   Str.   3 651 6   15'-6"   Str.   2 652 6   7'-6"   Str.   1 653 6   18'-3"   Str.   2					1			270
649 6   1   16'-0"   Str.   2   2   2   2   2   2   2   2   2			2	12'-0"	Str.			36
650 6 1 20°-9" Str. 3 651 6 1 15°-6" Str. 2 652 6 1 7'-6" Str. 1 653 6 1 18°-3" Str. 2	648	6	38			*		2,567
651 6 1 15'-6" Str. 2 652 6 1 7'-6" Str. 1 653 6 1 18'-3" Str. 2	649	6	1	16'-0"	Str.			24
652 6 1 7'-6" Str. 1 653 6 1 18'-3" Str. 2	650	6	1	20+-9*	Str.			31
652 6 1 7'-6" Str. 1 653 6 1 18'-3" Str. 2	651	6	1	15*-6*	Str.			23
653 6   18'-3" Str. 2			i		7			11
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FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	120
2	оню			122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT







BENDING DIAGRAMS

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42 R-17 5 DECK SLAB

REINFORCEMENT SCHEDULE

CUYAHOGA COUNTY CLEVELAND scale *None* made*R.K.* date 2-25-54

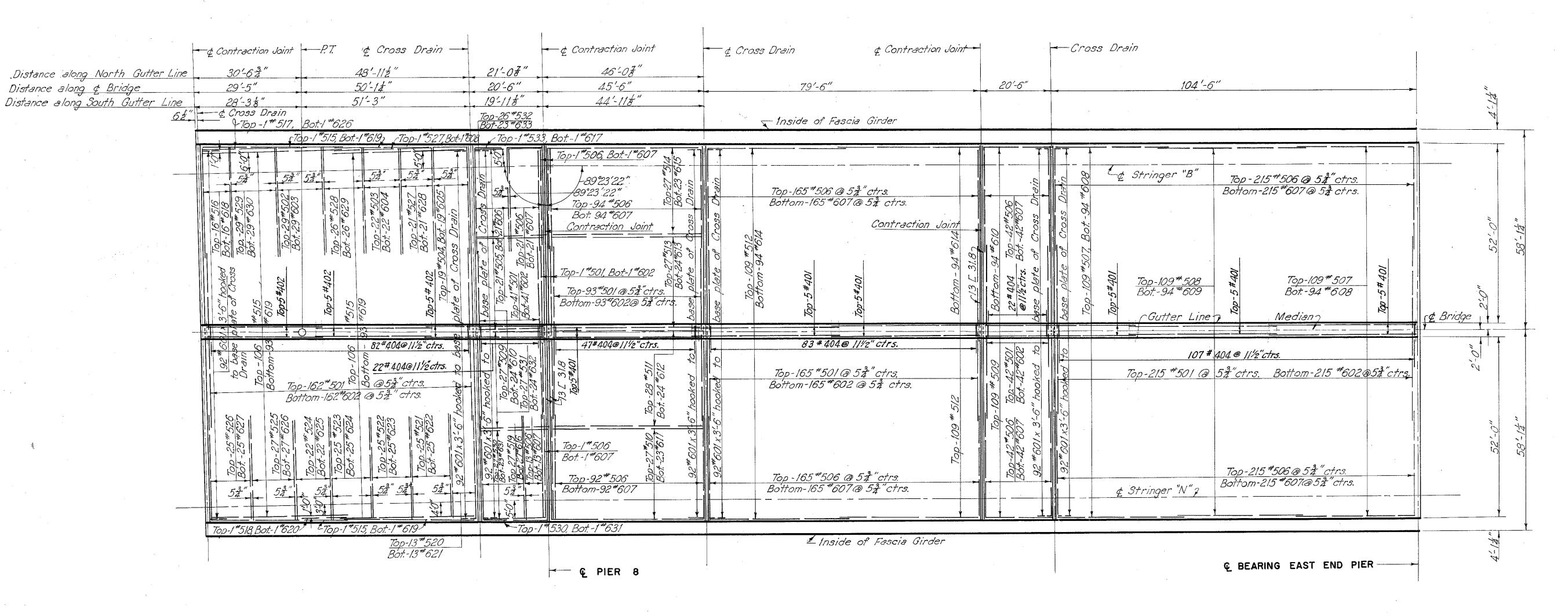
HOWARD, NEEDLES, TAMMEN & BERGENDOFF

TRCD DATE SATE 923-54 KANSAS CITY CLEVELAND NEW YORK 914-14 SHEET 2.120

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FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	119
2	оню	458 1 <u>1</u>		12:

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT



SLAB PLAN - UNIT 9

All longitudinal bars are to be parallel to stringer except bars at the edges of slab which are parallel to gutter lines. For spacing of longitudinal bars, see Typical Section, Sheet.

All transverse bars are to be normal to stringer and at 5% "ctrs. except extra bars parallel to edge of joints and cross drains. Top transverse are to be spliced at mid-point between Stringers "E" and "F" and Stringers "J" and "K". Bottom transverse bars are to be spliced over Stringer "E" and

For Details of Contraction Joint, see Sheet 114 For Reinforcing Steel Schedule, see Sheet 121. For Details of Cross Drain, See Sheet 105

Stringer "K"

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42R - 17.5

SLAB PLAN

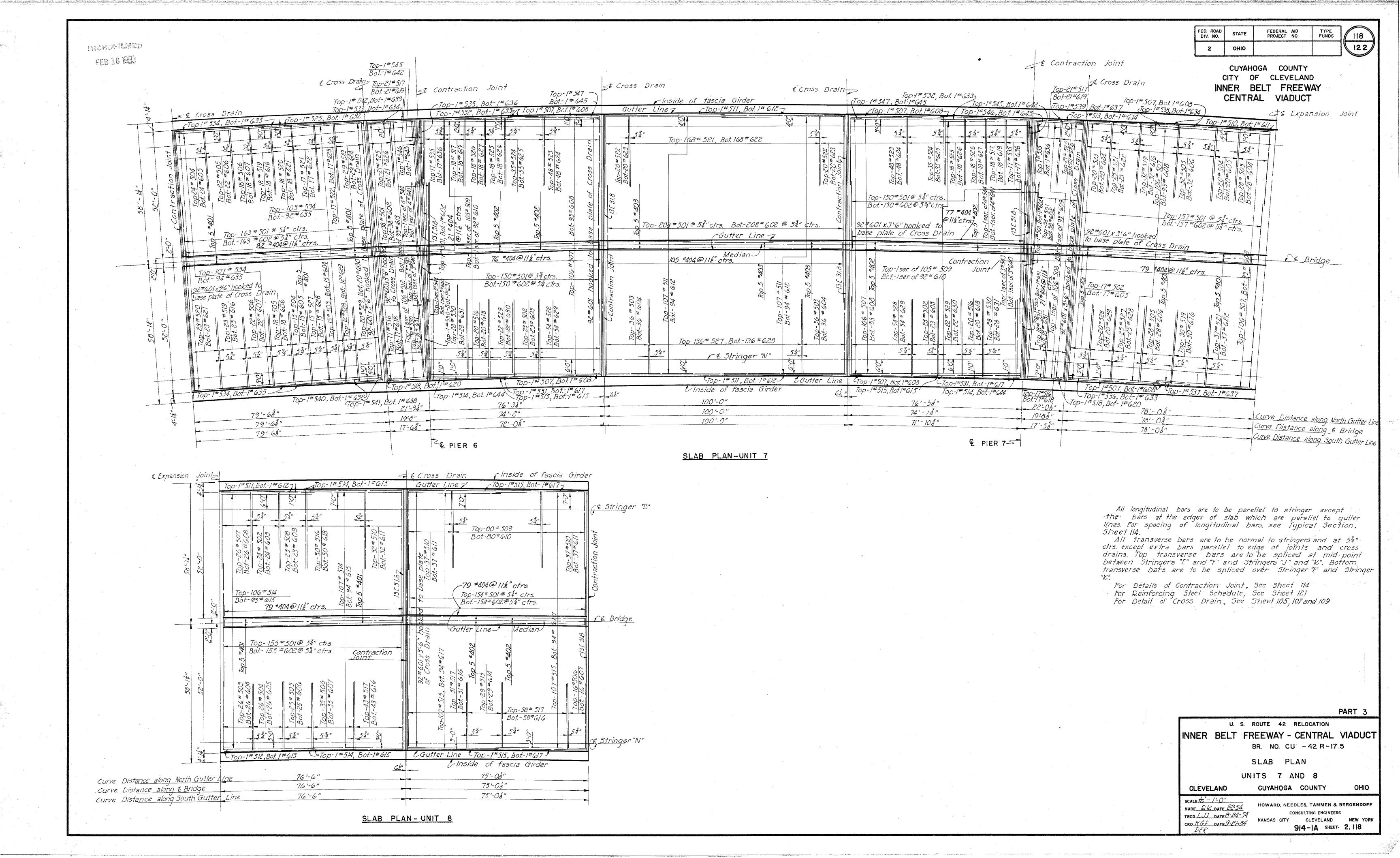
UNIT 9

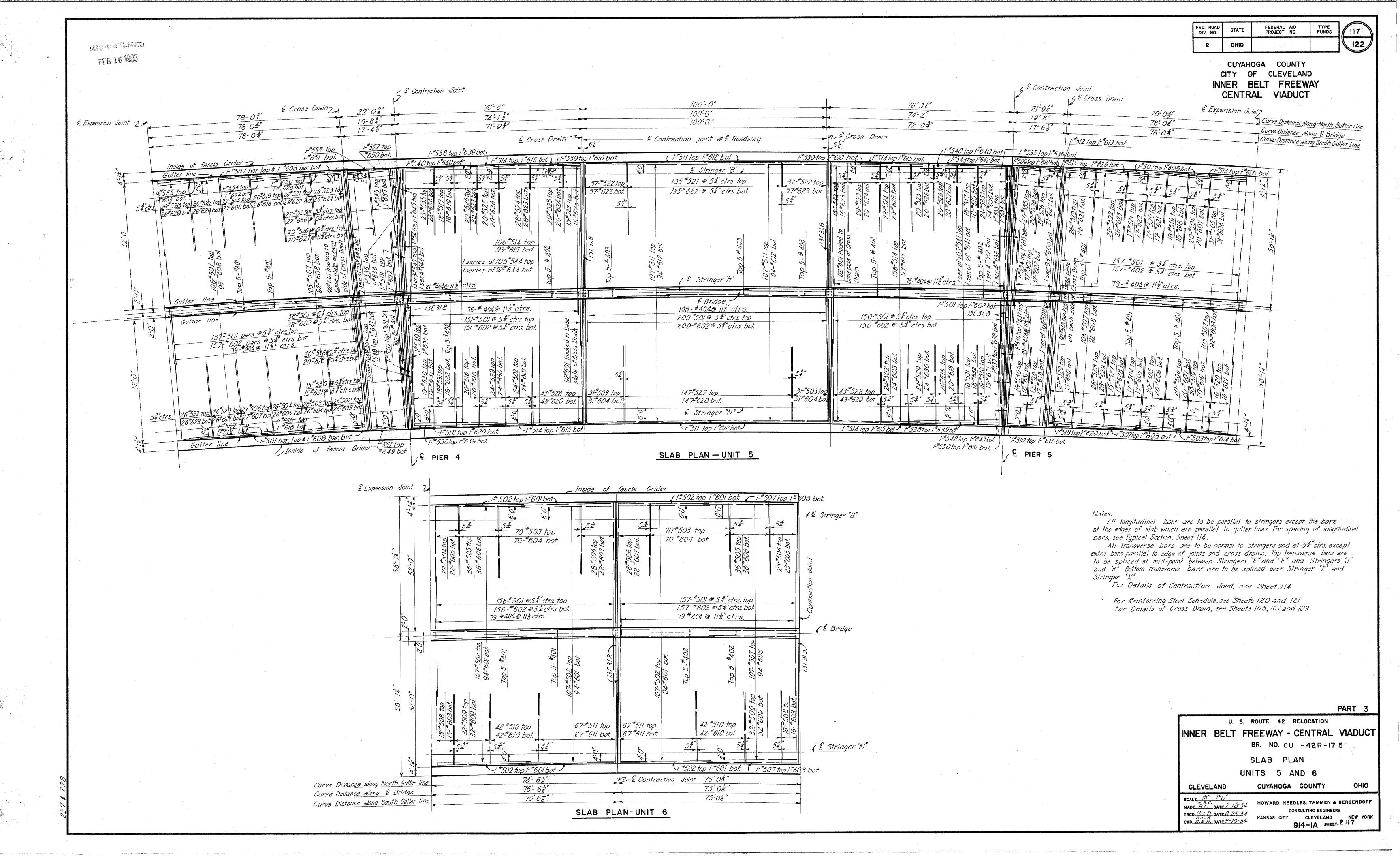
CUYAHOGA COUNTY

SCALE 16 = 1'-0" HOWARD, NEEDLES, TAMMEN & BERGENDOFF KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET 2.119

MADE R.K. DATE 2-4-54 TRCD<u>BMO</u> DATE 8-26-54 CKD BEE DATE 9-1/-54

CLEVELAND



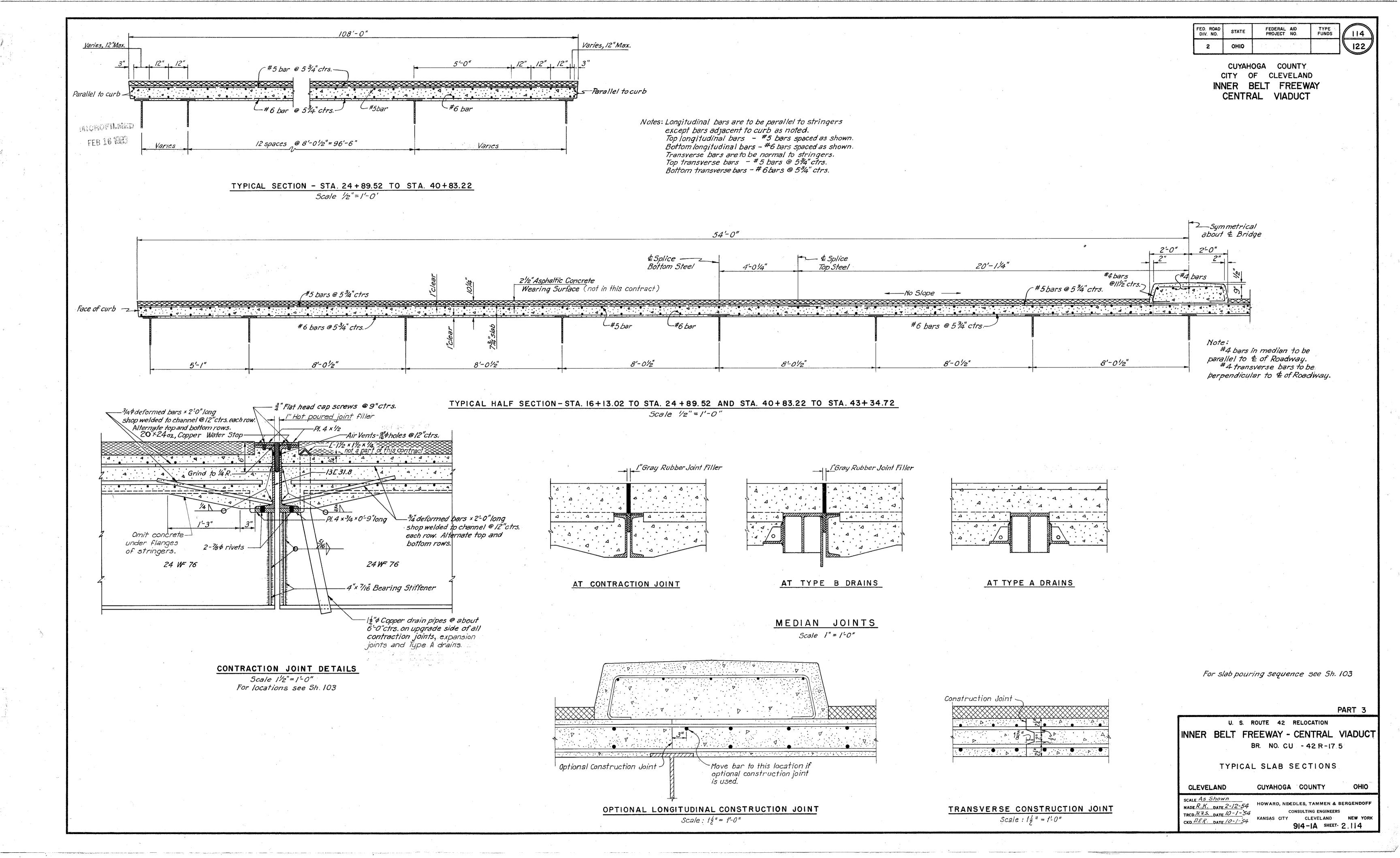


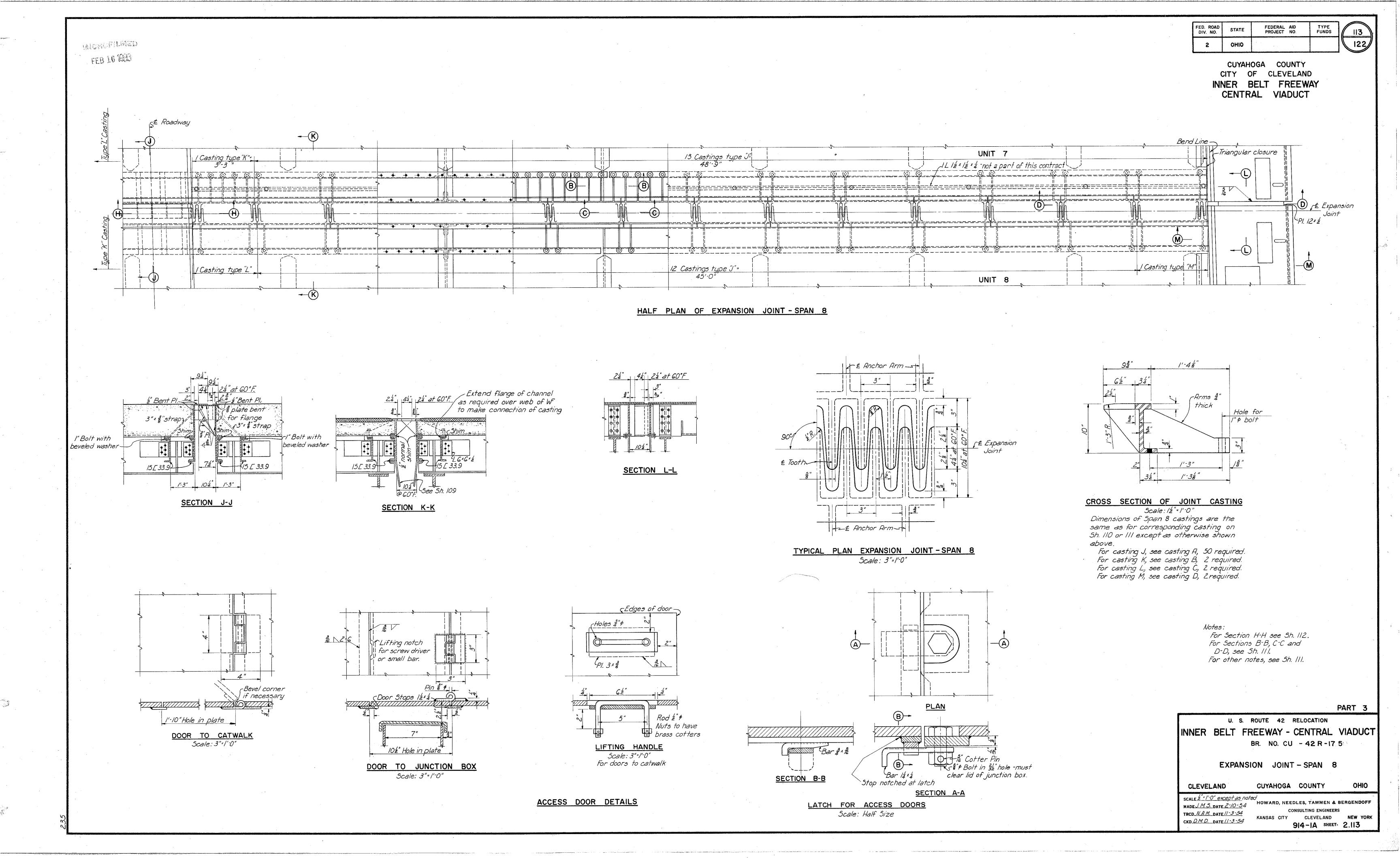
FED. ROAD DIV. NO. TYPE FUNDS FEDERAL AID PROJECT NO. 116 MICROPILMED 122 OHIO FEB 16 (88) CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT 75'-6" 21'-0<del>8</del>" 79′-6±″ Distance along North Gutter Line 20'-6" 78'-0" 100'-0" 75'-0" 20'-6" *75'-0"* 79'-6±" Distance along & Bridge  $19'-1/\frac{7}{8}"$ 74'-6" Distance along South Gutter Line 79'-6<del>‡</del>" *⊈ Contraction Joint* <u>¢ Contraction Joint</u> ¢ <u>Contraction Joint</u> Inside of Fascia Girder 7 € Contraction Joint 2- & Cross Drain (1-#516 bar top and 1-#616 bar bot.) 1-#522 top, 1-#623 bot. Gutter lines € Stringer "B" 1-#519 top 1-#619 bot. | 154-#519 bars @5¾" ctrs. top | 154-#619 bars @5¾" ctrs. bot. 54-#509 top. | 56-#510 top | 54-#511 top | 54-#611 bot. 41-#501 bars @53" ctrs. top 41-#601 bars @53" ctrs. bot | 154 Lines of 2-#519 bars and 1-#501 bar @ 5¾" ctrs. top | 209 Lines of 2-#519 bars and 1-#501 bar @ 5¾" ctrs. top | 209 Lines of 2-#619 bars and 1-#601 bar @ 5¾" ctrs. bot. | 209 Lines of 2-#619 bars and 1-#601 bar @ 5¾" ctrs. bot. 157 Lines of 2-4519 bars and 1-4501 bar @ 53 ctrs. top | 153-#50| bars @ 5½ ctrs. top | 153-#60| bars @ 5½ ctrs. bot. 164-#501 bars @ 53 "ctrs. top 164-#601 bars @ 53"ctrs. bot. 157 Lines of 2-#619 bars and 1-#601 bar @ 53 ctrs. bot. 78 - # 404@//2"ctrs 80 - #404@11/2" ctrs. 106 - #404 @ 11/2" ctrs. 77-#404@11½" ctrs. |-#601 bot. -88°-55'-54" Gutter line > ¢ Bridae-1°-04'-06'' <u>& Bridge</u> -\$3 # 404@ 11/2"ctrs. Gutter line -88°-55'-54" -\ 42 Lines of 2-3 #519 bars and 89°27'57" 22-#404@11/2"ctrs. 92-#620x3'-6" hooked to base plate of Cross Drain 5 | 1#50| bar@53" ctrs. top

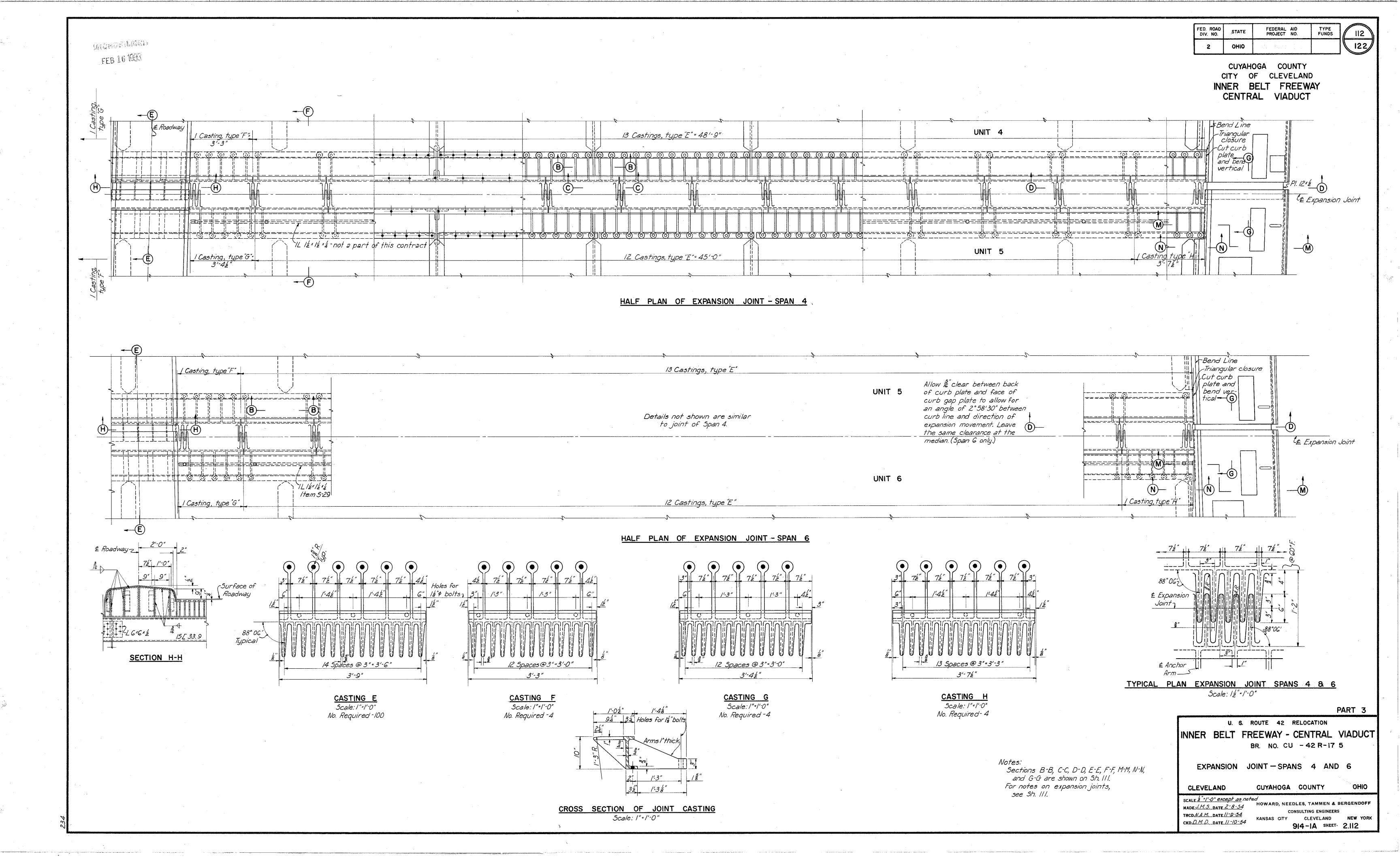
6 | 42 Lines of 2
#6/9 bars and 13 <u>E 31.8</u> 0 5 V-#601 bar@53" ctrs. bot. 56-#513 top 56-#613 bot. 1-#619 bot. . | 152-#519 bars @5¾ "ctrs. top | 152-#619 bars @5¾ "ctrs. bot. 54-#512 top 54-#612 bot. 54-#614 bot. r£ Stringer "N" 55 / line as : 1-#508 top, 1-#608 bot. 1-#516 bar top and 1-#616 bar bot. -6 Gutter line-¢ Cross Drain 62" 6 ½" • £ Cross Drain Inside of Fascia Girder © Cross Drain 62 Contraction Joint ~ PIER 2 ~\_ L PIER 3 250'-0" at & Bridge 2-£ Expansion joint SLAB PLAN-UNIT 3 /Inside of Fascia Girder Cross Drain - & Contraction Joint 2-PC Sta. 26+10.1210 & Contraction Joint \* £ Expansion Joint 11-#508 bar, top and 1-#608 bar, bot. #510 top \$ #610 bot. 1-#509 bar, top and 1-#609 bar, bot. > Notes: All longitudinal bars are to be parallel to stringers Gutter line except the bars at the edges of slab which are parallel #5/2 top \$ #6// bot. to gutter lines. For spacing of longitudinal bars, see Typical Section, Sheet 114. £ Stringer "B" All transverse bars are to be normal to stingers and at 5% ctrs. except extra bars parallel to edges of joints | 103-#502 bars @ 5¾" ctrs. top | 103-#504 bars @ 5¾" ctrs. top | 69-#504 bars @ 5¾"ctrs. top | 69-#506 bars @ 5¾"ctrs. top | 69-#604 bars @ 5¾"ctrs. bot. and cross drains. Top traverse bars are to be spliced at mid-point between Stringers "E" and "F", and Stringers "J" and "K". Bottom transverse bars are to be spliced over Stringer "E" and Stringer "K". For Contraction Joint Detail, see Sheet 114 For Cross Drain Details, see Sheets 105, 107 and 109 206-#501 bars @ 5¾"ctrs.top 206-#601 bars @ 5¾"ctrs.bot. For Reinforcement Schedule, see Sheet 120 208-#501 bars @5¾"ctrs. top 208-#601 bars @ 5\(\frac{2}{4}\)"ctrs.bot. +88°55'-54" 104- # 404 @ 11/2"ctrs. ~~88°-55'-54" 105-#404 @ 11/2" ctrs. 88°-55'-54" Tangent to & Roadway Gutter line~ 1°-04'-06" LE Stringer "H" Gutter line 69-#507 bars @5\$"ctrs. top 69-#607 bars @ 53 "ctrs.bot. PART 3 8 69-\*505 bars @ 5¾"ctrs. top 70-\*503 bars @ 5¾"ctrs. top 69-\*605 bars @ 5¾"ctrs. bot. 70-\*603 bars @ 5¾"ctrs. bot. U. S. ROUTE 42 RELOCATION #605 bars @ 53 "ctrs. " 6. INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R-17, 5 SLAB PLAN #511 top \$ 610 bot. -1-#509 bar top and 1-#609 bar bot. 2 UNITS 3 AND 4 Distance along North Gutter Line 19-68" 80'-5<del>4</del>" 101'-64" CUYAHOGA COUNTY CLEVELAND 1-5/3 top. 79′-5<u>‡</u>″ Distance along & Bridge 101'-64" SCALE 16 "= /-0" 1-612 bot. HOWARD, NEEDLES, TAMMEN & BERGENDOFF 78′-5″ Distance along South Gutter Line 21'-78" 101'-64" MADE WBC DATE 1-29-54 CONSULTING ENGINEERS TRCD JAV DATE 8-24-54
CKD D. E. R. DATE 9-10-54 CLEVELAND NEW YORK SLAB PLAN - UNIT 4 914-1A SHEET- 2.116

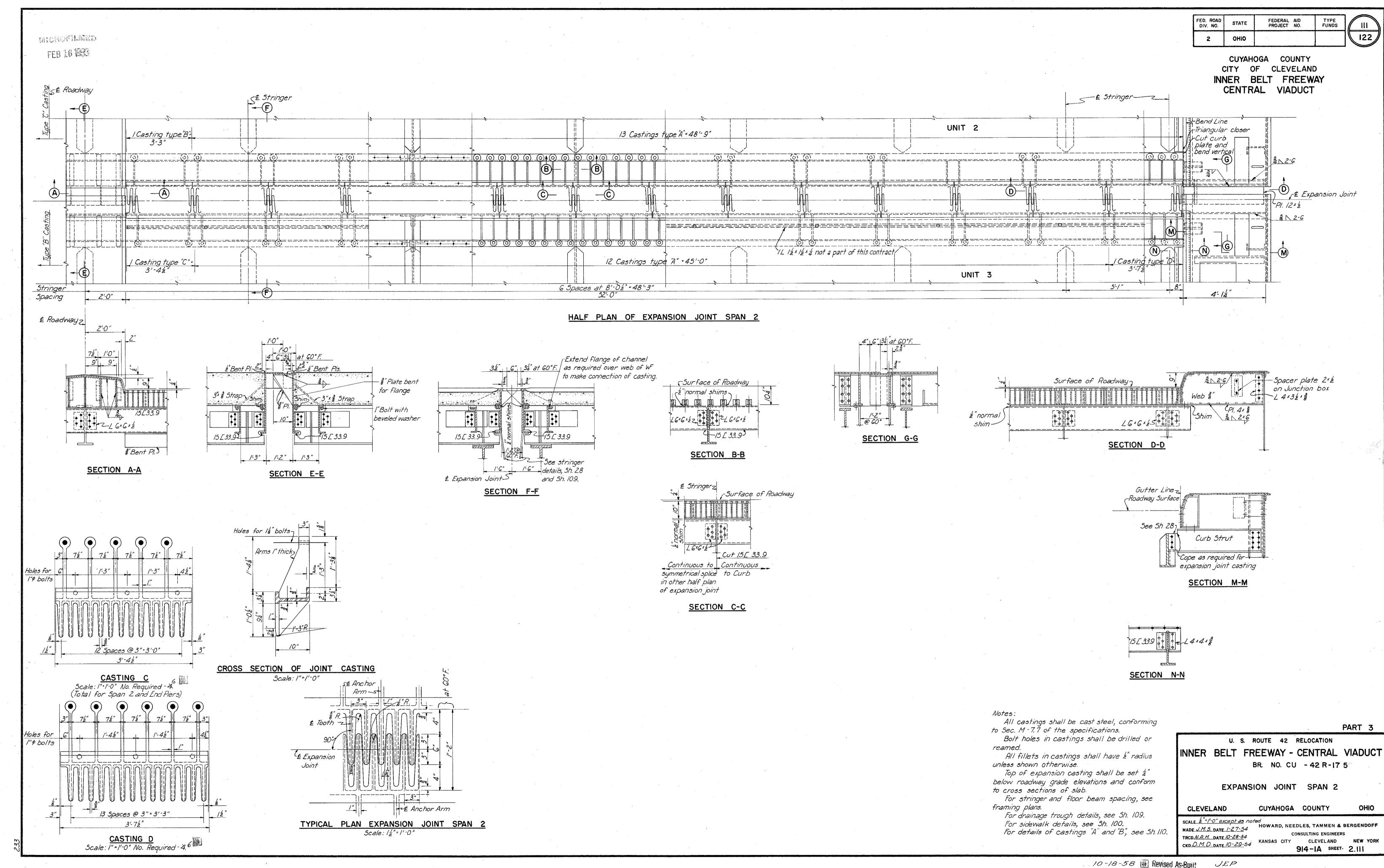
FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. TYPE FUNDS STATE 122 MOROFILMED & Cross Drain Cross Drain - ¢ Cross Drain OHIO FEB 16 PASS 20'-6" 79'-6" 104'-6" 54'-6" 45'-6" CUYAHOGA COUNTY & Cross Drain \_\_\_\_\_62" CITY OF CLEVELAND INNER BELT FREEWAY Gutter Line-CENTRAL VIADUCT Contraction Joint-Top-163 #506@ 5¾"ctrs. Bot.-163 #607@ 5¾"ctrs. -Contraction Joint Top-42#506 Bot.-42#607 Top-215 #506@ 5¾" ctrs. Bottom-215 #607@ 5¾" ctrs. Top-94#506 Bot.-94#607 Top-113#506@5\\delta\ctrs.
Bot:-113#607@5\\delta\ctrs. Top-163 #501 @ 5\frac{2}{3}" ctrs. Bot.-163 #602@ 5\frac{2}{3}" ctrs. Top-109#507 Bot: -94#608 Top-109# 508 Bot:-94#609 Top-113#501@54"ctrs. Bot:-113#602@54"ctrs. 82-#404@11/2"ctrs. Top-94#501@5¾"ctrs. Bot.-94#602@5¾"ctrs. 108-# 404@ 11/2" ctrs. <sup>4</sup>Gutter Line → ←Median Top-109#507 Bot.-94#608 Top 215 #501 @ 5¾ "ctrs. Bottom-215#602 @ 5¾ "ctrs. Top-215 #506 @ 5¾"ctrs. Bottom-215 #607 @ 5¾"ctrs. Top-163 #506 @ 5¾ ctrs. Bot.-163 #607 @ 5¾ ctrs. Top-113#506@ 5\(\frac{2}{3}\)"ctrs.
Bot.-113#607@5\(\frac{2}{3}\)"ctrs. Gutter Line 1 Inside of Fascia Girder Top-42 # 506 Bot:-42 # 607 Top-42#506 Bot:-42#607 - C BEARING WEST END PIER ¢ PIER I ---SLAB PLAN - UNIT I # Expansion Joint 201'-6" 100'-0" 101'-6" 4 Cross Drain 62" Inside of Fascia Girder-Gutter Line All longitudinal bars are to be parallel to stringers except bars at edges of curved portion of slab which are parallel to gutter line. For spacing of longitudinal bars, see Typical Section Sheet 114. Top-206 #504 @ 5¾ " ctrs. Bot.-206 #604 @ 5¾ " ctrs. Top-208#504 @ 5¾ " ctrs. Bot:-208#604 @ 5¾ " ctrs. All transverse bars are to be normal to & Bridge and at 5% ctrs. Top transverse bars are to be spliced at mid-point between Stringers "E" and "F" and Stringers "U" and "K". Bottom transverse bars are to be spliced over Stringer "E" and --- Contraction Joint Stringer "K"
For Contraction Joint Detail, see Sheet 114 For Cross Drain Details, see Sheets 105, 107 and 109. For Reinforcement Schedule, see Sheet 120. 105 - # 404@ 11/2" ctrs 104 - # 404 @ 11/2"ctrs. Gutter Line-& Bridge 7 Median →
Top-208#501@ 5¾"ctrs.

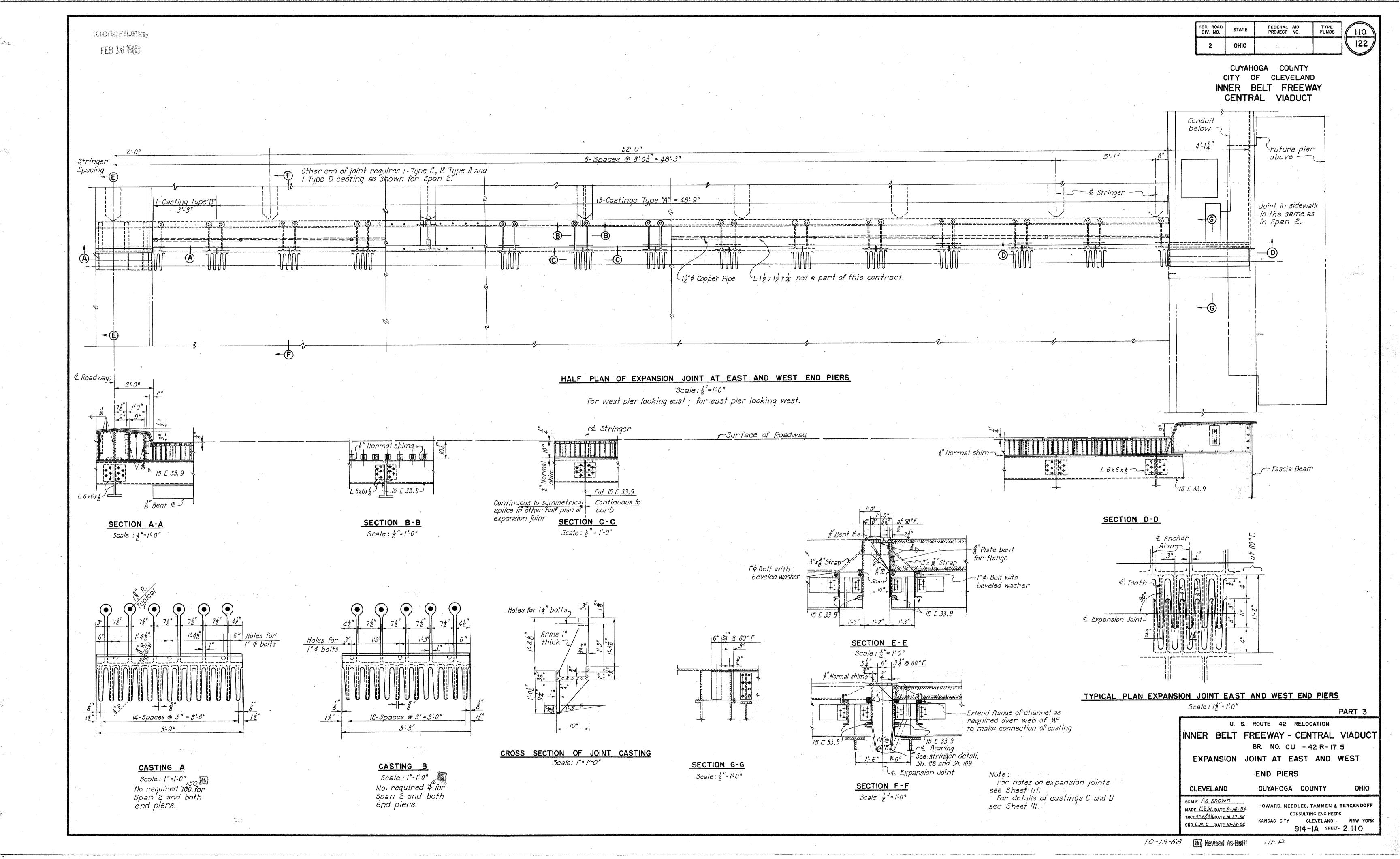
Bot: -208#602@5¾"ctrs. Top-206#501 @ 54" ctrs. Bot.-206#602 @ 54" ctrs. Top-206 #504 @ 5¾" ctrs. Bot.-206 #604 @ 5¾" ctrs. Top-208 #504 @ 5¾" ctrs. Bot:-208 #604 @ 5¾" ctrs. PART 3 U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R - 17.5 SLAB PLAN Gutter Line UNITS | AND 2 Linside of Fascia Girder CLEVELAND CUYAHOGA COUNTY SLAB PLAN - UNIT 2 SCALE 16 "= 1'-0" HOWARD, NEEDLES, TAMMEN & BERGENDOFF MADE R.K. DATE 1-22-54 trcd<u>8M0</u> date 8-19-54 ckd 8E2 date 9-9-54 KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET- 2.115

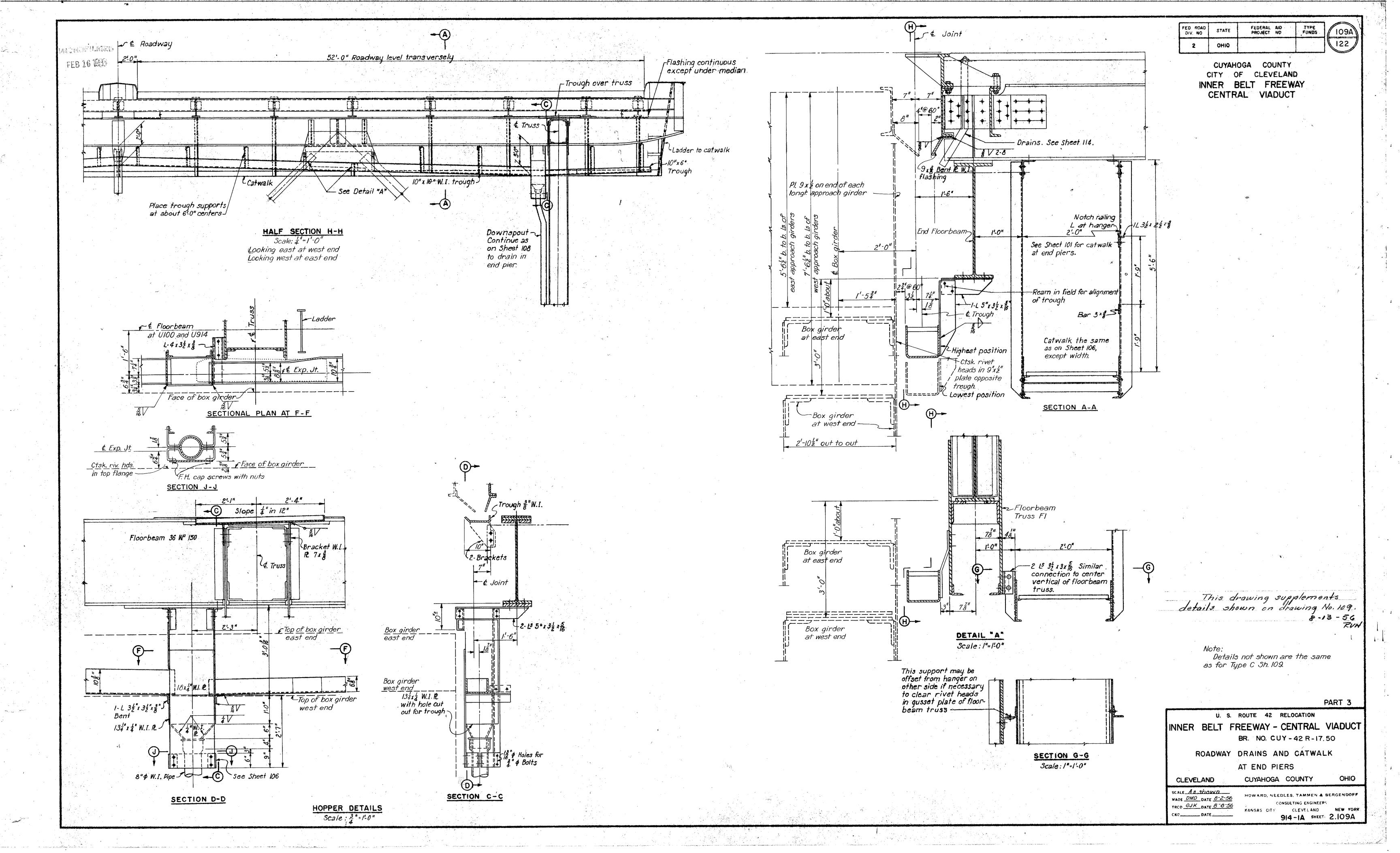


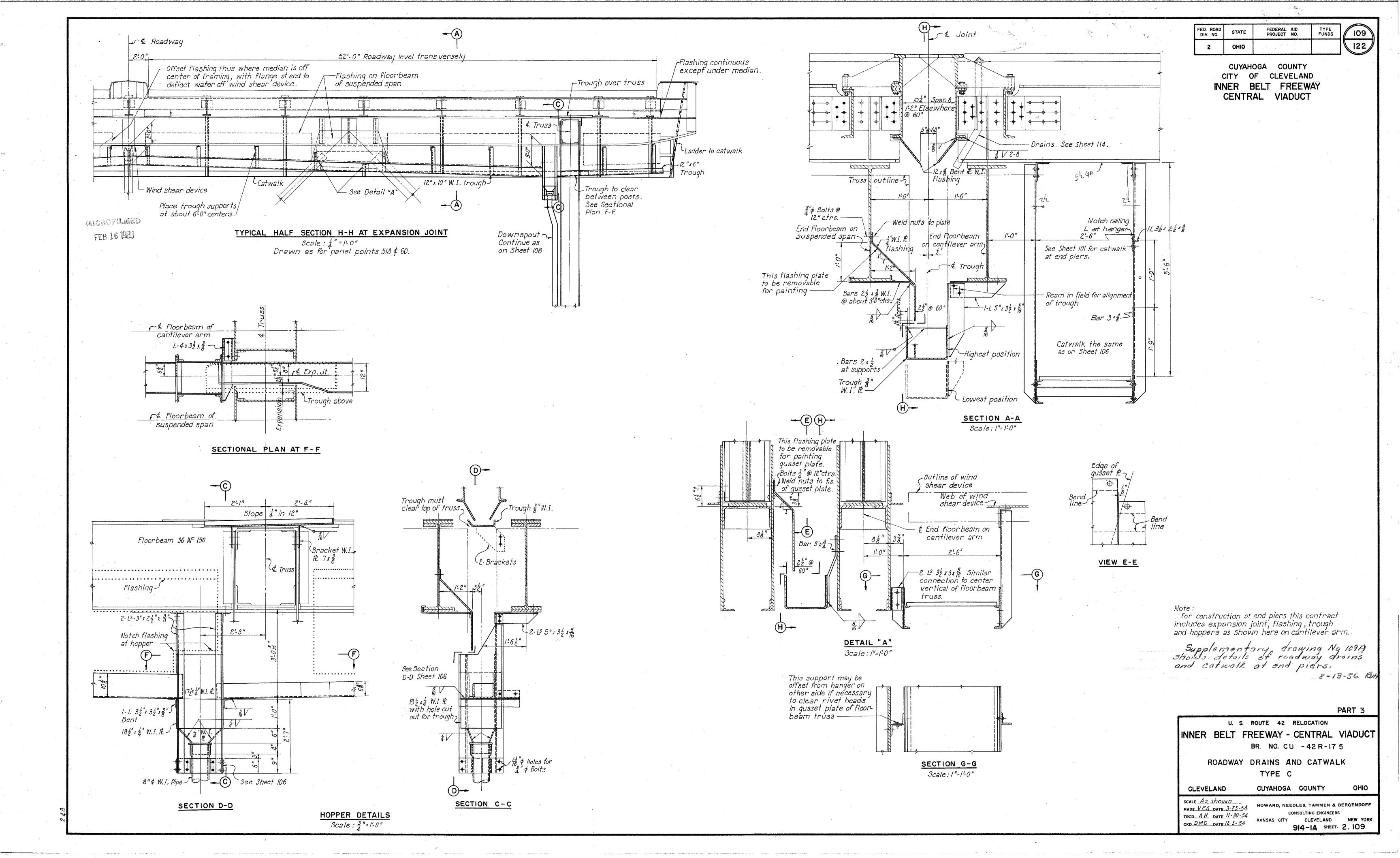


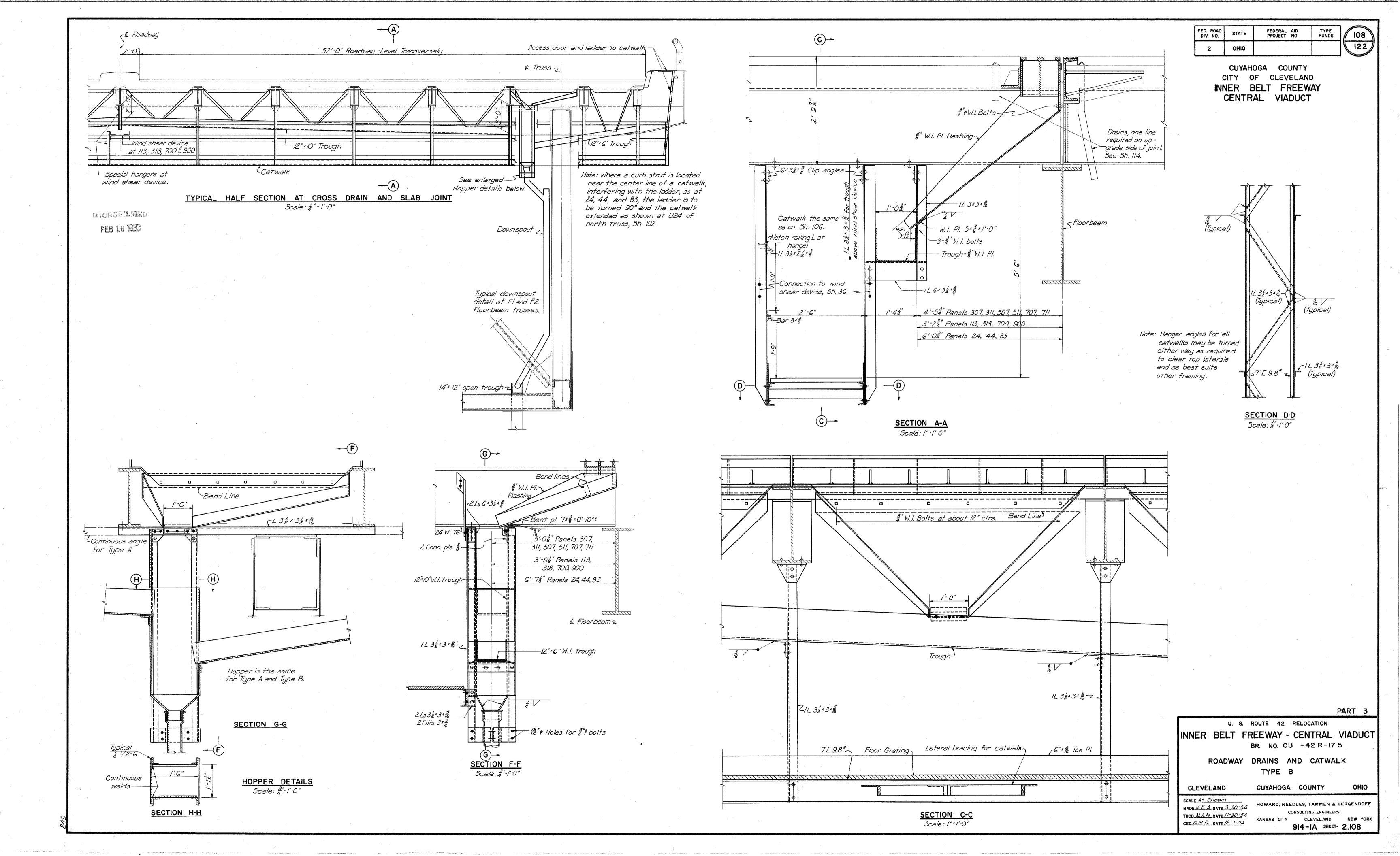


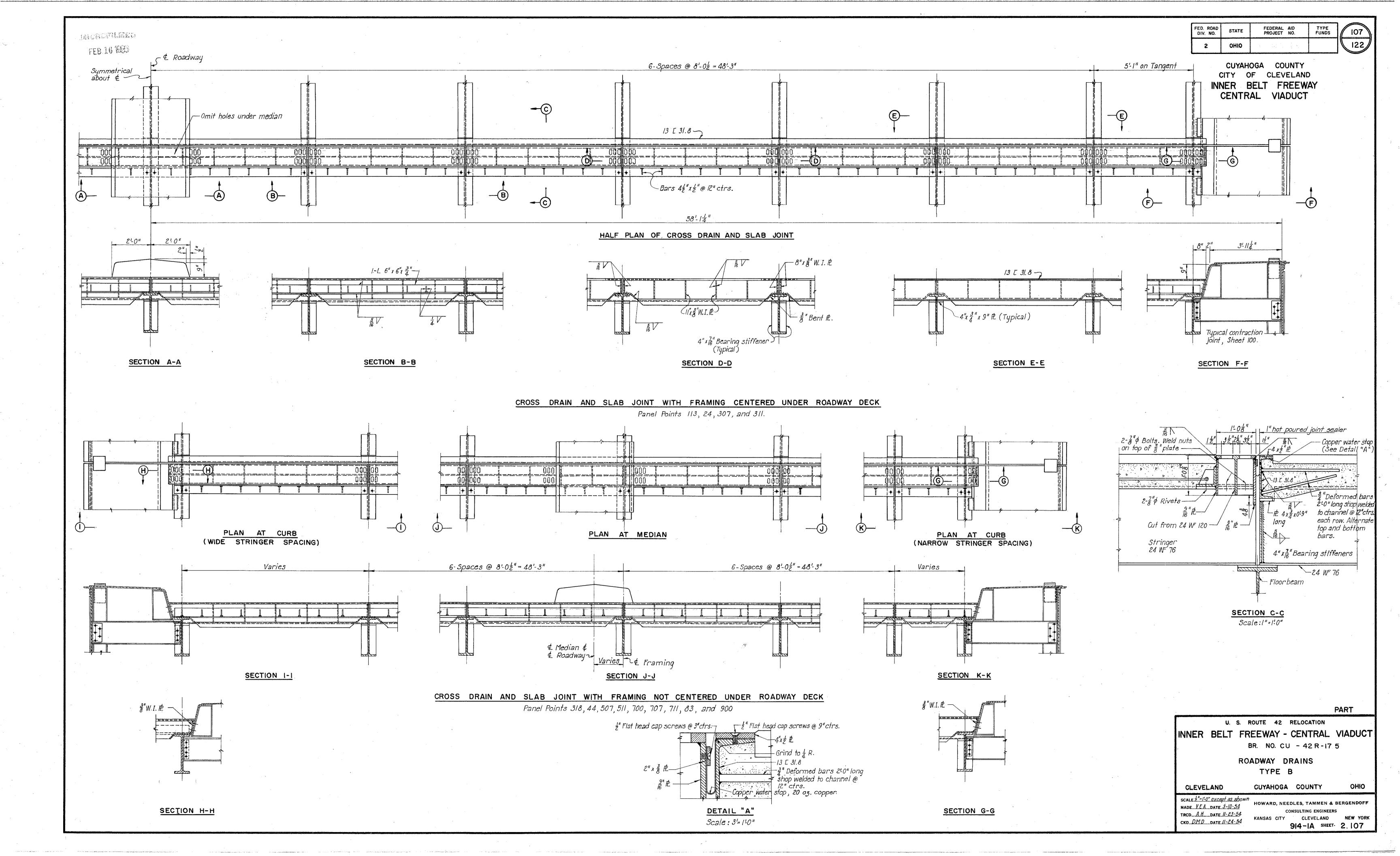


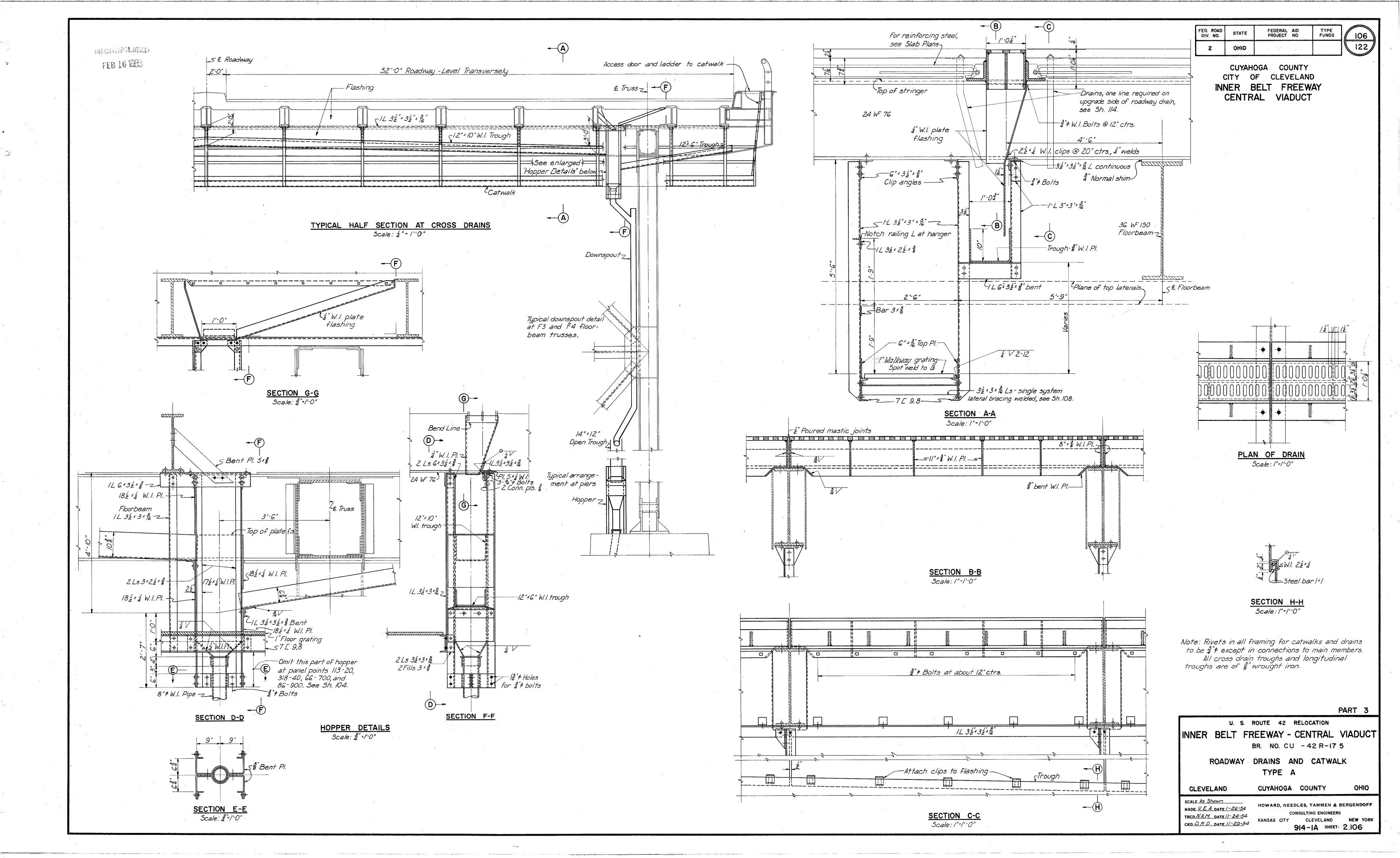


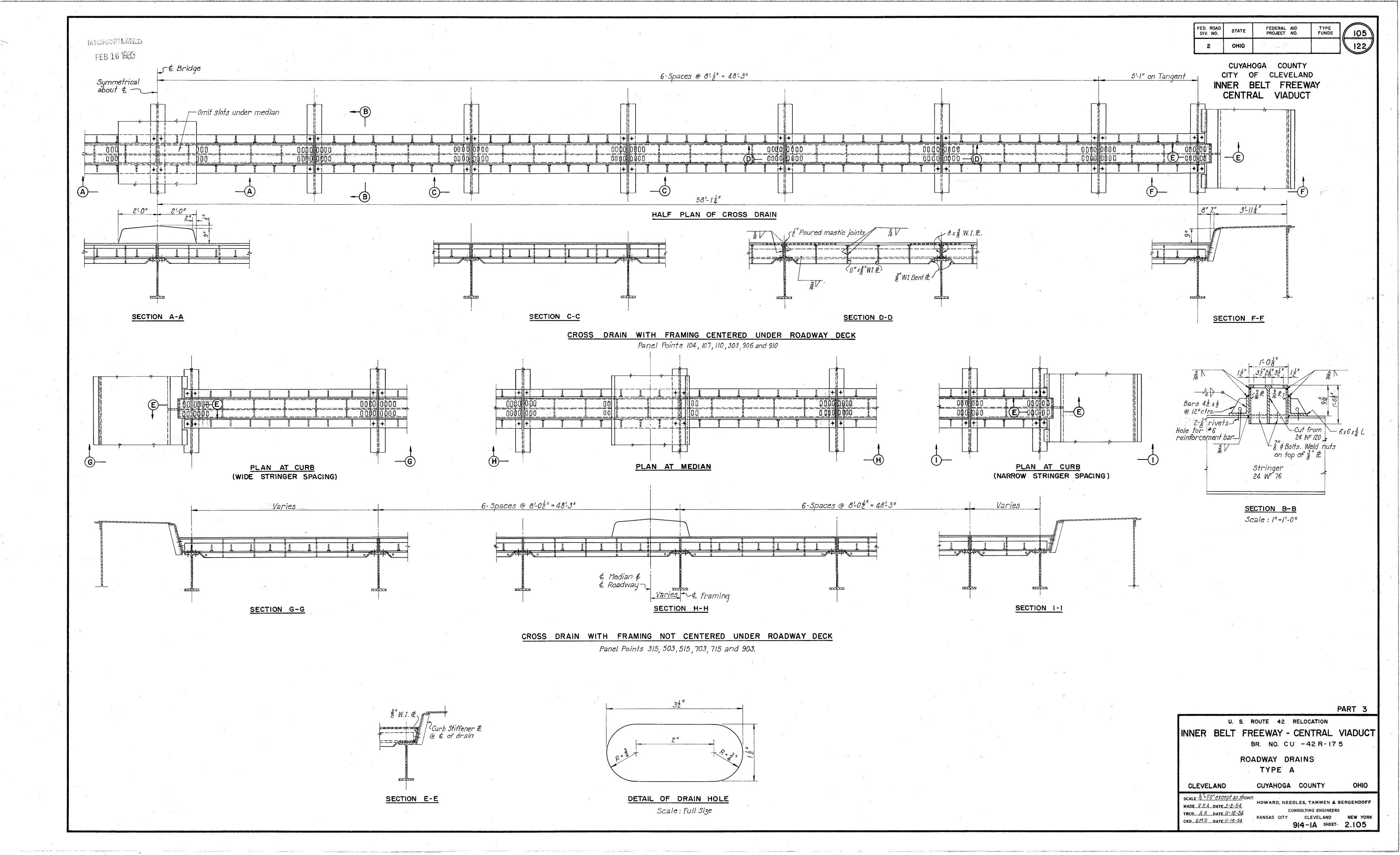


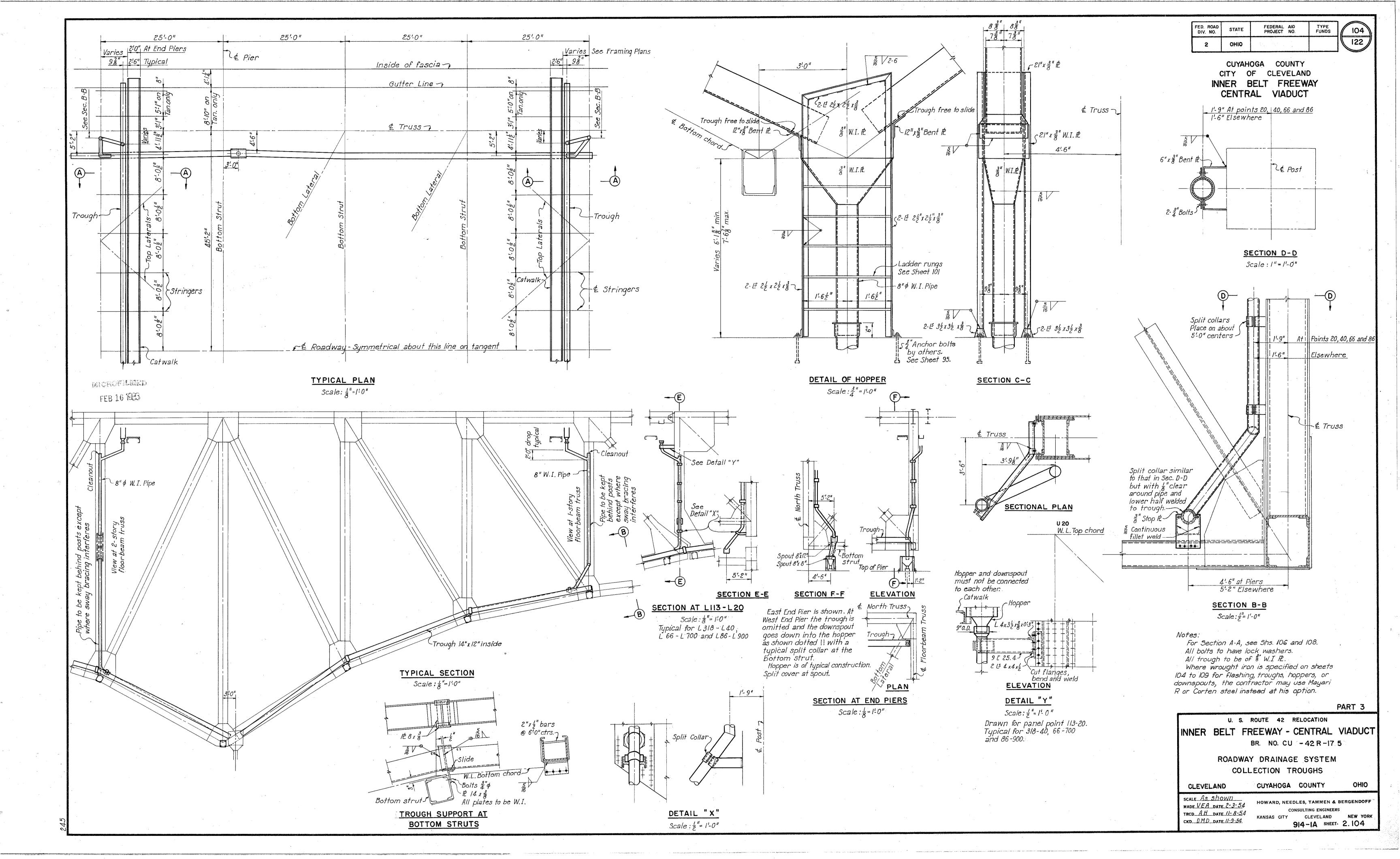


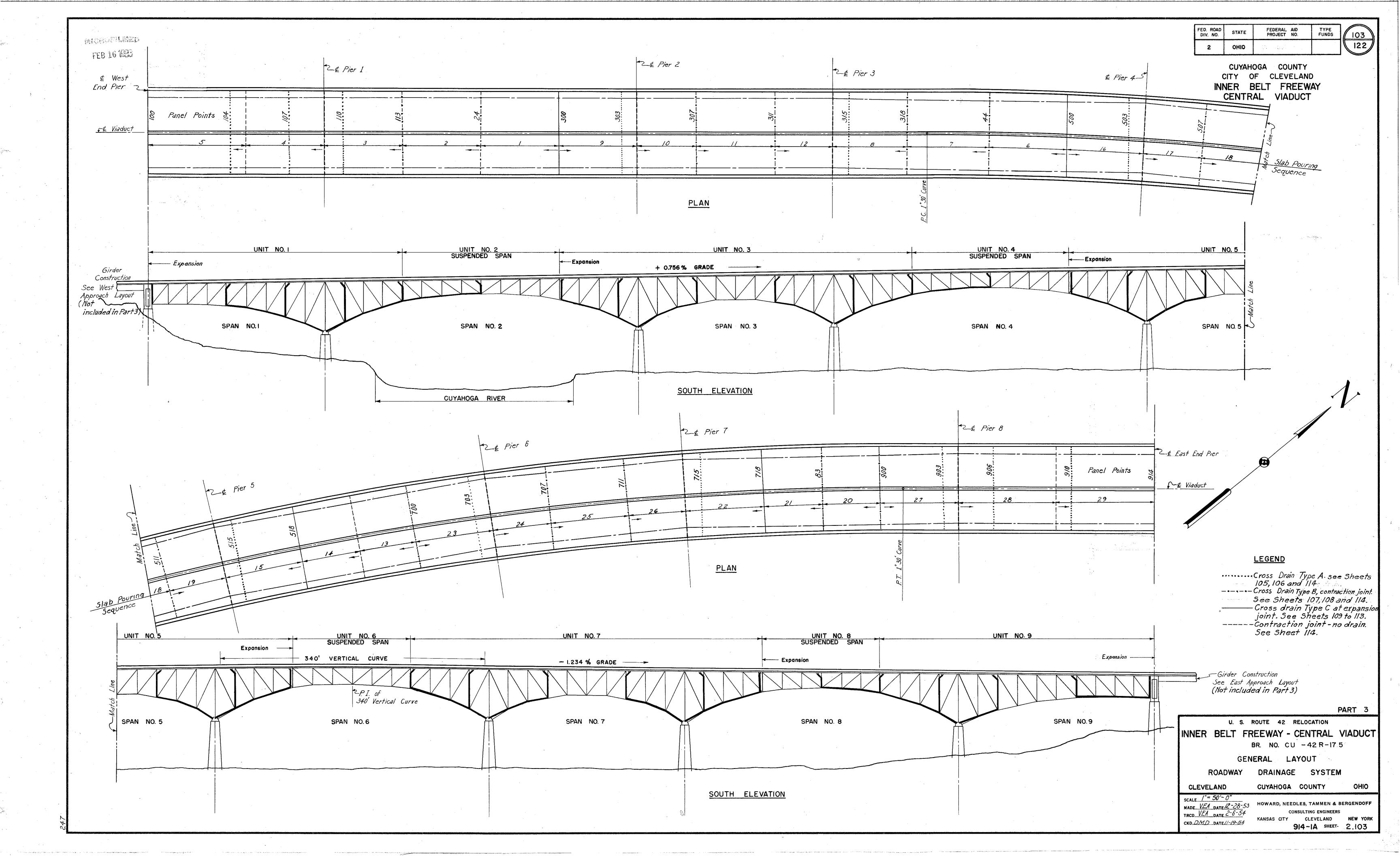


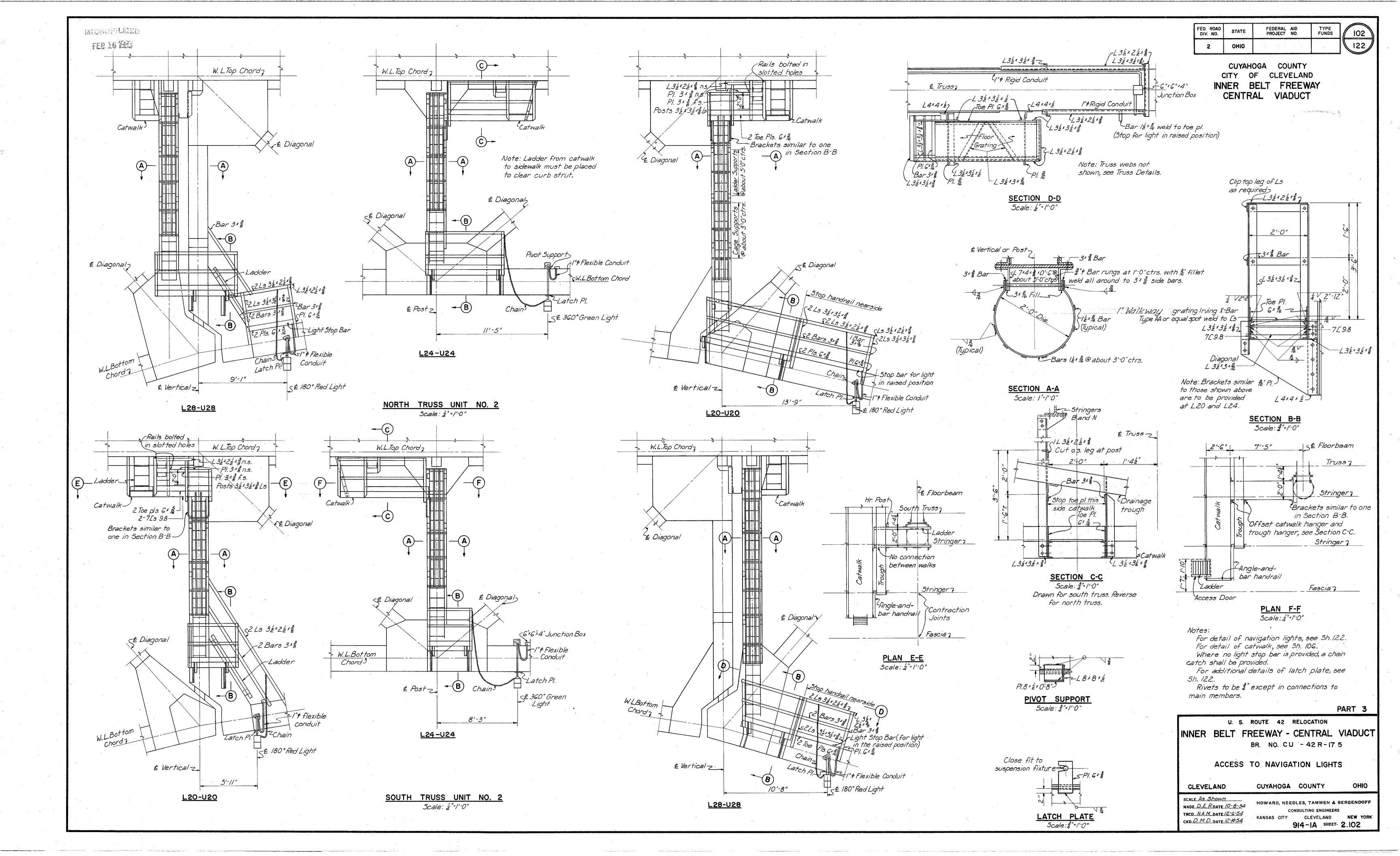


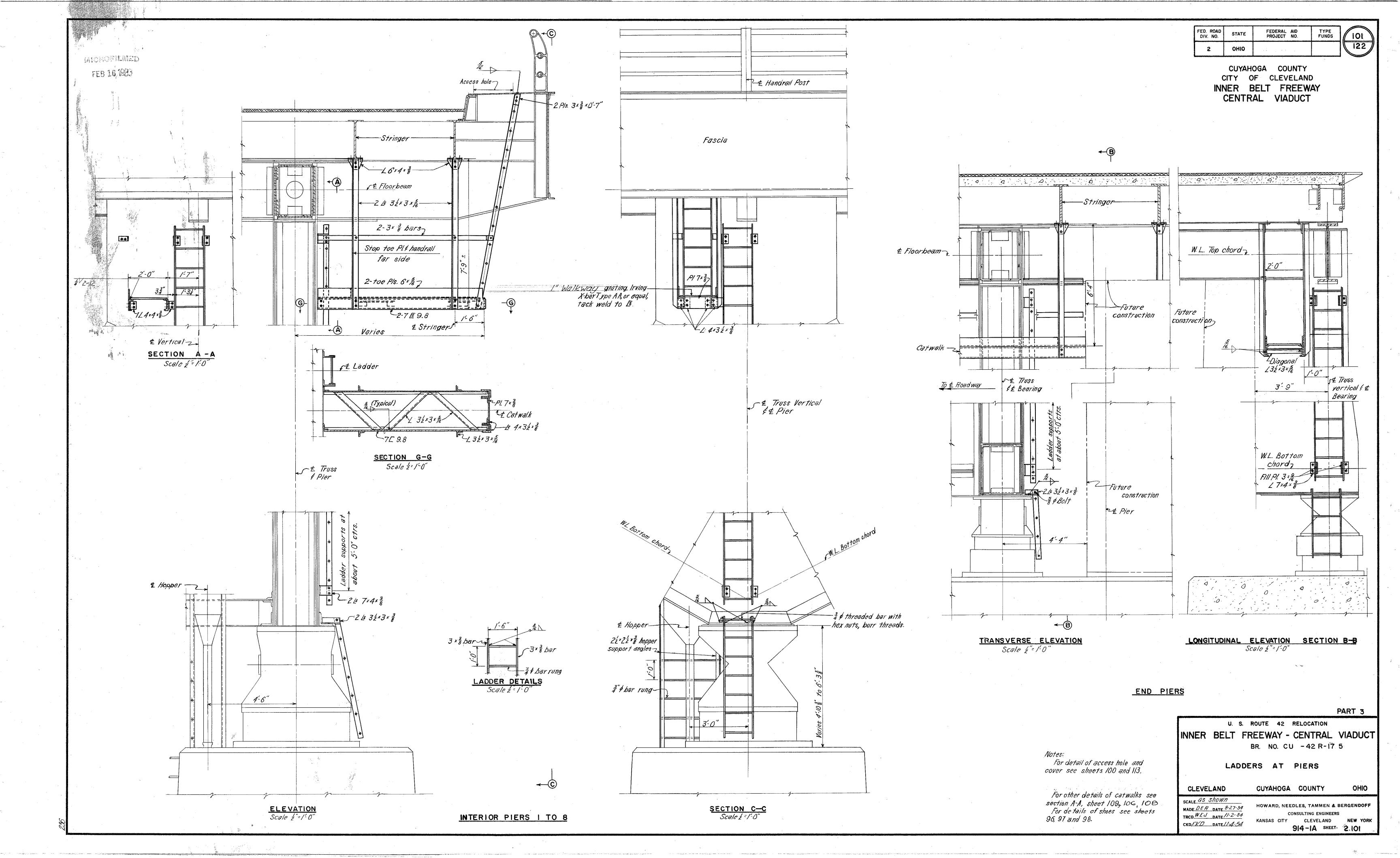


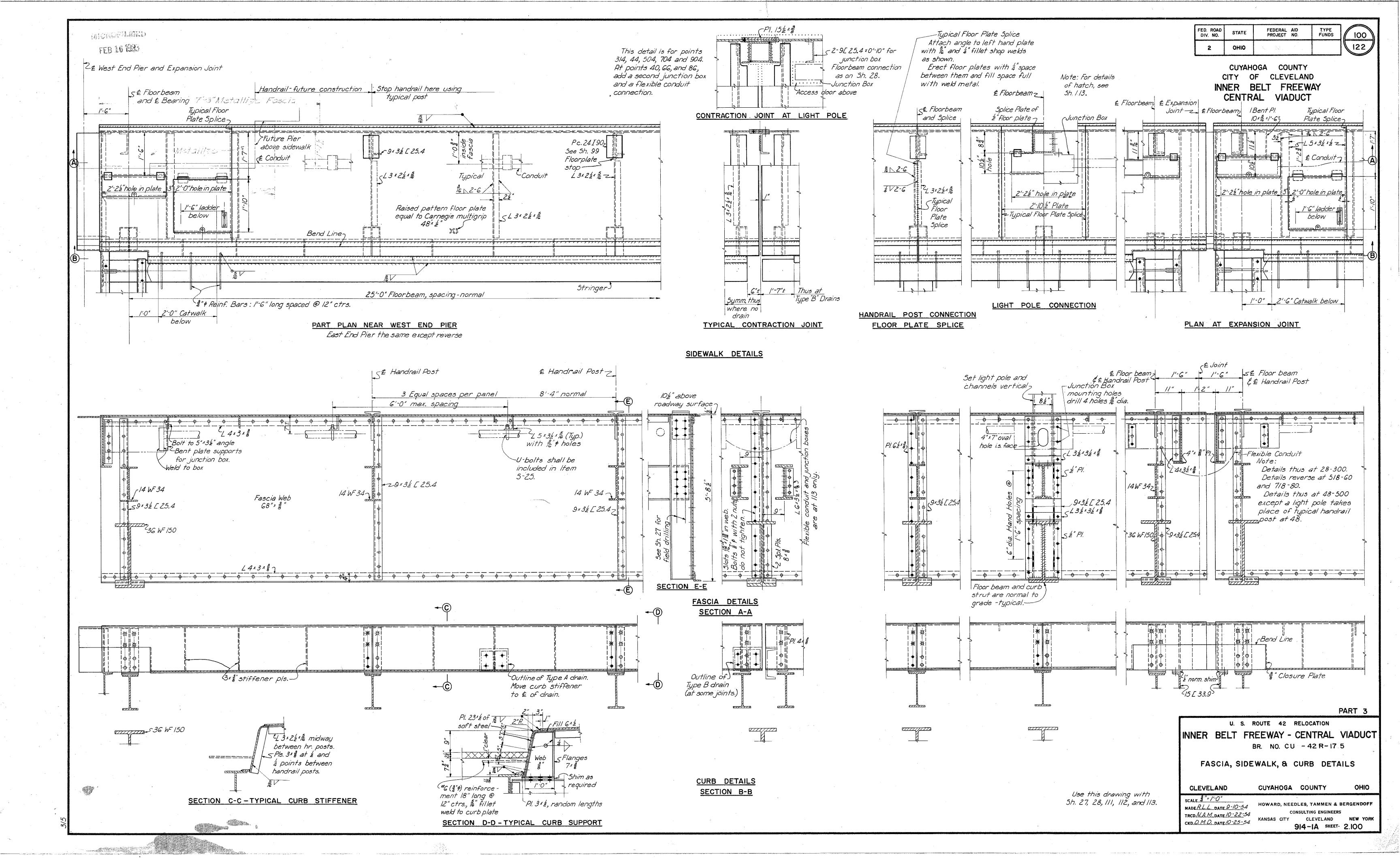


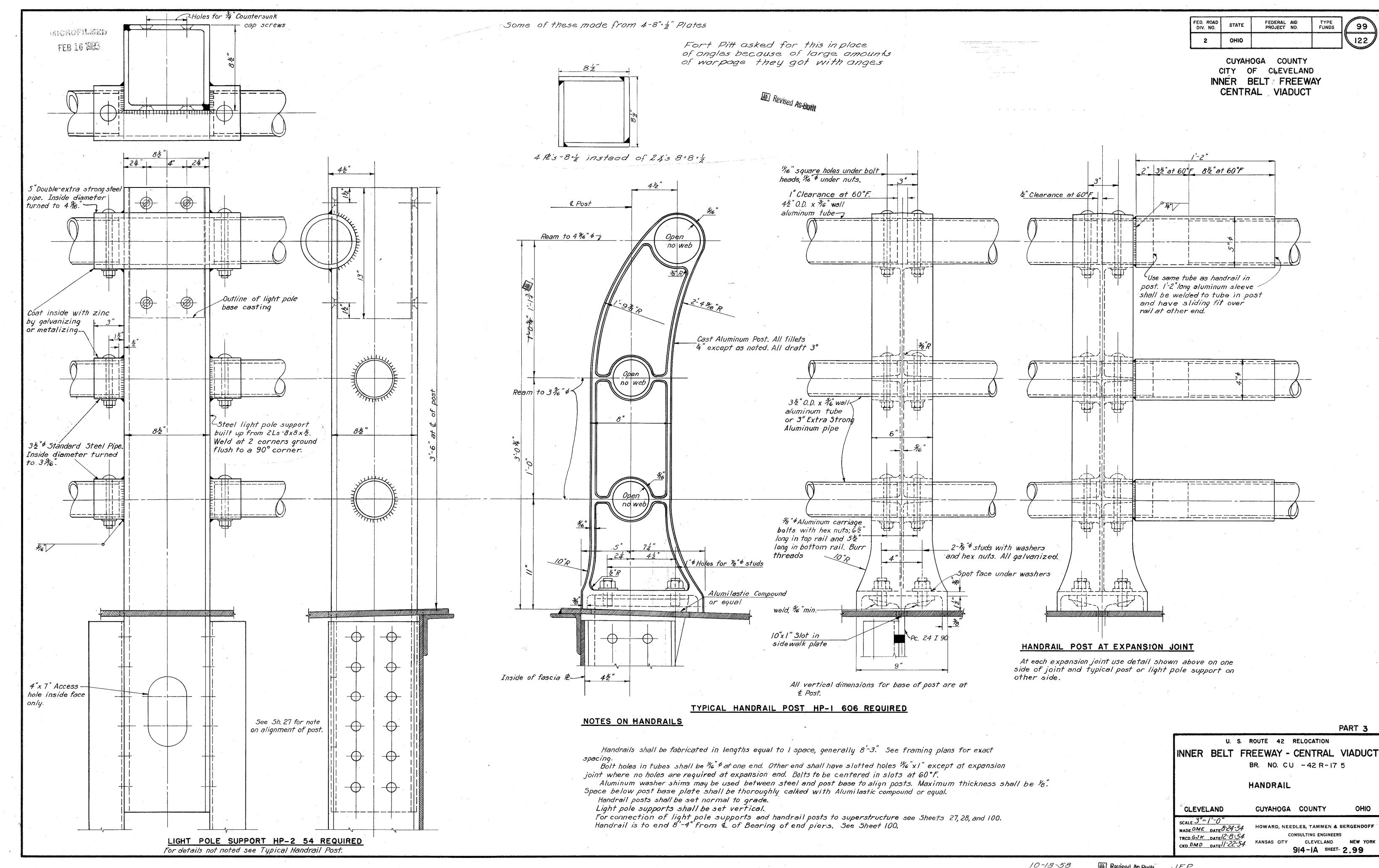


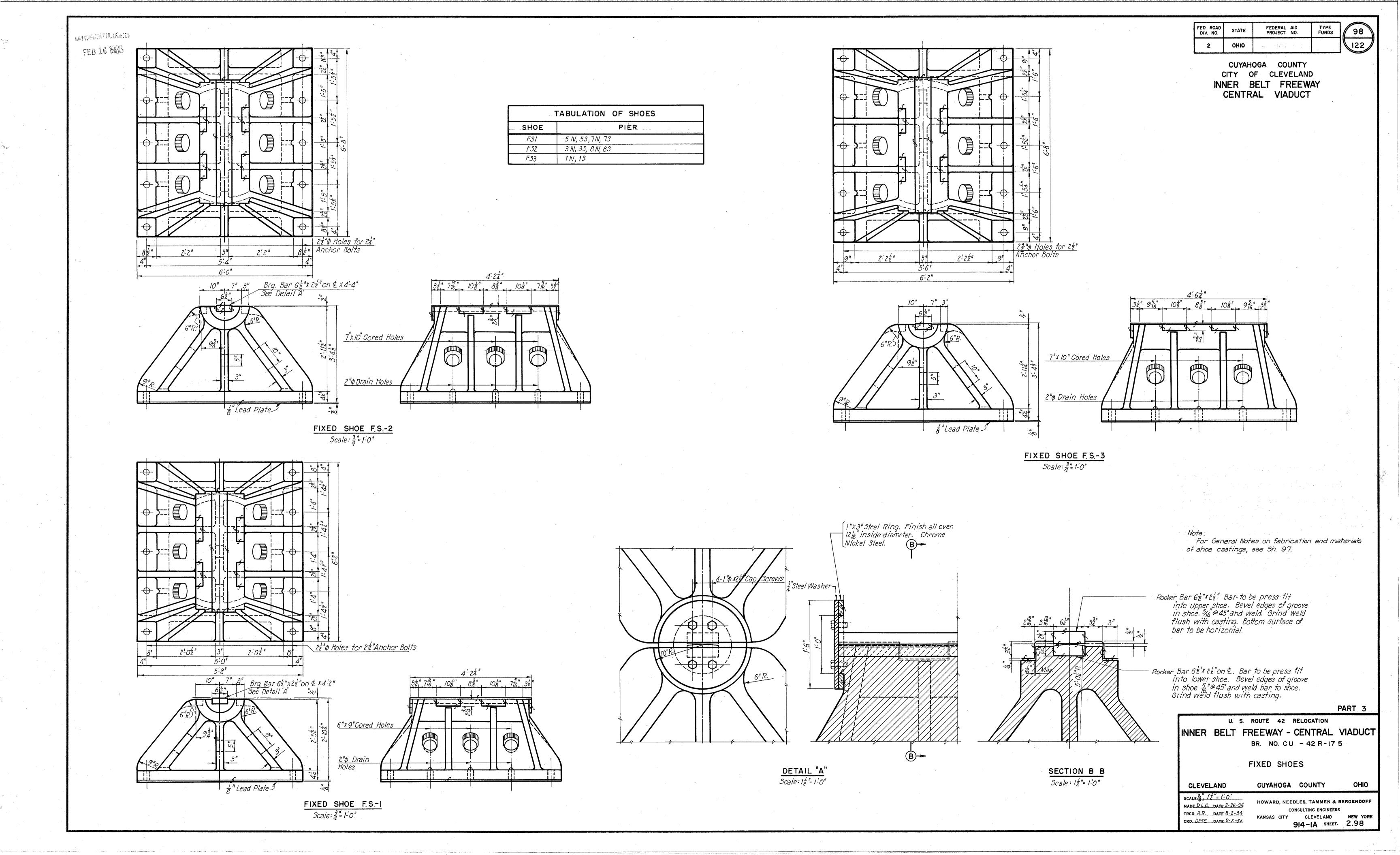


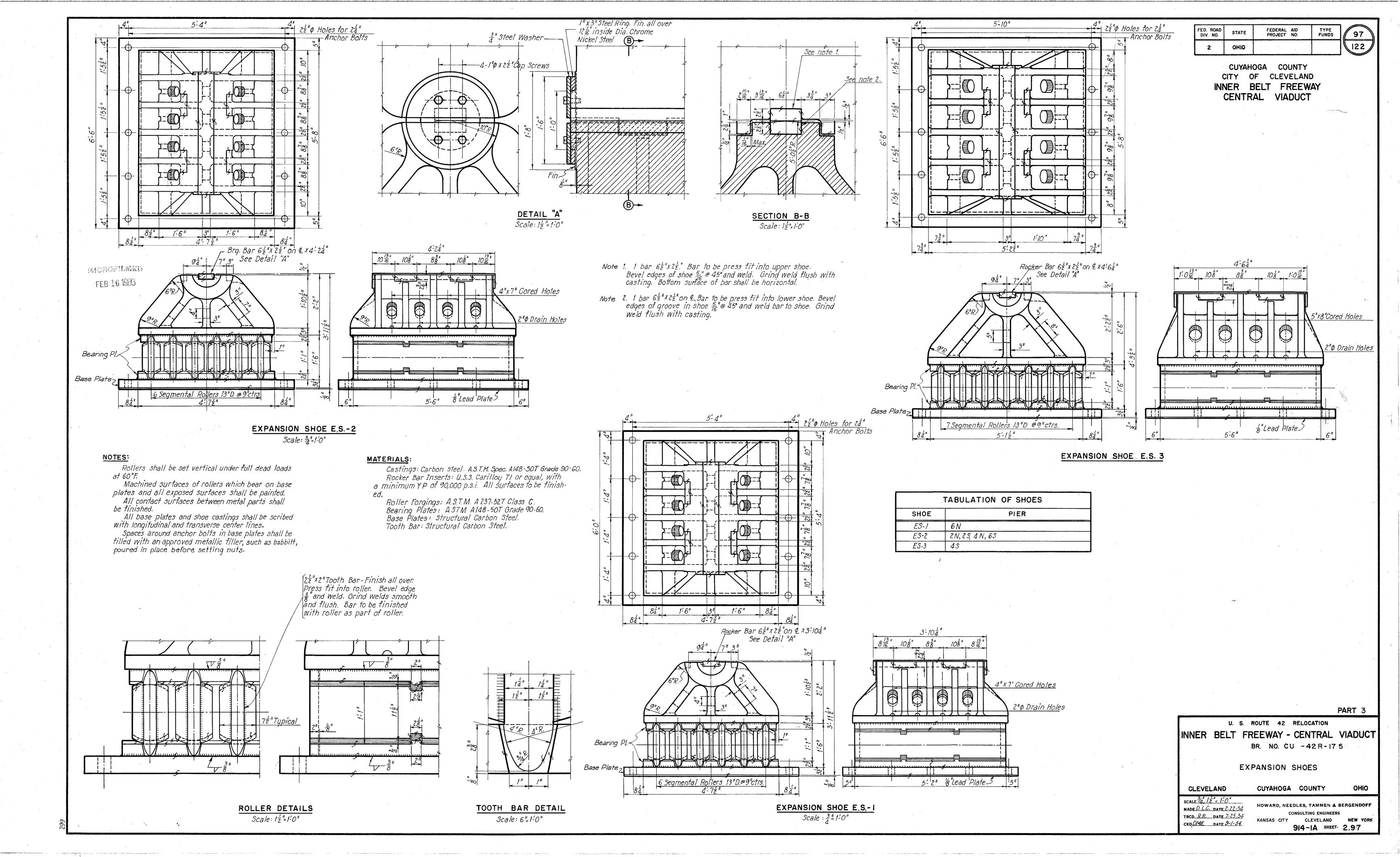


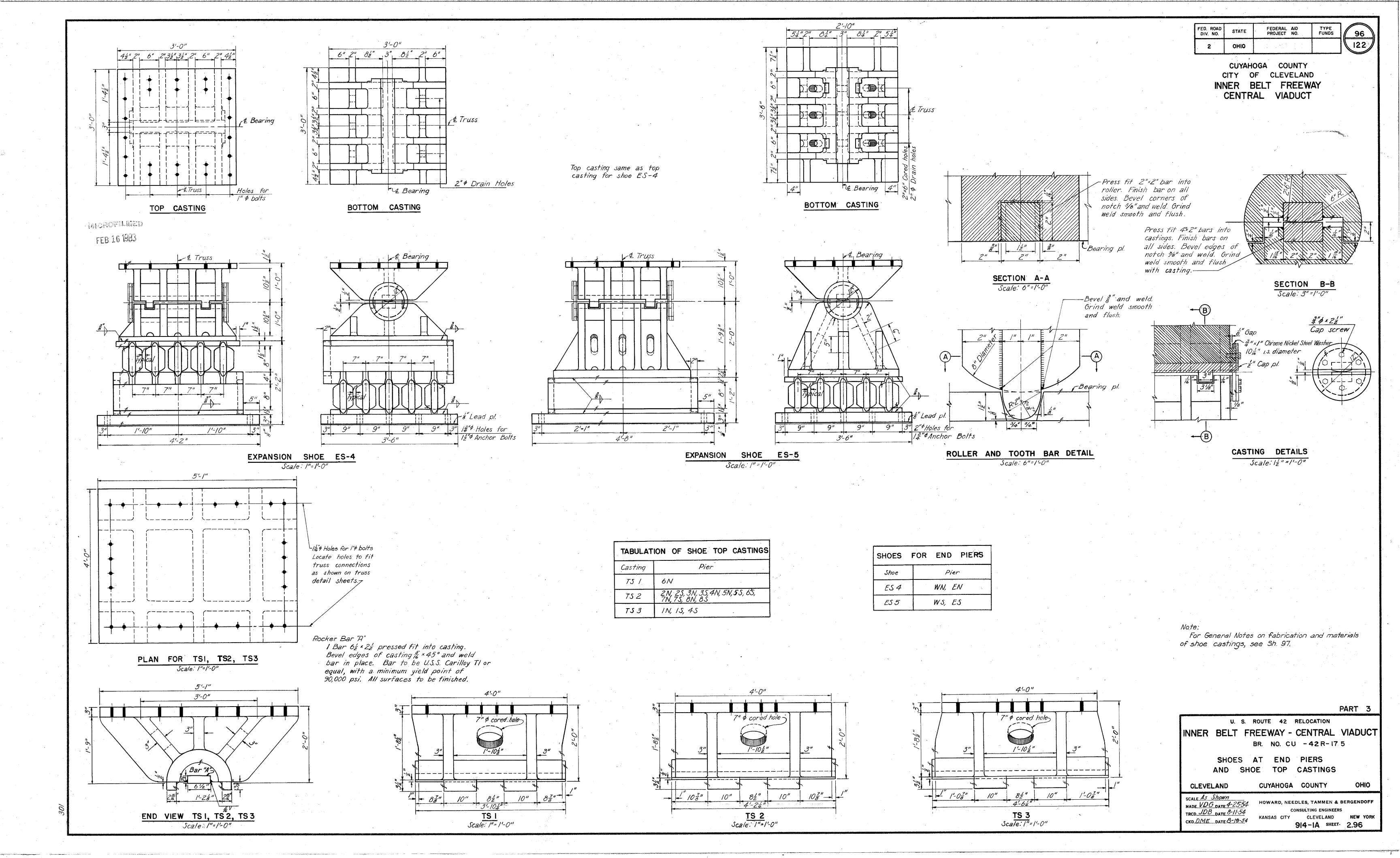


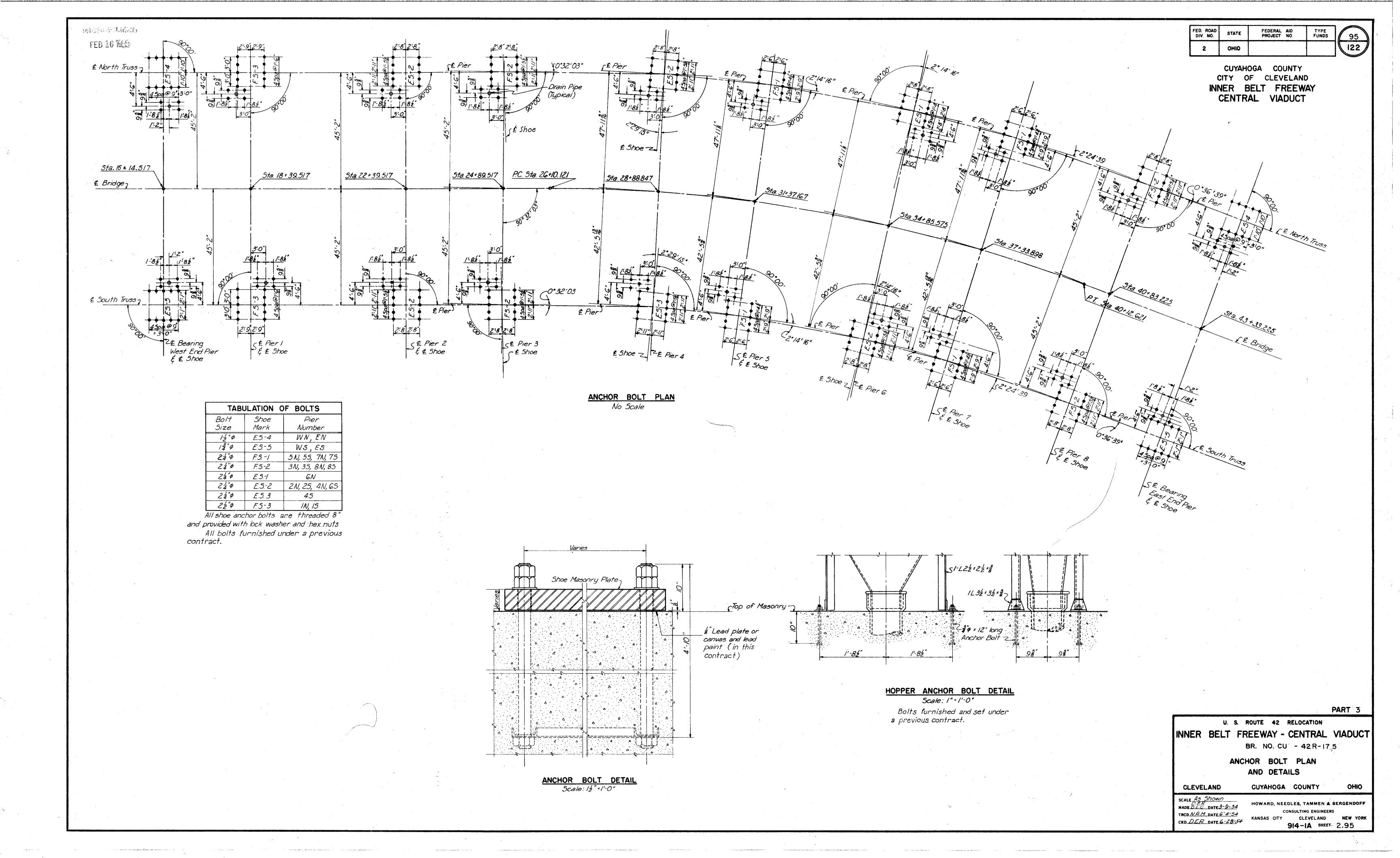


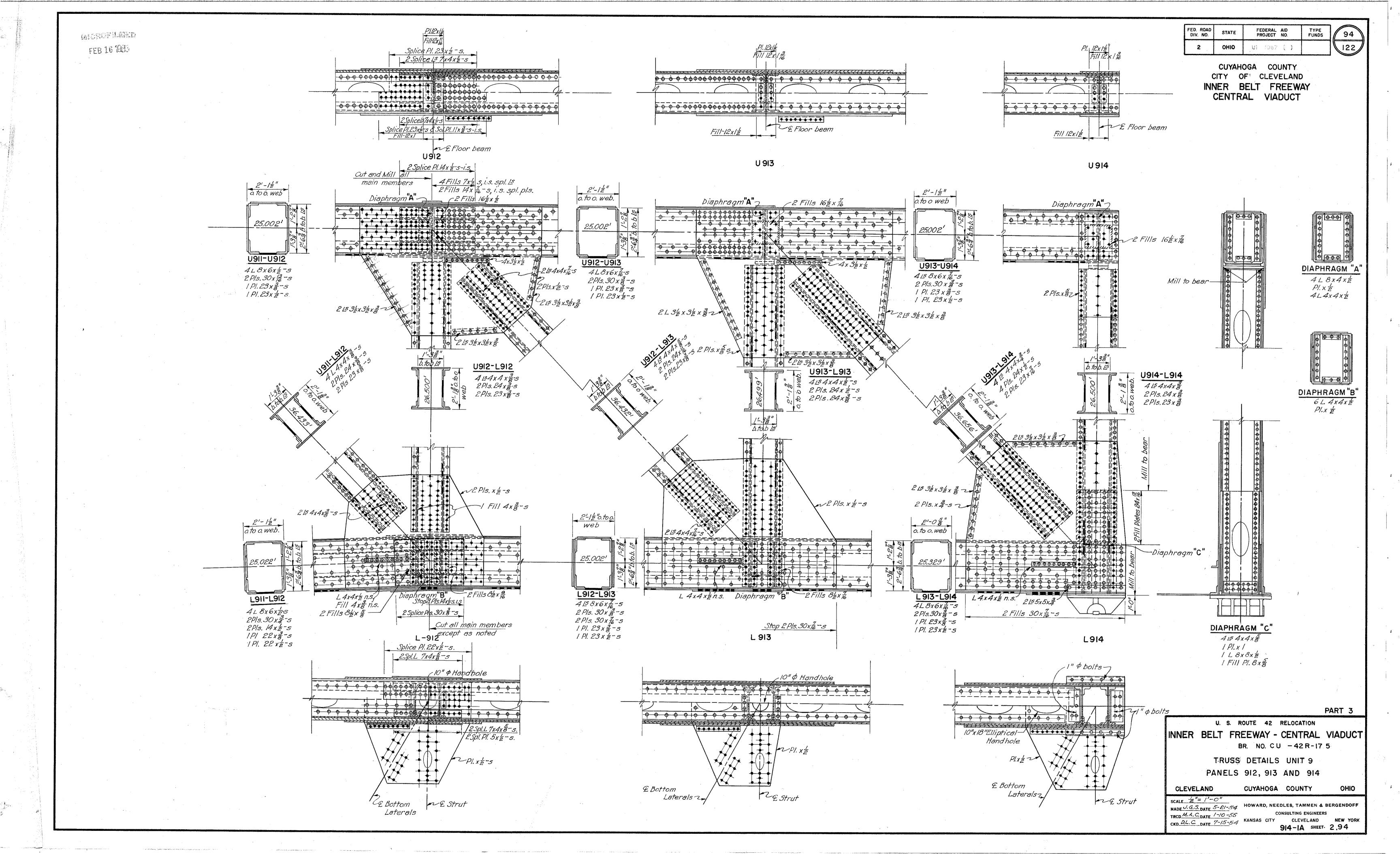


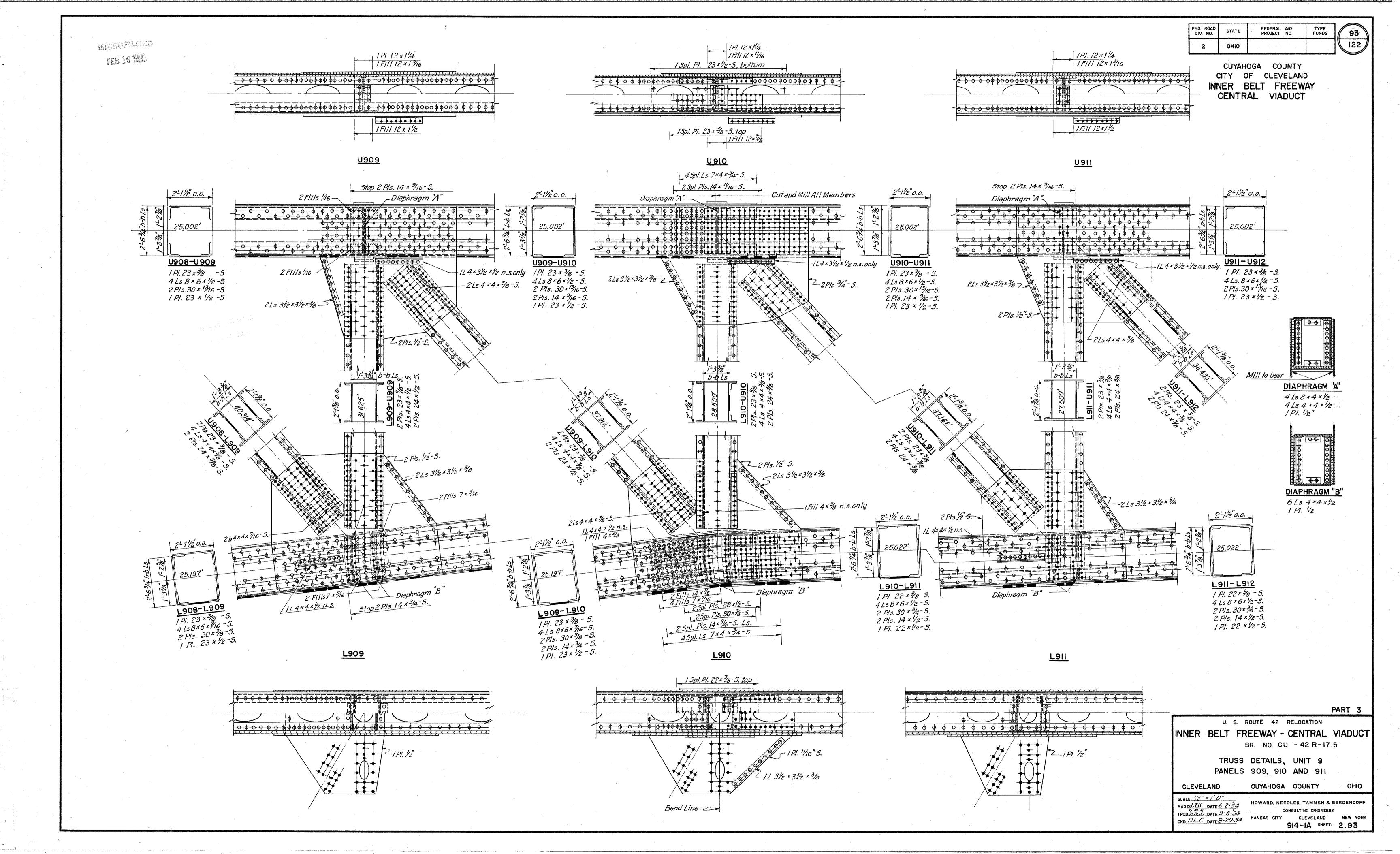


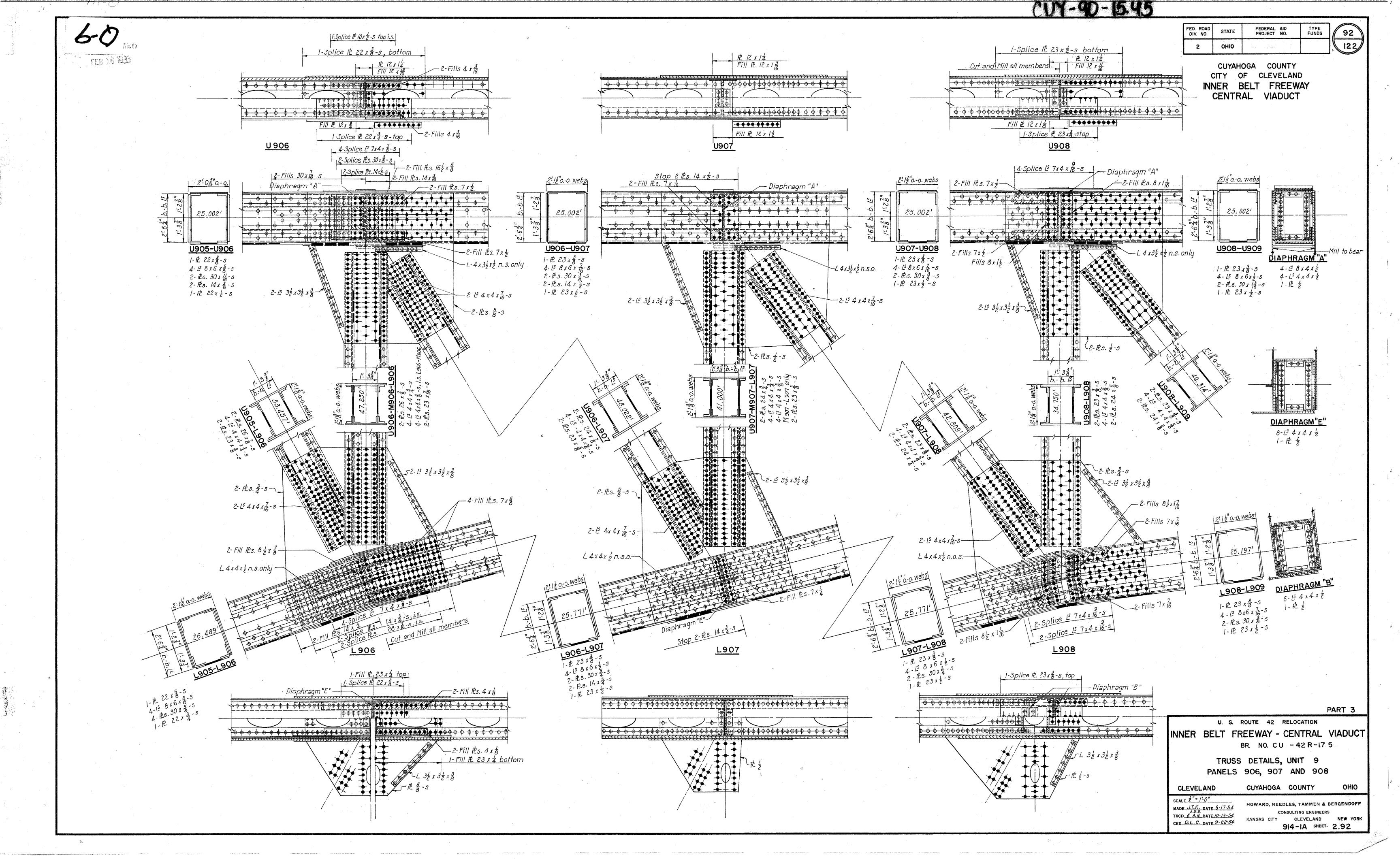


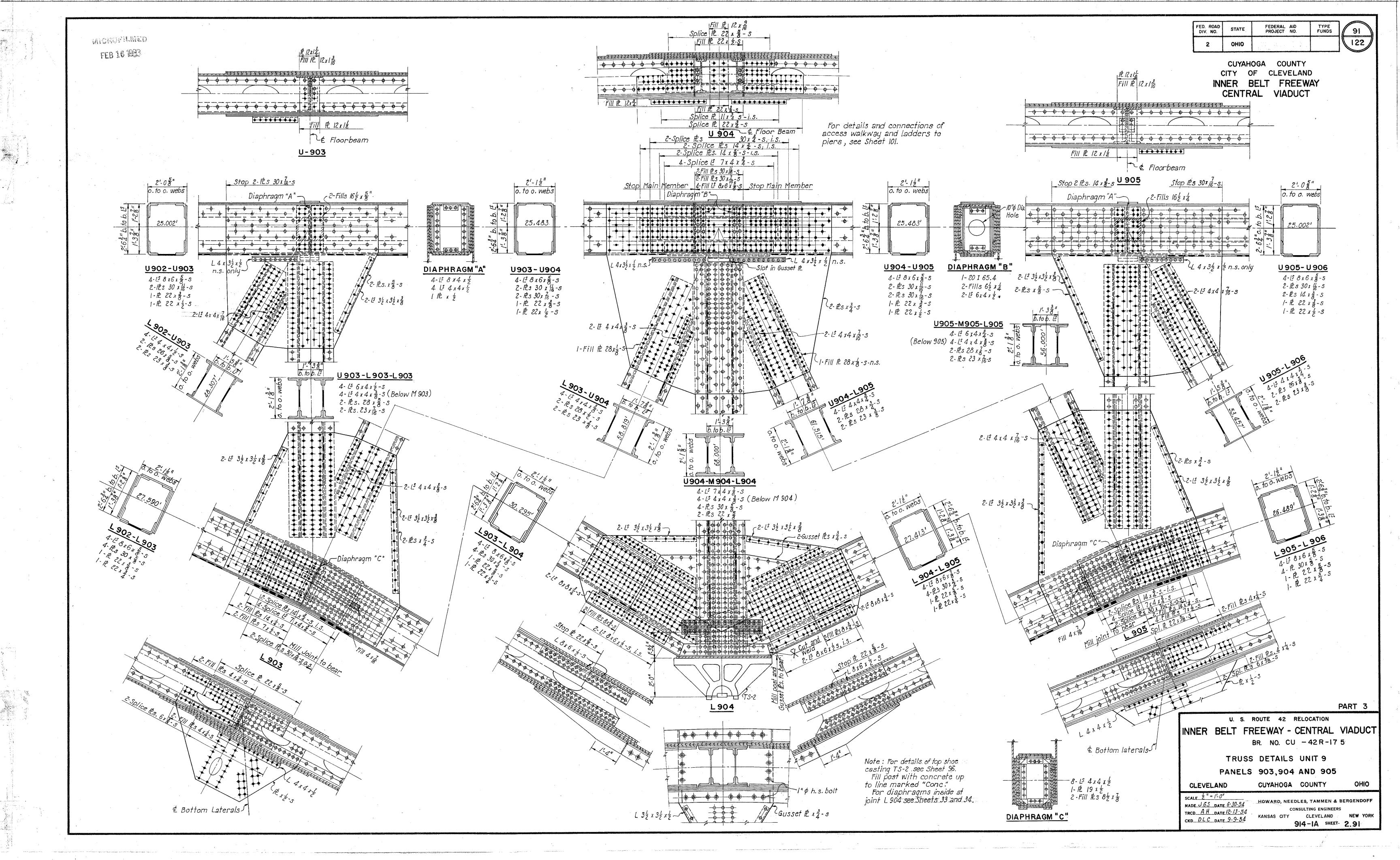












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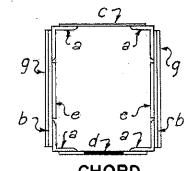
FEDERAL AID PROJECT NO. 122

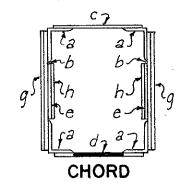
CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT

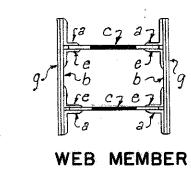
						·····	<u></u>						н .						<u> </u>									
					٦	<b>TENSION</b>	CHORE	)		-									COM	PRESSI	ON CHO	ORD			4			
MEMBER	U 900 U901	U901 U 902	Ü 902 1 1903	U 903	U904 11905	U 905 U 906	<i>и 906</i> И 907	L909 L910	L 910	L911	L912, 913	L 913 L 914	L 900 L <b>9</b> 01	L 901 L 902	L 902 L 9 <b>03</b>	L 903 L 904	L 904 L 905	L 905 L 906	L 906 L 907	L 907 L 908	L 908 L 909	U 907 U 908	U 908 И 909	U 909 U 910	U 910 U 911	U911 11912	U912 11913	U 913 U 914
Dead Load	9.00	+ 724	+ 1,360	+ 1,800	+:1,676	+ 1,129	+ 511	+ 673	+1,101	+ 1,243	+ 1,126	+ 697	754	- 1418	- 1988	-2445		-1775	- 1162	- 526	+ 108	- 107	- 66 <b>8</b>	- 1.100	-1242	-1126	- 697	
0.8 Dead Load	,	+ 579	+ 1,088	+1,440	+1341	+ 903	+ 409	+ 538	+ 881	+ 994	+ 901	+558	- 603	- 1134	-1590			- 1420	- 930	- 421	+ 86	- 86	- 534	- 880	- 994	- 901	- 558	
Live Load + Imp Tension			<del>, , , ,</del>	1								, , , , , , , , , , , , , , , , , , , ,																
Reduced L.L + Imp Tension	,	+ 195	+ : 343	+ 426	+ 5/3	+ 541	+ 545	+ 649	+ 697	+ 639	+ 509	+ 288						+ 147	+ 296	+ 443	+ 577	+ 551	+ 505	- 448	+ 348	+ 241	+ 120	
Live Load + Imp Comp.																	·											
Reduced LL + Imp Comp.	-				- /39	- 287	- 429	- 509	- 448	- 348	- 241	- 120	- 203	- 358	- 470	- 545	- 521	- 544	- 557	- 562	<i>- 556</i>	- 572	- 643		- 6 <i>38</i>	- 509	- 288	
Reduced LL+ImpTen.xD(CF)e		+ 323	+ 568	+ 706	+ 850	+ 897	+ 903	+1,076	+1,155	+ 1,059	+ 844	+ 477						+ 244	+ 491	+ 734	+ 956	+ 913	+ 837	+ 742	+ 577	+ 399	+ 199	
Reduced LL + ImpComp. x D(CF)					- 230	- 476	- 711	- 844	- 742	- 577	- 399	- 199	- 336	- 593	- 779	- 903	- 863	- 902	- 923	- 931	- 921	~ 948	-1066	- 1153	-1057	- 844	- 477	
Ratio = Line 4 or Line 6 Line 1 (Ten.)					- 0.08	- 0,25	-0.84	- 0.74	-0.41	- 0.28	-0.21	-0.17	·					- 0.08	- 0.25	-0.84	- 5. <i>15</i>	-5.15	- 0. 74	-0.41	-0.28	-0.21	- 0.17	,,
LL Sidewalk - Tension		+ 9	+ 16	+ 21	+ 27	+ 29	+ 29	+ 34	+ 35	+ 32	+ 25	+ 14						+ 7	+ 15	+ 22	+ 29	+ 29	+ 27	+ 24	+ 18	+ 13	+ 6	
LL Sidewalk - Comp.					- 7	- 14	- 22	- 27	- 24	- /8	- 13	- 6	- 9	- 17	- 24	- 29	-27	- 29	- 29	- 30	- 29	- 29	- 33	- 35	- 32	- 25	- 14	an same of the control of
Direct Design Stress		+ 911	+1,672	+2167	+ 2218	+1829	+ 1,341	+ 4648	+2,071	+ 2,085	+1,770	+1,049	-948	-1744	-2393	+2888	-2748	-2351	-1882	-1382	+ 1071	-/063	- 1633	- 2068	- 2083	-1700	-1049	
Direct Design Stress Reverse Design Stress										•											- 864	+ 856						
			40.000							•																		
Holes out									·																			
for Tension	~ · · · · · · · · · · · · · · · · · · ·	ļ					74								ļ	<u></u>						<u> </u>	•			<del> </del>		2 2 7/
a Angles 2	4x4x/2	4 x 4 x /2		8 x 6 x <sup>5</sup> /8			8x6 x 1/16		8 x 6 x /2		8 x 6 x 7/16						8x6x7/8			***************************************	8 x 6 x 7/16	<del></del>			8 x 6 x /2		8 x 6 x 7/16	
b 1. Web Plate 4	30 x 3/8	30 x <sup>3</sup> /8	30 x 1/16	-	30 x 1/16		30 x 3/8	30 x 3	30 x <sup>3</sup> /4	30 x <sup>3</sup> /4	30 x 3/8	30 x 3/8	30 x 3/8	30 x 3/8	30 x 5/8	30 x 3/4	30 x 3/4	30 x 5/8	30 x <sup>3</sup> /4	30 x <sup>3</sup> /4	30 x 3/8	30 x 3/8	30 x 13/16		30 x 13/16	30 x 13/16	30 x 3/8	
c Top Plate 3	23 x 5/16	23 x 5/16			22 x 3/8	22 x 3/8	23 x 3/8	23 x 3/8	22 x 3/8	22 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	23 x 3/8	23 x <sup>3</sup> /8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 2 3/8	23 x 3/8	23 x 3/8
d Bottom Plate 2	23 x 3/8*	23x3/8*)	22 x 1/2*	22x2*	22x1/2*)	<del></del>	23×/2*)	23 x ½ *)			23 x 1/2 *)	23x1/2*)	23x1/2*)		22 x 3/4 **)	) 22 × 3/4**)	22×3/1**)	22 x 3/4 * * )		23 x 1/2*)	23 x /2 *)	23 x /2 * )	23×2×1		23x1/2*)	23×12*)	23 x 1/2*)	23 x /2*)
e 1. Inside Web Plate 2						14 x 3/8	14 x 1/2	14 x 1/4	14 x /2	14 x 1/2				14 x 7/16					14 x 3/4					14 × <sup>9</sup> /16	14 x 3/16	<u> </u>		
g 2.0utside Web Plate 4				30 x 7/16	30 x 7/16						30 x 3/16			30 x 3/8	<i>30 x 5</i> ⁄8	30 x <sup>3</sup> /4	30 x <sup>3</sup> /4	30 x 5/8										
h 2. Inside Web Plate 2																<u> </u>												
Length In				<u> </u>								l	308.9"	312.7"	331.1"	353.6"	318.6	317.9"	309.3"	309.3"		300"	300"	300"	300"	300"	300"	300"
Length In Minimum Radius of Gyration In													- <del>  </del>				10,80	10.90	10.53	11.20	1 8 2 1 1 2	10.95	311.18	10.68	10.68	11.18	10.95	10.95
Allowable Stress Lbs/Sq.ln	21 000	21 000	21 000	21 000	24,000	24,000	21 000	24,000	21 000	24 000	21.000	21 000	10.63	10.84	10.90	10,80	19,600	19,610		19,650	24,000 t			19,640	19,640	19,670	19,650	19,650
Allowable Stress Lbs/Sq.ln Actual Gross Area Sq.ln	4.9.19	24,000 49.19	88.44	114.69	114.69	98,94	24,000 74.85	81,85	24,000 99.75	24,000 99.75	24, 000 87.10	24,000 60.85	19,610 60.85	19,620	19,570	158.67		131.19	107.63	86.63	60.85	60,85	90.38		106.13	90.38	60.85	60.85
Allowable Stress Lbs/Sq.ln Actual Gross Area Sq.ln Net Area Sq.ln	40.50	40.50	75 82	08 57	98.57	84.82	64.22	70.22	85.63	85.63	74.98	52 22	54.28	95,22	131.19	158.67		131.19	107.25	86.25	52.22	54.01	90.05		105.80	90.05	54.01	54.01
Actual Unit Stress Lbs./\$q.lr.		22,500	22 050	21,980	22,500	21,560	20,880	23 470	24/90 0.8%	24 350 1.5 %	23,610	20,090	17,470	18,320	131.19		17, 330	17,920		16,020	20,500 t	19,680	18,140		19,690	19,660	19,420	07.01
	5	3	C 2, 000	1 2, 500	5	5.,500	5	5,7,0	24,190 0.8%	S S	5,0,0	3	11,410	5	5	3	31,000	5	5	30,000	5	75,000	70,740	10,000	13,030	12,000	12,420	3
l Material		, ,	(4)	1 (v)	1 J	1 0	<del></del>	<u> </u>	I ,	J	L 3	1 0		(4)	(4)	1 /v1	(41)	(*)	[. J	<u> </u>				1 0		1 0	<u> </u>	
			(x)	(x)	(x)	(x)	(x)							(x)	(x)	(x)	(x)	(x)	(x)									•

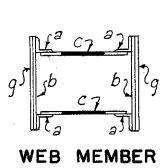
		-					<b>TENSION</b>	WEB	MEMBER	RS			-				÷						CON	PRESSIC	N WEB	MEMB	ERS								
M	EMBER L	L 900 U 901	L 901 U 902	L 902 U 903	L903 U904	U 904 L 903	U 905	U 906	U907	U 908	U909 L910	U910 L911	U 912 L 912	U 913 L 913	U 901 L 9 <b>0</b> 1	U 902 M 902	M 902 L <b>9</b> 02	U 903 M 903	M 903 L 903	U 904 M 904	M 904 L 904	U 905 M <b>9</b> 05	M 905 L 905	U 906 M <b>90</b> 6	M 906 L 906	U 907 M 907	M 907 L 907	U 908 L 908	1	U910: L910		U 911 L 912	U912 L913	U913 L914	U 914 L
ead Load		+ 1063	+1072	+ 850	+ 680		+ //69	+1188	+ 1058	+ 906	+ 655.	+ 2.11	+ 334	+ 609	- 898	- 9.91	- 1134	- 872	- /0/5	-1709	-1927	- 1178	-1321	-1162	-/305	- 993	- 1136	- 836	- 616 - 493	- 289	+ 2	- 170	- 625	- 1010	- 98
0.8 Dead Load		+ 850	+ 858	+ 680	+ 544	+ 840	+ 935			+ 725	+ 524		+ 26.7	+ 487		-793	- 907	- 872 - 698	- 8/2	- /367	- 1543	- 942	-1321 -10.57	- 930	-1044	- 794	- 909	-669	- 493	-231	+ 2	- 136	- 500	- 808	- 78
Live Load + ImpTens	sion										* -17													-											
Reduced LL + ImpTen	sion	+ 282	+ 279	+ 215	+178	+ 334	+ 336	+ 3/0	+ 297	+228	+ 200	+ 190	+ 223	- 274	1 SH			a .	V 1	+ 54	+ 45	+ 52	+ 52	+ 7	+ 7	+ 9	+ 9	+ 23	+ 42	+ ///	+ 154	+ 172	+ 176	+177	
Live Load + Imp Com	īD.																,					]	·										·		
Reduced L L + Imp C	omp.	, ,				-118	- 59	- 9	- 10	- 47	- 78	- 186	- 128	- 128	- 222	-239	- 285	-200	- 249	- 354	- 395	- 311	- 353	- 275	- 324	- 249	- 306	- 186	- /57	- 142	- 125	- 251	-349	-422	- 36
Reduced LL + ImpTer	1. x D (C F) e	+ 467	+462	+ 356	+ 295		+ 557	+ 514	+ 492	-378	+ 331	+ 315	+ 370	+ 434						+ 89	+ 76	+ 86	+ 86	+ 12	+ 12	+ 15	+ 15	+ 38	+ 70	+184	+ 255	+ 285	+ 292	+ 293	
Reduced LL + Imp Con	np. x D(CF)e			* * *		- 196	- 98	_ /5	- 17	- 78	- 129	- 308	- 212	-212	- 368	- 396	-472	- 331	-4/3	- 587	- <i>655</i>	- 5/5	- <i>58</i> 5	- 456	- 537	-413	-507	- 308	- 260	-235	- 207	- 4/6	- 578	- 699	- 60
Reduced LL+lmpCon Ratio = Line 4 Line (Comp.) or L	Line 6					- 0.11	- 0.05	- 0.008			-0.12	- 0.88	- 0.39	-0.21						- 0.03	- 0.03	- 0.04	- 0.04	- 0.00	- 0.00	-0.01	- 0.00	- 0.03	-0.05	- 0. 38	- 62.5	- 1,01	- 0.28	- 0.17	
LL Sidewalk - Tension		+ 13	+ 13	+ 10	+ 8	+ 17	+ 16	+ 14	+ 13		+ //	+ //	+ //	+ 14						+ 2	+ 2	+ 3	+ 3	0	0	0	0	+ 1	+ /	+ 5	+ 7	+ 10	+ 9	+ 9	
LL Sidewalk -Comp.					-	- 6	- 3	- 0	- 1	- 2	- 3	- 8	- 7	- 7	- 11	-12	- 14	-10	- 12	- 20	- 22	- 15	- 17	- 13	- 15	- 12	- 14	- [[	- 9	- 8	-:7.	- //	- 16	- 21	_
Direct Design Stress	•	+ 1330	+ 1333	+1046	+847	+1411	+ 1508	+ 1478	+ 1351	+1115	+866	+ 495	+ 648	+ 955	- 1097	-1201	-/393	-1039	- 1237	-1974	- 2220	-1472	~ 1659	-1399	- 1596	-1219	-/430	- 988	- 772	- 474	-264	- 563	- 1094	- 1528	- 1.3:
Reverse Design Stres													1		70 0 7	1	1	,,,,,	,,,,,,	,,,,		,,,,,		,,,,,,							-212	+ .3			<del></del>
												1															ŀ							1	
																							;			* .							1		
Section	Holes out for Tension																							,											
Outer Angles	2 4	4 x 4 x 3/8	$4 \times 4 \times \frac{3}{4}$	4×4×1/2	4 x 4 x 3/8	4 x 4 x 3/4	4 4 x 4 x 3/4	4 4 x 4 x 3/4	$4 4 \times 4 \times \frac{3}{4}$	1 4 x 4 x 5/8	4 x 4 x 3/8	4 x 4 x 3/8	4 x 4 x <sup>3</sup> /8 24 x <sup>3</sup> /8 ) 23 x <sup>3</sup> /8 * *)	4x4x1/2	4 x 4 x 5/8	4 x 4 x 3/4	4 x 4 x 3/4	6 x 4 x 1/2	6x4x1/2	7x4x7/8	7 x 4 x 1/8	6 x 4 x <sup>3</sup> / <sub>4</sub>	6x4x3/4	4 x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 5/8	4x4x1/2	4 x 4 x 3/8	4 x 4 x 3/8	4x4x3/8	4x4x5/8	4 x 4 x 3/4	4 x 4
I. Web Plates	3	24 x 13/16	24 x 13/16	26 x 5/8	28 x 1/2	28 x <sup>3</sup> /4	26 x 3/8	24 × 1/8	24 x 3/4	24 x 5/8	24 1/2	24 x 3/8	24 x 3/8	24 x 1/2	24 × 3/4	26 x 3/4	26 x 3/4	28 x 5/8	28 x 5/8	30 x 5/8	30 x 5/8	28 x 7/8	28 x 7/8	26 x 7/8	26 x 7/8	24 x 3/4	24 x 3/4	24 x 3/8	24 x /2	24 x 3/8	24 x 3/8	24 x 3/8	24 x 1/16	24 x 1/2	24 x
Cover Plates	2 2	23 x 7/16**)	23 × 7/6**)	23 x 3/8 **.	23 x 3/8 * *.	) 23 x 3/8 * *	1)23 x 3/8 * *	) 23,3/8 **	) 23 x 3/4 **	) 23 x 3/8 * *	23 x 3/8 * * >	23 x 3/8 * *	) 23 x 3/4 * *)	24 x 3/8 * *)	73 x 3/4 * *	23 × 1/6 * *)	23 x 7/6 * *)	23 x 7/6**)	23 x 7/16**)	22 x 3/4 * )	22 x 5/8 * * )	23 x 7/6**)	23 ×7/6**)	23 x 7/16 **)	23x1/6**)	23 x 3/8 * * )	) 23 x 3/8 * * )	24 x <sup>3</sup> /8 23 x <sup>3</sup> /8 **)	23×3/8**)	23x38**)	23 x 3/8 * *.	23 x 3/8**)	23 x 3/8**)	23 x 7/6**)	23 x
Inner Angles	2			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				1		-						4×4×3/8		4 x 4 x 3/8		4 x 4 x 3/8		4 x 4 x 3/8		4 x 4 x 3/8		4 x 4 x 3/8								
2. Web Plates	3		····		<del> </del>			·····								<del> </del>				30 x 5/8	30 x 5/8													24 x 1/2	
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							·								<u> </u>		<del></del>																
			· · · · · · · · · · · · · · · · · · ·																																
							1						<u>-                                    </u>					P-1							<u> </u>										
Length	1/2.	. 4													408"	4.96"	496"	636"	636"	816"	816	672"	672"	567"	567"	4.92"	492"	417"	379.5"	342"	330"	437.2	437.2	439.87"	3
Tinimum Radius of Gui	ration In.								<del> </del>					· · · · · · · · · · · · · · · · · · ·	7.67	<del> </del>	777	8 54	8.25	9.08	8 92	8.58	8.28	7.96	7 75	7.75	7.55	7.74	7.71	342" 7.70	7:70	7, 70	7. 70	7.63	7
Mowable Stress /	bs./5q.ln. 5q.ln.	24,000	24 000	24 000	24 000	24 000	24 000	24 000	24 000	24 000	21 000	18,000	24 000	24 000	18,700	7.99	7.77	17 270	17 270	9.08 16,160 125.44	16 160	8.58 17,180	17 180	567" 7. 96 17, 540 78,64	17.540	18 050	18 050	18,670	18 890	19 090	14 540	18 520	7.70 18,520 61.19 59.64	18.470	14.
Allowable Stress L. Actual Gross Area	Sa. In.	72.14	72.14	57. 25	4.9.19	73.51	77.01	73.51	24,000 67.51	58.19	45.19	39.19	39.19	49.50	6/1/9	18,120 72.14	18,120 83.58	65.38	76.82	125 11	136.88	88.14	99.58	78 64	90.08	67.51	78.95	58.19	48.75	39 /9	39.19	39 /9	61.19	81.14	39
let Area	Sa Inl	59.52	59.52	46.75	40.69	60.01	62.51	60.76	55.51	1701	37.60	32.44	32.44	40.00	6/1 10	72 11	83.58	61.78	76.82	125.44	136.88	88.14	99 58	78.64	90.08	67.51	78.95	54.50	42.09	3/.33	31,33	31,33	59.64	81.14	3
Actual Unit Stress /	hs/S0 /n		22,340	22,370	20,810	23, 510	24,120 0.5	% 24 370 1.2%	· 24,340 1.4.9	6 23,260	22,980	15,250	19,980	23,880	17 100	16,650	16,680	16,810	16,100	15 710	16,200	16, 700	99.58 99.58 16,660	17,780 1.4%	17,720	18,060	18,110	18,130	18,130	15 130	6,650	17,960	18,340	18,830 1.9.%	4,
Actual Unit Stress L Material		5	5	5	1 .5	5	.5	.5	S S	.5	5	10,230	5	5	5	3	5	.5	3	5,5,40	S	3	.5,500	S	3	1 3	1 8	1 5	.5,.55	5	C C	5	5	5	1 (
		(x)	(X)		( X )			<u> </u>					<del></del>	<u> </u>	(×)	(x)	(x)			<u> </u>		1		<u> </u>	<u> </u>				<u> </u>	1 -	<u> </u>	<u> </u>			4

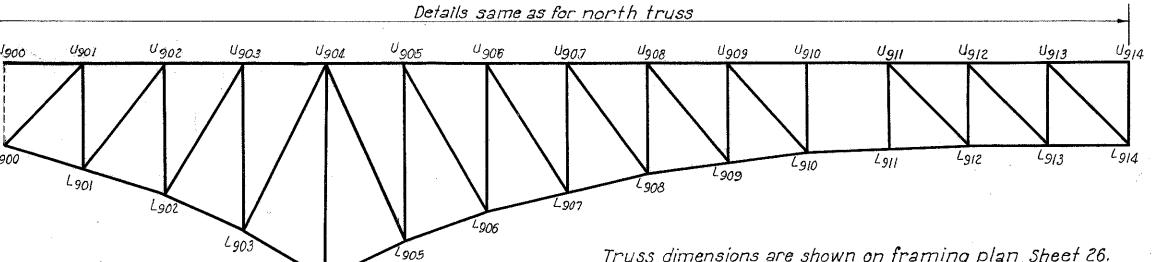
(x) Heavier Section = same
as in Unit 9 North
x) Handhole II" wide
x x) Handhole IO" wide
S = Special Steel
C = Carbon Steel











CLEVELAND Truss dimensions are shown on framing plan, Sheet 26, Trusses of north and south trusses are similar except as affected by horizontal bend at panel 904. SCALE None

STRESS SHEET UNIT 9 SOUTH TRUSS

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU -42 R-17 5

CUYAHOGA COUNTY

MADE H.W.L. DATE 5-11-53
6.J.K.
TRCD ♣ A.H. DATE 9-21-54
CKD 6.H.H DATE 9-22-54

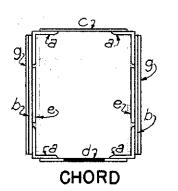
HOWARD, NEEDLES, TAMMEN & BERGENDOFF KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET 2.90

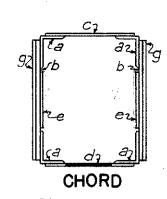
PART 3

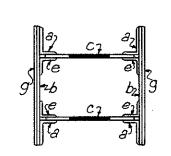
All live and dead load stresses.

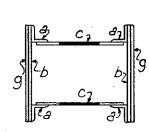
Line 29, net area for tension or effective gross area for compression.

FEB 16 Mass









WEB MEMBER

FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE Funds	89
2	оню	Hard to the second of the seco		122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

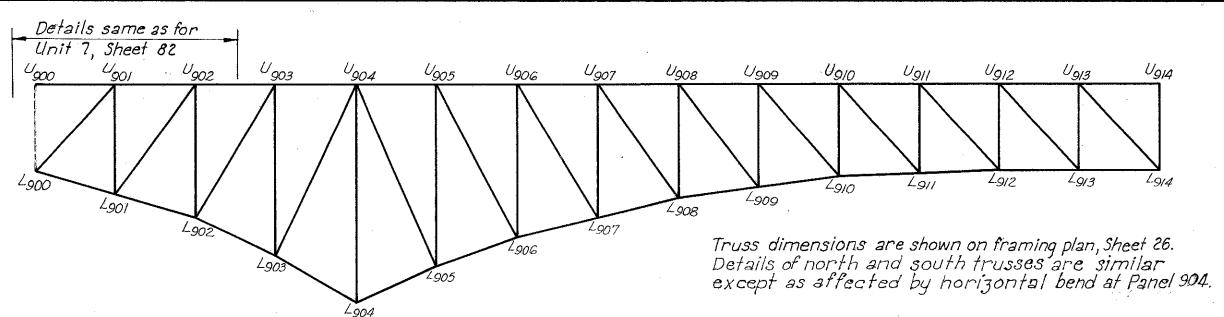
			•	•	•	TENSION	CHOR												COM	APRESSI	ON CHO	ORD						
MEMBER	U900 U90	U901 U902	U902 U903	U903 U904	U904 4 U <b>90</b> 5	U905 U906	U906 U907	L.909   910	L910 L911	L911 L912	L912 L913	L913 L914	L900 L901	L901 L902	L902 L903	1.903 1.904	L904 4 L905	L905 L906	L906 L907	L907 L908	L908 L909	U907 U908	U908 11909	U909 U910	U910 U911	U911 U912	U912 U913	U913
Dead Load	·	+ 772	+ 1450		+ 1812	+ 1269	+ 652				+ 1065	+ 669	- 805	- 1512	-2114	-2598		-1920		<del></del>	- 36	+ 36	- 536	- 983			- 669	03/
0.8 Dead Load		+ 6/8	+ //60	+ /532	+ 1450		+ 522				+ 852	+ 535	II		-1691	- 2078	<del></del>	- 1536		<u> </u>		+ 29	- 429	- 786				
Live Load + ImpTension												•			1	1 20,0	1337	7000	1070		1	, ,	753	700			000	
Reduced LL + Imp Tension		+ 210	+ 369	+ 458	+ 551	+ 581	+ 586	+ 651	+ 699	+ 641	+ 510	+ 288						+ 147	+ 297	+ 440	+578	+ 592	+ 543	+ 482	+ 374	+ 259	+ 129	
Live Load + Imp Comp.																											. ,	·
Reduced LL+ImpComp.					- 139	- 288	- 431	- 547	- 482	- 375	- 259	- 129	- 219	- 331	- 505	- 586	- 559	- 584	- 6/5	- 604	- 597	- 573	-645	-698	- 640	- 510	- 289	
Reduced LL+ Imp. Ten. × D(CF)e		+ 348	+ 612	+ 759	+ 9/3	+ 963	+ 971	+1079	+1158	+1062	- 845	+. 477		1				+ 244		4	+ 958	+ 981	+ 900	+ 799	+ 620	+ 429		
Reduced LL+ ImpComp. *D(CF)e					- 230	- 477	- 714	- 906	- 799	- 621	- 429	- 214	- 362	- 630	- 837	- 97/	- 923	- 968	- 1019	-1001	- 989	- 950	-1069	-//57	- 1061	- 845	-479	
Ratio=					- 0.08	-0.23	- 0.66	- 1.01	-0.49	-0.323	-0.243	- 0.193							-0.227	-0.65	- 16.0	-/5.9	-1.01		-0.325			
LL Sidewalk - Tension		+ 9	+ 16	15 +	+ 27	+ 29	+ 29	+ 34	+ 36	+ 32	+ 2.5	+ 14						+ 7	+ /5	+ 22	+ 29	+ 29	+ 27	+ 24	+ 18		+ 6	
LL Sidewalk - Comp.					- 7	- 14	- 22	- 27	- 24	- 18	- /3	- 6	- 9	- 17	- 24	- 29	- 28	- 29	- 30	- 30	- 29	- 29	- 33	- 36	- 32	- 25	- 14	
Direct Design Stress		+ 975	+ 1788	+ 2312	+ 23.90	+ 2007	+ 1522	+ 1546	+ /98/	+ 2016	+ 1722	+ 1026	-/015	- 1857	- 2552	-3078	<del></del>		- 2095		-1047	+ 1039	-1531	-1979	-2015	-1722		<u> </u>
Reverse Design Stress																		1			+ 958	- 950				1	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1
													···												****			
																					1							
Holes out																												
SECTION for Tension																					ļ						 	
Angles 2	4x4x/2	4x4x1/2	8x6x3/8	8 x 6 x 5/8	8x6x5/8					8x6x1/2	8x6x716						8x6x78										8 x 6 x 1/16	8 x 6 x
1. Web Plate 4	30 x 3/8				30 x 1/16		30 x <sup>3</sup> /8	30 x 3/8	1		30 x 3∕8	30 x 3/8		30 x <sup>3</sup> /8	30 x 5⁄8				30 x <sup>3</sup> /4	30 x 3/4	30 x <sup>3</sup> ∕8	30 x 3/8	30 x 13/16	30 x 13/16	30x 13/16	30 x 13/16	30 x <sup>3</sup> /8	30 x
Top Plate 3		23 x <sup>5</sup> /16		22 x 3/8	22 x <sup>3</sup> /8	22 x 3/8	23 x <sup>3</sup> /8	23 x 1/8		22 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	22 x <sup>5</sup> /8	22 x 5/8	22 x 5/8	22 x 5/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	.23 x 3/8	23 x
Bot tom Plate 2	23x38*)	23, 3/8 *	22×/2*)	22 x /2*	22 x /2*	22 x /2 * )	23x1/2*)	23 x 1/2*)	22x1/2*)	22x/2*)	23 x 1/2 *)	23x1/2*)	23 x 1/2 *)	23 x /2 * )	22x34**)	) 22x <sup>3</sup> /4 * *	) 22 x 3/4 * *)	22 x 3/4 * *	23 x 1/2 *)	23x 2*)	23 x 1/2 *)	23 x 1/2 *)	23 x 1/2 *)	23 x 1/2 *	) 23x 12*)	23x 1/2 *)	23 x 1/2 *)	23 x /2
I. Inside Web Plate 2						14 x 3/8	14 x /2	14 x 3/4	14x1/2	14 x 1/2				14 x 7/16					14 x 3/4					14 x 3/16	14 x 9/16			
2. Outside Web Plate 4				30 x 1/16	30 x 7/6						30 x 7/16			30 x 3/8	30 x 5/8	30x 3/4	30 x <sup>3</sup> /4	30 x 5/8										
								,																				
Length - In.													308.9"	312.7"	331.1"	363.5"	329.0"	3/7.9"	309.3"	309.3"	302.4"	300"	300"	300 "	300"	300"	300"	300'
Min. Radius of Gyration-In.													10.63	10.84	10.90	10.80	10.80	10.90	10.53	11.20	10.95	10.95	11.18	10.68	10.68	11.18	10.95	10.95
Min. Radius of Gyration-In. Allowable Stress-Lbs./5g.In.	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	19,610	19,620	19,570			19,610								19,670		
Actual Gross Area - Sg. In.	49,19	49.19	88.44	1/4.69	114.69	98.94	74.85	81.85	99.75	99.75	87.10	60.85	60.85	95.60	/3/./9	158.67	158.67	131.19	107.63		60.85	60.85	90.38	106.13	106.13	90.38	60.85	60.8
Vet Area-Sq. In.	40.50		75.82	98.57	98.57	84.82	64,22	70.22	85.63	85.63	74.98	52.22	54.28	95.22	131.19	158.67		131.19	107.25		54.01	54.01	90.05	/05.80	105.80	90.05	54.01	54.0
Actual Unit Stress-Lbs.   Sq. In.		24,050	23,580	23,420	24,250 1%		23,680		23,130			19, 640	M	19,500	19,420	19,390	18,500	19, 300	19,520	18,180	/9,390	17,580	17,000	18,710	19,050	19,090	19,030	
Material	S	S	3	S	5	S	S	S	S	5	S	S	5	3	5	5	5	5	S	5	5	S	S	S	5	\ \frac{1}{S}	S	S
				<u> </u>	···			(x)	(x)	(x)	<del></del>		H		<u> </u>		<u> </u>	1				<u> </u>	<del></del>	(x)	(x)	<u> </u>		

		•					<b>TENSIO</b>	N WE	B ME	<b>MBERS</b>	<b>;</b>	u.						-						CON	<b>MPRESSIO</b>	N WEB	MEMB	ERS								
MI	EMBER 19	00 U901	.901 U902	L902 U903	L903 U904	U904 L90	11905 25 L9	906 0906	6 U9 1907	107 L	1908 1909	U909   910	U910 1 911	U912 1 912	U9/3 / 9/3	U901   901	U902 M902	M902 L902	U903 2 <b>M90</b> 3	M903 2905	U904 M904	M904 L904	U905 1 M905	M905 1 905	U906 M906	M906 1 906	U907 M907	M907	U908 1 908	U909 / 909	1.910	U911 1911	U911 1912	U912   913	U913 ( L914	U914 L91
Dead Load	+	1138	+ 1143	+ 897	+ 755	+ 1038	+ //60	0 + 11	183 +	1055	+ 923	+ 678	+ 250		+ 579	- 967		-1202	- 9/9	- 1064	-1784		-/175	- 1320	-1160	- 1303	- 991	-1134		- 634	- 318	- 30	-126	- 577		- 98
0.8 Dead Load	<i>†</i>	910	+ 915	+ 718	+ 604	+ 830	+ 928	8 + 9	946 +		+ 738	+ 542	+ 200	+ 238	+ 463	- 774	- 847	- 962	- 735	- 851	-1427	- 1490		-1056		- 1042	- 793	- 907	- 678				- 101	-462	<del></del>	- 78
Live Load + Imp Tension																										<u></u>										
Reduced LL+ImpTensic	<i>y</i> 7 <i>+</i>	305	+ 315	+ 227	+ 196	+ 335	+ 33	7 + 3	310 +	298	+ 231	+ 204	+ 184	+ 223	2.74						+ 45	+ 54	+ 56	+ 56	+ 8	+ 8	+ 9	+ 9	+ 23	+ 42	+ 111	+ 154	+ 177	+ 186	+ 188	·
Live Load + Imp Comp																																1				1
Reduced LL+Imp Con						- 119	- 63	3 –	9 –	13	- 47	- 79	- 187	- 141.	- 137	- 239	- 254	- 304	- 211	- 264	- 360	- 397	- 312	- 355	- 275	- 320	- 252	- 300	- 188	- 159	- 147	-131	- 252	- 35L	- 423	- 38
Reduced LL + ImpTen. x		505	+ 522	+ 376	+ 325		+ 559	9 + 5			+ 383	+ 338	+ 305	+ 370	+ 454						+ 75	+ 89	+ 93	+ 93	+ 13	+ 13	+ 15	+ 15	+ 38	+ 70	+ 184	+ 255	+ 293		+ 3/2	
Reduced LL+ImpComp.	*D(CF)e					- 197	- 104	<i>I</i> –	15	22	- 79	- 131	- 310	- 233	- 227	- 396	- 421	- 504	- 350	- 437	- 597	- 658	- 5/7	- 588	- 456	- 530	-418	-497	- 311	- 263	- 243	-217	- 418	- 582	- 701	- 63
Ratio = Line I (Comp.) or Line	ne G   (Ten)					- 0.114	- 0.05	54 - 0	0.0	0.0	- 0.05	-0.12	~0.75	- 0.48	- 0.238						- 0.025	-0.024	-0.048	-0.042	- 0.00	- 0.0	-0.01	-0.0	-0,026	-0.065	-0.33	<u> </u>	-1.40	-0.32		
LL Sidewalk - Tension	+	13	+ 13	+ 10	+ B	+ 17	+ 10	6 +	14 +	13	+ 12	+ //	+ 11	+ //	+ 13					-	+ 2	+ 2	+ 3	+ 3	0	0	0	0	+ /	+ 2	+ 5	+ 7	+ 10	+ 10	+ 9	<u></u>
LL Sidewalk - Comp.						- 6	- 3	3 6	0 -	1	- 2	- 3	- 8	- 7	- 7	- //	- 12	- 14	- 10	- 12	- 21	- <i>23</i>	- 15	- 18	- 13	- 15	- 12	- 14	- //	_ 9	- 8	<del>- 7</del>	- //	- 17	- 21	- 1
Direct Design Stress	+	1428	+ 1450	+ 1104	+ 937	+ 1402	+ /503	3 + 14	173 +	1351	+1133	+891	+ 516	+ 6/9	+ 930	- 1/81	- 1280	- 1480	- 1095	- 1300	- 2045	-2171	- 1472	-1662	- 1397	-1587	-1223	-1223	-1000	- 779	- 505	- 248	- 530	-1061	- 1496	-142
Reverse Design Stress								***************************************									,															***************************************	+ 112			· 7 L
											·								· ·								<del> </del>	·			+	1				1
																																1				
	Holes out																													1	†	1				,
SECTION	for Tension																														,	1				i .
Outer Angles	2 4	x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 1/2	4 x 4 x 3/8	4 x 4 x 3/	4 4x4x	3/4 4 x 4	1 x 3/4 4	x4 x 3/4	4 x 4 x 5/8	4 x 4 x 3/8	4x4x3/8	4 x 4 x 3/8	4 x 4 x 1/2	4 x 4 x 3/8	4 x 4 x 3/4	4x4x3/4	6 x 4 x 1/2	6 x 4 x 1/2	7x4x78	7 x 4 x 3/A	6 x 4 x 3/4	6x4x3/4	4 x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 3/4	4 x 4 x 5/8	4 x 4 x 1/2	4x4x3/8	4 x 4 x 3/8	4 x 4 x 3/A	4 x 4 x 5/8	4 x 4 x 3/4	4 x 4 x 3/
I. Web Plate	3. 24	x 13/16	24 x 13/16	26 x 5⁄8	28 x 1/2	28 x <sup>3</sup> /4	26 x 7/2	8 24 x	x 7/8 2	24 x 3/4	24 x 5/8	24 x 1/2	24 1 3/8	24 x 3/8	24 x 1/2	24 x <sup>3</sup> /4	26 x 3/4	26 x 3/4	28 x 5/8	28 x 5/8	30 x 5/8	30 x 5/8	28 x 7/8	28 x 3/8	26 x 1/8	26 x 1/8	24 1 3/4	24,3/4	24 x 5/8	24 x 1/2	24 x <sup>3</sup> /8 ) 23 x <sup>3</sup> /8**)	24 x 3/8	24 x 3/8	24 x 1/16	24 x 1/2	24 x 3/
Cover Plate	2 23	x 7/6**)	23 x 7/6* *)	23 x 3/8**	23 x 3/8 **	) 23 x 3/8**	23 x 3/8 *	**) 23 x	3/8**) 23	x3/8**) 2	23 x 3/8 * *)	23x 3/8 **)	23 x 3/8**	23x3/8**	24 x 3/8**	23 x 3/8 **)	23 x 7/6**	23 x 7/6 * *.	) 23×7/6**	) 23 x 7/6 **	) 22 x 5/8 * * )	22 x 5/8 **	23 x 7/6**	23 × 7/6**)	23 x 7/6**)	23 x 1/6* *)	23,3/8**)	23 x 3/8 * *	) 23x38**	) 23 x 3/8**)	1 23x 3/8**)	23x 38**)	23x3x*	23 x 3/4 **)	23 x 7/6**)	23 x 3/8*
Inner Angles	2														7			4 x 4 x 3/8		4 x 4 x 3/8		4 x 4 x 3/8		4 x 4 x 3/8	-	4 1 4 1 3/8		4 x 4 x 3/	<del>-</del>			1		Ŭ		
2. Web Plate	3																				30 x 5/8										†	1			24 x 1/2	
																															†	1				
																															1				•	·
Length - In.					<b>_</b>											408"	496 "	496"	636"	636"	816"	8/6"	672"	672"	567"	567"	492	492" 7.55	417"	379.5"	342"	330"	437.2"	437.2"	439.87"	3/8"
Min. Radius of Gyratio												<del> </del>				7.67	7.99	7.77	8.54	8.25	9.08	8.92	8.58	8.28	7. 96	7. 75	7, 75	7.55	7.74	7. 71	7.70		7.70	7.70	7.63	7. 70
<u> Allowable Stress-Lbs./</u>		4,000		24,000		24,000	24,00		000 2	4,000	24,000	24,000		+ <u>-</u>	24,000	<del></del>	18,120	18,120	17,270	17,270		16,160	17,180	17,180	17,540	17,540	18,050	18,050	18,670	18,890	19,090	14,540	18,520	18,520	18,470	14,570
Actual Gross Area-5q.	In.	72.14	72.14	57.25	49.19	73,51	77.0	1 73.	3.51 C	67.51	<i>58.19</i>	45.19	39.19	39./9	49.50		72.14	83.58	65.38	76.82	125.44	/36,88	88.14		78.64	90.08		78.95	58.19	48.75	39.19	39.19	39.19	<del></del>	81.14	39.19
Net Area-Sq. In. Actual Unit Stress-Lk		59.52	59.52	46.75	40.69	60.01 23,370	62.51	/ 60	7. 76	55.51	47.94	37.69	32.44	32.44	40,00	64.19	72.14	83.58	61.78 17,720 2.5%	76.82	125.44	136.88	88.14	99,58	78.64	90.08	67.51	78.95	54.50	42.09	31.33	3/,88	31.33	59.64	81.14	31.88
Actual Unit Stress-LL	<u> 5./ 5q. In.</u>   23	,970 2	4,320 1.5%	23,600	23,000	23,370	24,040 0.	5.% 24,240	1.8% 24,3	40 1.4%	23,640	23,620	15,910	19,080	23,250	18,400	17,730	17,000	17,720 2.6%	16,920	16,300	15,870	16,650	16,700	17,750 1.2%	17,600	18,120	17, 960	18, 350	18,500	16,120	7,460	16,910	17,800	18,540	4,450
Material		S	5	3	<i>S</i>	S	<i>S</i>	5	s	$\mathcal{S}$	${\mathcal S}$	${\mathcal S}$	C	5	5	5	1 5	3	S	S	S	5	S	S	l S	5	l S	5	S	S	5	C	S	3	S	$\overline{c}$

- (x) Heavier Section = Same as in Unit 9 South
   x) Handhole II" wide
   x x) Handhole I0" wide
   S = Special Steel
   C = Carbon Steel

- All dead and live load stresses are in kips.

Line 29, net area for tension or effective gross area for compression.



PART 3

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42 R-17.5

STRESS SHEET UNIT 9 NORTH TRUSS

CUYAHOGA COUNTY CLEVELAND

SCALE None MADE H.W.L.DATE 5-8-54 TRCD*NAM\_fA.H.*DATE 9-24-54 CKD *G.H.H.* DATE 7-24-54

HOWARD, NEEDLES, TAMMEN & BERGENDOFF

KANSAS CITY CLEVELAND NEW YORK 914-IA SHEET 2.89

mcrofiled FEB 16 (%)

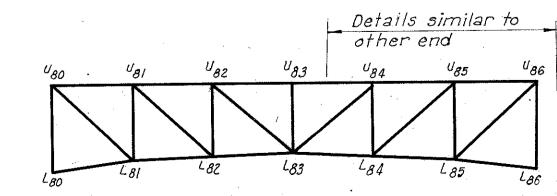
<u></u>																							<del></del>	<u> </u>	
	TENSION	CHOR	D-SOUT	H TRUS	SS	COMP	RESSION	CHORE	SOUT	H TRUS	SS	INE		•	TENSION	CHORD	-NORTH	I TRUS	S	COM	PRESSI	ON CHO	RD-NOR		USS
L80	L 81 , 00	L82	L83 L84		L 85 . L 86	U80 U8/	U81 U82	U82 U83	U 83 U 84	U84 U85	U 85 U 86	-	MEMBER	L <b>8</b> 0 L 81	L81	L82 L83	L83 L84	L84 L85	L.85 L.86	U80 U81	U81 U82	U 82 U 83	U 83 U84	U 84 U 85	U85 U86
0 4.81	+ 731	+ 1, 222	+1,222	+ 731	2	- 7 <i>31</i>	-1,221	-1,445	-1,445	-1.221	-731	1	Dead Load	0	+ 784	+ 1,312		+ 784	0	- 783	-1,311	- 1,550	- 1,550	- 1,311	- 783
0	+ 585	+ 978	+ 978	+ 585	0	- 585	-,227	7	-1,156	977	- 585	2	0.8 Dead Load	0	+ 627	+1,050		+ 627	0			-1,240		-1,049	- 626
0	+ 227	+ 366	+ 366	+ 277	0	380	- 1, 9 17	-1,750	-7,130	511	505	2	Live Load + Impact - Tension	0	+ 246	+ 397	+ 397	+ 246	0						
0	+ 227	+ 366	+ 366	+ 277	0	ļ	<b>-</b>					1	Reduced L.L + Impact - Tension	Ö	+ 246	+ 397		+ 246	0						
0	7 6 6 7	7 300	7 300	7 617	0	- 227	- 366	- 407	- 407	- 366	- 227	<u>4</u>	Live Load + Impact - Comp		7 240	1 007	, 337	, ,,,,		- 246	- 397	- 441	- 441	- 397	- 246
						- 227	- 366	- 407	- 407	- 366		6	Reduced L.L. + Impact - Comp.							- 246	- 397	- 441	- 441	- <i>3</i> 97	- 246
	+ 376	+ 606	t 606	+ 376	0	- 221	- 300	407	407	300	2 4 7	7	Red. L.L. + ImpTension x D (C F) e	0	+ 408	+ 658	+ 658	+ 408	0						** **
- 0	7 3 10	7 800	1 000	1 370	-	- 376	- 606	- 675	- 675	- 606	- 376	92	Red. L.L. + Imp Comp. x D (CF) e	1	1 400	<del>                                     </del>	* 000	7 400		- 408	- 6 <i>58</i>	- 731	- 731	- 658	- 408
						3/6	7 000	075	- 070	- 000	- 310	0								400		, , ,			
			1 12	<u> </u>				***************************************				9	Ratio = Line 1 comp or Line 1 (Tension)	<b> </b>	1	16	+ 16	+ 10	0						
0	+ 9	+ 15	+ 15	+ 9	0		1.5		7.5	/ =		10	L.L. Sidewalk - Tension	0	+ 10	+ 16	7 10	T IU	<u> </u>	- 10	- 16	- 19	- /9	- 16	- 10
***************************************						- 9	- 15	- 18	- 18	- 15	- 9	11	L. L. Sidewalk - Compression		1	1 1 2 2 4	1 1 70 4	1.045		L		–		-1,723	-1,044
0	+ 970	+1,599	+1,599	+ 970	0	- 970	-1,598	-1,849	- 1,849	- 1,598	- 97 <i>0</i>	12	Direct Design Stress-2+++++++++++++++++++++++++++++++++++	0	+1,045	+1,724	+1,124	+1,045	0	-1,044	-1,723	- 1,990	-1,990	-1, 163	-1,044
								·				13	Reverse Design Stress												
·		,										14													
						4					:	15			1							***			
												<i>i6</i>													
												17			`										
4 x 4 x 5/16	4x4x3/8	4x4 x 1/8	$4 \times 4 \times \frac{3}{8}$	4x4x3/8	4 x 4 x 5/16	8x6x7/6	8x6x 7/16	8 x 6 x 1/2	8x6x1/2	8 x 6 x 5/16	8 x 6 x 1/16		Section												
30 x <sup>3</sup> /8	30 x 7/16	30 x 7/16	30 x 7/16	30 x 7/16	30 x 3/8	30 x 3/8	30 x 3/8	30 x 3/4	30 x 3/4	30 x 3/8	30 x 3/8		a Flange Angles . 2 2	4 x 4 x 5/16	4 x 4 x 3/8	4 x 4 x 3/8	4 x 4 x 3/8	4x4x3/8	4 x 4 x 5/16	8 x 6 x /2				8x6x1/2	
23 x 5/16	23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8	23 x 716	23 x 3/8	23 x 3/8	23 x 3/8	23 1 3/8	23 x 3/8	23 x 3/8		b 1st Web Plate 2 4	30 x 3/8	30 x 1/2	30 x 1/2	30 x 1/2	30 x 1/2	30 x 3/8	30 x <sup>3</sup> /8		30 x <sup>13</sup> /16	30 x 13/16		30 x 3/8
23 x36 (11" Hole)	23 x /2 (11"Hole)	23x/2 (11"Hole)	23x2 (11" Hole)	23 x /2 (11"Hole)	23x 3/8 (11"Hole)	23x /2 (11"Hole	23 x /2 (11" Hole)	23x/2 (11 "Hole)	23x /2 (11"Hole)	23x1/2 (11"Hole)	23x1/2 (11"Hole)		c Top Cover Plate 🔑 3	23 x 5/16	23 x 3/8	23 x 3/8		23 x 3/8		23 x 3/8		23 x 3/8	23 x 3/8	23 x 3/8	23 x 3/8
		30 x 1/2	30 x 1/2		-		30 x 3/8			30 x 3/8			d Bottom Cover Plate & 2	23 x 3/8 (11" Hole	) 23x/2 (11"Hole)	23x /2 (11"Hole)	23x1/2 (11" Hole)	23x1/2 (11"Hole)	23x 3 (11" Hole)	23 x 1/2 (11"Hole)	23x /2 (11"Hole)	23 x/2 (11"Hole)	23x1/2 (11"Hole)	23 x ½ (11"Hole)	23x1/2 (11"Hole)
				·				14 x 3/8	14 x 3/8				g 2nd Web Plate 4			30 x 1/2	30 x 1/2				30 x <sup>7</sup> 16			30 x 7/16	
			*	***************************************									h Inside Web Plate 3 2									14 x 7/16	14 x 7/6		
				1		<u> </u>		٠,,					8											*	
					, .	1															,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				
					. نهر								H												
		<u> </u>			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	300	300	300	300	300	300	25	Length In.							300"	300"	300"	300"	300"	300"
				1		10.63	11.19	11.00	11.00	11.19	10.63	26	Min. Radius of Gyration In							10.59	11.18	10.84	10.84	11.18	10.59
18,000	24,000	.24,000	24,000	24,000	18,000	19,630	19,670	19,660	19,660	19,670	19,630	27	Allowable Stress Lbs./Sq./		24,000	24,000	24,000	24,000	18,000	19,630	19,670	19,650	19,650	19,670	19,630
43.79	52.32	82,32	82.32	52.32	43.79	60.85	83.35	97.13	97.13	83,35		28		43.79	56.07	86.07	86.07	56.07	43.79	64.13	90.38	102.63	102.63	90.38	64.13
36.60	43.69	69.69	69.69	43.69	36,60	54.28	82.97	96.75	96.75	82.97	54.28	29			46.94	72.94	72.94	46.94	36.60	<i>57.56</i>	90.00	102.25	102.25	90.00	<i>57.56</i>
20.00	40.03	03.03	0.3.03	40.03	20,00	14.00	06,01	30.10	30.10	1 04.37	U4760	<u></u>	1 , 10 , 11 , 10	·II ~~~~~	70,01	1 ,								/ A 1 47 A	150

+ 993       + 654       + 293       + 293         + 794       + 523       + 234       + 234         + 308       + 226       + 146       + 146         + 308       + 226       + 146       + 146         -19       - 54       - 54         -19       - 54       - 54         + 510       + 374       + 242       + 242         - 31       - 89       - 89	2 L 83 L 83 U84 293 + 293 234 + 234 146 + 146 146 + 146 54 - 54	L84 U85 L85 3 +654 + 4 +523 + 5 +226 +	5 U86 U80 L80 + 993 - 738 + 794 - 591	-547	U82 _ L82					NE.					RS - NO			1100	101	1102	(103	1100		
+993 $+654$ $+293$ $+293+794$ $+523$ $+234$ $+234+308$ $+226$ $+146$ $+146+308$ $+226$ $+146$ $+146-19$ $-54$ $-54-19$ $-54$ $-54+510$ $+374$ $+242$ $+242-31$ $-89$ $-89-0.029$ $-0.184$ $-0.184+12$ $+9$ $+5$ $+5-2$ $-2+1.316$ $+906$ $+481$ $+481+4814 \times 4 \times \frac{1}{2} \times 4 \times 4 \times \frac{1}{2} \times 4 \times 4 \times \frac{3}{2} \times 4 \times 4 \times \frac{3}{2} \times 24 \times $	293 + 293 234 + 234 146 + 146 146 + 146 54 - 54 - 54 - 54	3 + 654 + 4 + 523 + 5 + 226 +	+ 993   - 738 + 794   - 591	-547	- 20A			/ 851	L86		MEMBER	U80 L81	U81 L82	182 L83	183 U84 L	:84 U85 L	.85 U86	U80 L80 L	U81 L81	U82 L82	U83 L83	U84 L84	185 L85	186 L86
+794 $+523$ $+234$ $+234+308$ $+226$ $+146$ $+146+308$ $+226$ $+146$ $+146-19$ $-54$ $-54-19$ $-54$ $-54+510$ $+374$ $+242$ $+242-31$ $-89$ $-89-0.029$ $-0.184$ $-0.184+12$ $+9$ $+5$ $+5-2$ $-2+1.316$ $+906$ $+481$ $+481+4814 \times 4 \times \frac{1}{2} 4 \times 4 \times \frac{1}{2} 4 \times 4 \times \frac{3}{2} 4 \times 4 \times \frac{3}{2} 24 \times \frac{3}{2} 23 \times \frac{3}{2} (10"Hole) 23 \times \frac{3}{2} (10"Hole)$	234 + 234 146 + 146 146 + 146 54 - 54 - 54 - 54	4 + 523 + 5 + 226 +	+794 - 591			-118	-298	- 547	-809	7	Dead Load	+1,062	+ 705	+312	+312	+ 705	+1,062	- 804	- 596	- 332	- 139	- 332	- 596	- 876
+308 $+226$ $+146$ $+146+308$ $+226$ $+146$ $+146-19$ $-54$ $-54-19$ $-54$ $-54+510$ $+374$ $+242$ $+242-31$ $-89$ $-89-0.029$ $-0.184$ $-0.184+12$ $+9$ $+5$ $+5-2$ $-2+1.316$ $+906$ $+481$ $+481+4814 \times 4 \times \frac{1}{2} 4 \times 4 \times \frac{1}{2} 4 \times 4 \times \frac{3}{2} 4 \times 4 \times \frac{3}{2}$	146 + 146 146 + 146 54 - 54 - 54 - 54	5 + 226 +	1	- 438	- 238	- 94	- 238	- 438	- 647	2	0.8 Dead Load	+ 850	+ 564	+ 250	+ 250	+564	+ 850	- 643	- 4.77	- 266	- ///	- 266	-477	- 701
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	146 + 146 54 - 54 - 54 - 54		+ 308		+ 15		+ 15			3	Live Load + Impact - Tension	+ 334	+ 245	+158	+ 158	+245	+ 334			+ 16		+ 16		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	- 54 - 54	1	+ 308		+ 15		+15			4	Reduced LL+ Impact - Tension	+ 334	+ 245	+158	+158		+ 334			+ 16		+ /6		
+ 510		7 - 19	- 21.9	-164	- 103	- 47	- 103	-164	- 224	5	Live Load + Impact - Comp.		- 21	- 58	- 58	- 21		- 237	- /78	- 111	- 51	- ///	- 178	- 244
- 31 - 89 - 89 -0.029 - 0.184 - 0.184 + 12 + 9 + 5 + 5 -2 - 2 +1.316 + 906 + 481 + 481 4 x 4 x ½ 4 x 4 x ½ 4 x 4 x 3/8 4 x 4 x 3/8 24 x 3/6 24 x 3/6 24 x 3/8 24 x 3/8 22 x 3/6 (10"Hole) 23 x 3/6 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole)	242 +242		-219	- 164	- 103	- 47	- 103	- 164	-221	6	Reduced L.L.+ Impact - Comp.		- 21	- 58	- 58	- 21		- 237	-178	- 111	- 51	- ///	- 178	- 240
-0.029 -0.184 -0.184 +12 +9 +5 +5 -2 -2 +1.316 +906 +481 +481 4 x 4 x ½ 4 x 4 x ½ 4 x 4 x 3/8 24 x ½ 24 x ½ 24 x 3/8 22 x ½ (10"Hole) 23			+ 5/0		+ 25		+ 25		.,	7	Reduced L.L. + ImpTension x D (CF) e	+ 553	+ 406	+262	+262		+553			+ 26		+ 26	0.05	
+ 12 + 9 + 5 + 5 - 2 - 2 + 1,316 + 906 + 481 + 481 4 x 4 x ½ 4 x 4 x ½ 4 x 4 x 3/8 4 x 4 x 3/8 24 x 3/6 24 x 3/6 24 x 3/8 24 x 3/8 22 x 3/6 (10"Hole) 23 x 3/6 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole)			- 363	-272	- /7/	- 78	- 171	-272	- 366	8	Reduced L.L. + Imp Comp. x D (CF) e		- 35	- <b>. 9</b> 6	- 96	- 35		- 393	- 295	- 184	- 85	- 1.8:4	- 295	- 398
-2 -2 +1.316 +906 +481 +481 4 x 4 x ½ 4 x 4 x ½ 4 x 4 x ¾ 4 x 4 x ½ 24 x ¾ 6 24 x ¾ 6 24 x ¾ 24 x ¾ 8 22 x ¾ 6 (0"Hole) 23 x ¾ 6 (10"Hole) 23 x ¾ (10"Hole)	0.184 - 0.184	4 -0.029			-0.020		-0.020			9	Ratio = Line 4 or Line 6 Line 1 (Tension)		0.030	0.186	0.186	0.030				- 0.048		-0.048		
+1.316 +906 +481 +481 4 x 4 x 1/2 4 x 4 x 1/2 4 x 4 x 3/8 4 x 4 x 3/8 24 x 3/6 24 x 3/6 24 x 3/8 24 x 3/8 22 x 3/6 (10"Hole) 23 x 3/6 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole)	+5 +5	+ 9 +	+ 12		+ 1		+ /			10	L.L. Sidewalk - Tension	+ 13	+9	+6	+6	+ 9	+ 13				· · · · · · · · · · · · · · · · · · ·	1	- 7	÷ 10
4 x 4 x ½ 4 x 4 x ½ 4 x 4 x ¾ 4 x 4 x ¾ 2 24 x ¾ 6 24 x ¾ 6 24 x ¾ 6 24 x ¾ 8 24 x ¾ 8 22 x ¾ 6 (10"Hole) 23			- 10	- 7	- 4	-/	- 4	- 7	- 10	11	L. L. Sidewalk - Compression		-0.4	-2	- 2	-0.4		- 10	-/	- 4	- /	- 4	- <i>1</i> - 779	-1109
24 x 7/6	481 + 481	1 + 906 + 1.	1.316 - 964	- 7/7	- 413	-173	-413	-717	-1023	12	Direct Design Stress @+7+@or @+8+1	+ 1,416	+ 9.79	+518	+5/8	f 979	+1,416	-1046	- 779	-454	- 197	- 454	- //9	-1109
24 x 7/6 24 x 7/6 24 x 3/8 24 x 3/8 22 x 7/6 (10"Hole) 23 x 3/6 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole) 23 x 3/8 (10"Hole)										13	Reverse Design Stress													
24 x 1/6 24 x 1/6 24 x 1/8 24 x 1/8 22 x 1/6 (10"Hole) 23 x 1/6 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole)				· · · · · · · · · · · · · · · · · · ·		<b></b>				14										I				
24 x 1/6 24 x 1/6 24 x 1/8 24 x 1/8 22 x 1/6 (10"Hole) 23 x 1/6 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole)	<u></u>					<b></b>				15														
24 x 1/6 24 x 1/6 24 x 1/8 24 x 1/8 22 x 1/6 (10"Hole) 23 x 1/6 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole)					<b></b>					16	:		<u> </u>							l	<b> </b>			
24 x 1/6 24 x 1/6 24 x 1/8 24 x 1/8 22 x 1/6 (10"Hole) 23 x 1/6 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole)					-	<del></del>				1/		18												
24 x 1/6 24 x 1/6 24 x 1/8 24 x 1/8 22 x 1/6 (10"Hole) 23 x 1/6 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole) 23 x 1/8 (10"Hole)	34 4 34	3.		3,	1 3 3	1 3/	3,	4 4 34	A - 100 y 100 y 200 y 200 1		Section E	1 1 1/2	1 - 1 - 1/2	3. 1. 3.	1 1 30	1 1 1/2	1 1 1 1/2	11.3/0	1 × 1 × 3/2	1 1 1 3/0	4 x 4 x 3/8	1 , 1 , 3/2	1 × 1 × 3/0	1 1 1 , 3/0
82 x 2/16(10"Hole) 23 x 2/16(10"Hole) 23 x 3/8(10"Hole) 23 x 3/8(10"Hole)					4 x 4 x 3/8						a. Flange Angles 5 2 b. 1st Web Plate 5 3		4x4x1/2 24x1/2	$\frac{4 \times 4 \times 8}{24 \times \frac{3}{8}}$	24 x 3/8	21 x 1/2	24 x 1/2	24 x <sup>3</sup> / <sub>4</sub>	24 x 9/16	21 × 3/0	24 x 3/8	21 × 3/0	21 × 9/16	24 x 3/4
22 x 7/6 (10 Hole) 23 x 7/6 (10 Hole) 23 x 7/8 (10 Hole) 23 x 7/8 (10 Hole)	$\frac{4x}{8}$ $\frac{24x}{8}$	$\frac{7}{8}$ $\frac{24 \times 7}{16}$ $\frac{2}{3}$	24 x 1/16 24 x 1/16	6 24 x 1/2	24 x 3/8	24 x 3/8	24 x 3/8	24 x 1/2	24 x 11/16			- 24 x 1/2	24 X /2	24 × 78	24 X /8	24 X /2	2.3.(10"Hola)				23x3/8 (10"Hole)			
24 x 716	(10"Hole) 23x78 (10"Hole)	)(e) C3x716(10"Hole) ZZ x4	76 (10" HOIE) 23x % (10 HOIE	2) C3 x 10 (10" 1101e)	C3x78(10"Hole)	23 x 79 (10 Hole)	23x78(IV NOIE)	CJ X/8 ( NO HOIE)	Z3X78(  U NOIE)		C. Cover Plates = 2	24 x 1/2	LUX/16(10 note) C	3178 (10 1101@)	cox & (10 Hole) c	JANIB (IU TIOIE) ZI	24 x 1/2	CJX78 (10 HOIE) C	3x 8 (10 1101E) 1	CJA 18 (10 HOIE)	CSA-8(ID HOTE)	CSC 8 (10 HOTE)	(27 /8 (10 11010)	coxia (io moto)
			4 x //6			<del> </del>					g. 2nd Web Plate 5 3	£4 x/2.					C4 × /2							
	<u> </u>					<del> </del>					3	<b></b>												
						<b> </b>																		
						1					<u> </u>	1					1							
					-						10										<u> </u>			
			320	276	264	252	264	276.	320	25	Length /n.	1						320	276	264	252	264	276	320
	1		7.60		7.70	7.70	7.70	7.60	7,60	26	Min. Radius of Gyration In.							7.47	7. 56	7.70	* 7.70	7.70	7,56	7.47
24,000 24,000 18,000 18,000		0 24,000 24	4,000 19,180	<del></del>	14,700	, ·	14, 700	19,390	19,180	27	Allowable Stress Lbs./Sq./n.	24 000	24,000	18,000	18,000	24,000	24,000	19,150	19, 390	14,700		14.700	19,390	19,150
	000 18 000		67.50 57.75		39.19	39./9	39.19	45.19	57.75	28	Actual Gross Area Sq. In.		50.38	39.19	39.19	50.38	72.00	57.19	48.19	39.19	39. / 9	39.19	48.19	57.19
	8,000 18,000 19 19 39 19	4 39.01 5	56.50 56.20	0 38.52	31,88	31.88	31.88	38.52	56.20	29	Net Area Sq. In.	60.50	41.63	32.44	32.44	41.63	60.50	57.19	42.79	31.88	31.88	31.88	42.79	<i>57. [9</i>
	39.19 39.19		3,270 17,150			5,420	12,950	18,610	18,220	30	Actual Unit Stress Lbs./Sq. In.		23,500	15,960	15,690	23,500	23,410	18,290	18,200	14,240	6,180	14,240	18,200	19,390
S $S$ $C$ $C$	39.19 39.19 32.44 32.44	10 1 2.5 2 10 1 2 2		- 5	$\frac{1}{C}$	C	C	S	5	31	Material	5	3	C	C	S	3	5	5	C	C	C	Ş	S
	39.19 39.19 32.44 32.44	20 23,230 23 S	S II S		*					H		#	t				i	1				1 .		

S = Special Steel C = Carbon Steel

All dead and live load stresses are in kips. Line 29, net are for tension or effective gross area for compression.

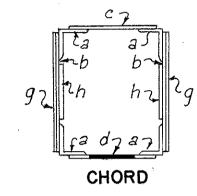
All details are the same as for the respective truss of Unit 6 except as modified by grades. See Sheets 28 and 29.



Truss dimensions are shown on framing plan, Sheet 25.

FEDERAL AID PROJECT NO.

CITY OF CLEVELAND CENTRAL VIADUCT



PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU -42 R-17:5 STRESS SHEET UNIT 8

NORTH AND SOUTH TRUSSES

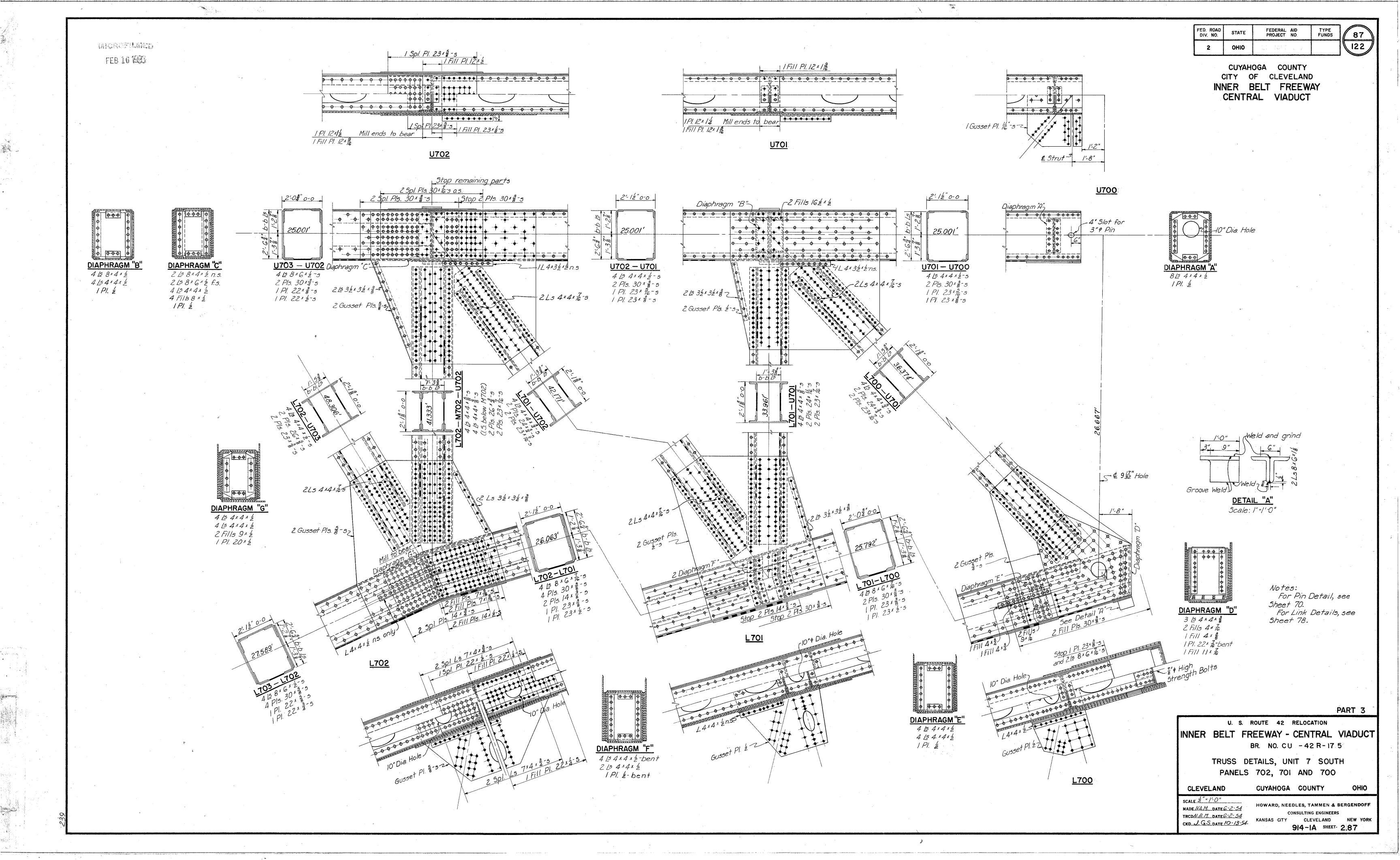
SCALE *None*MADE *D.M. E.* DATE 5: 4:54

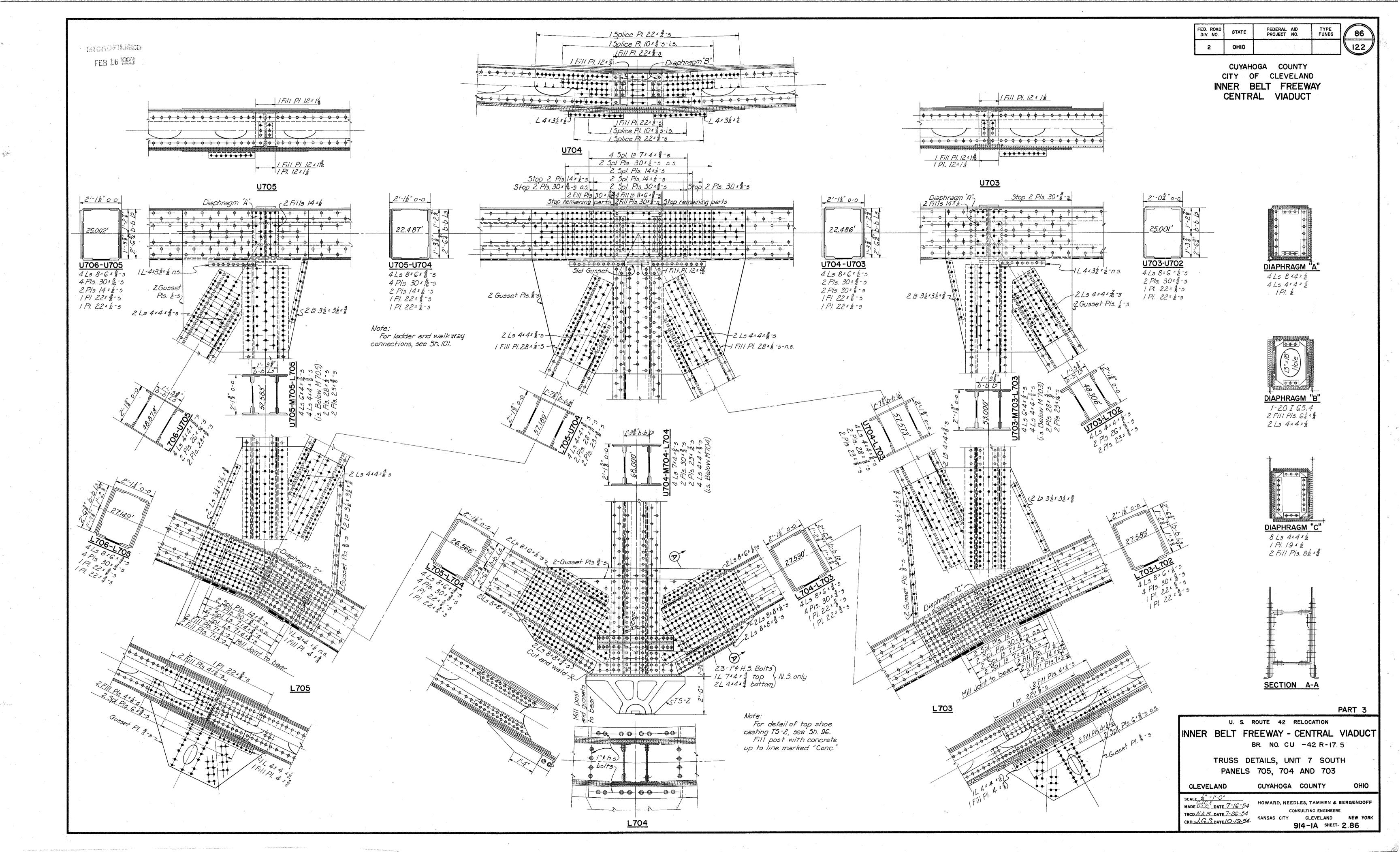
TRCD & A.H. DATE 9:47-54

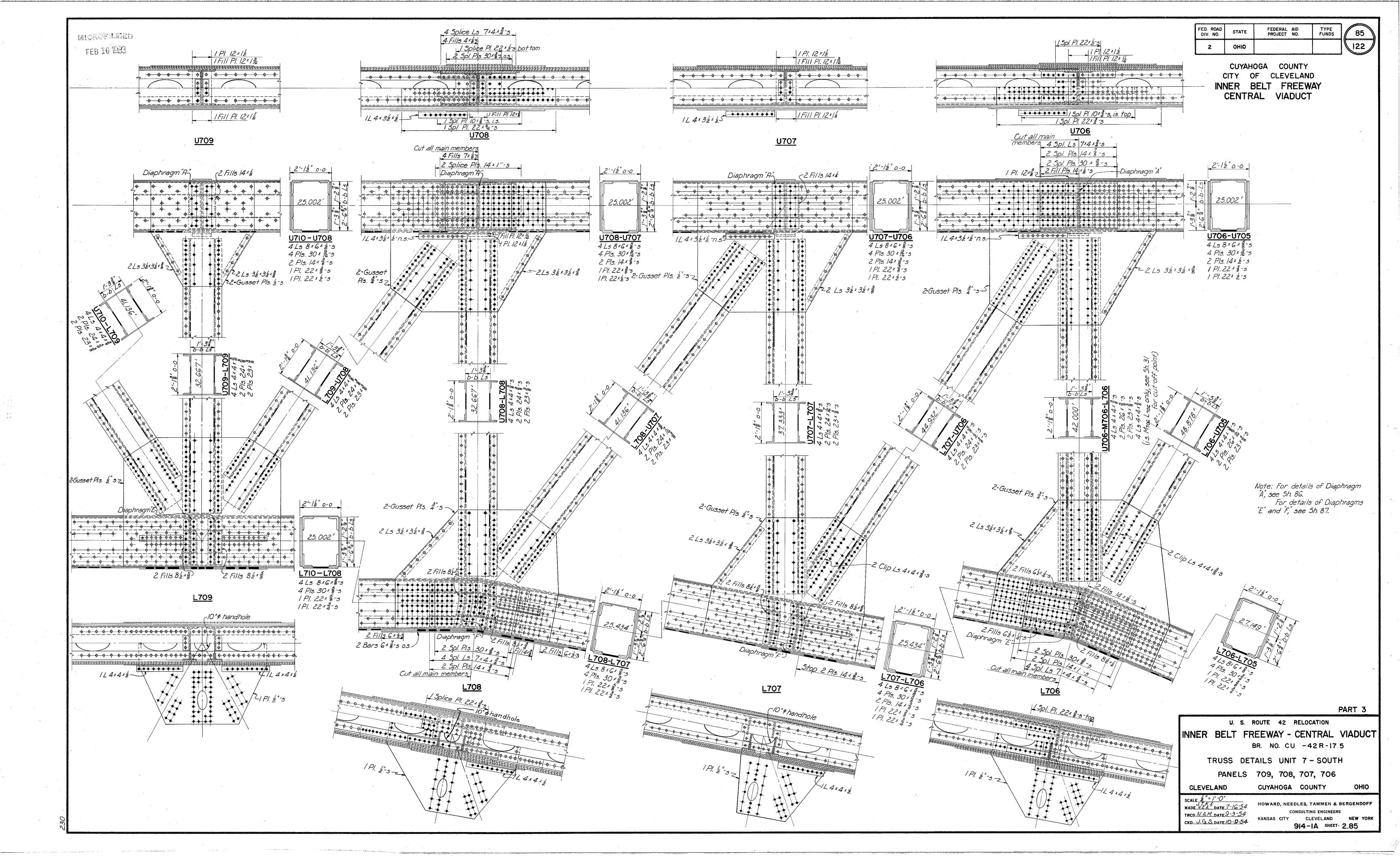
CUYAHOGA COUNTY

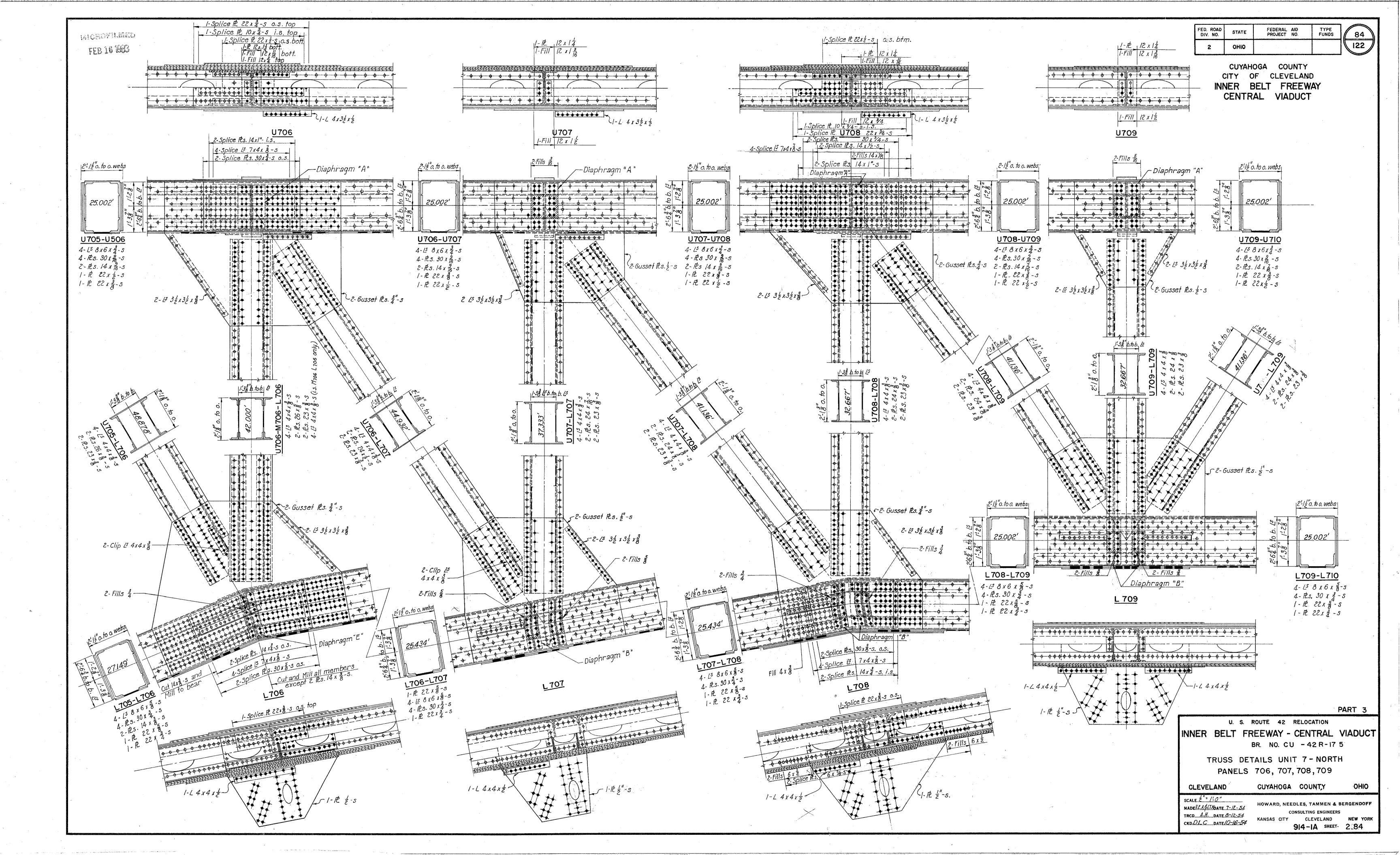
CLEVELAND

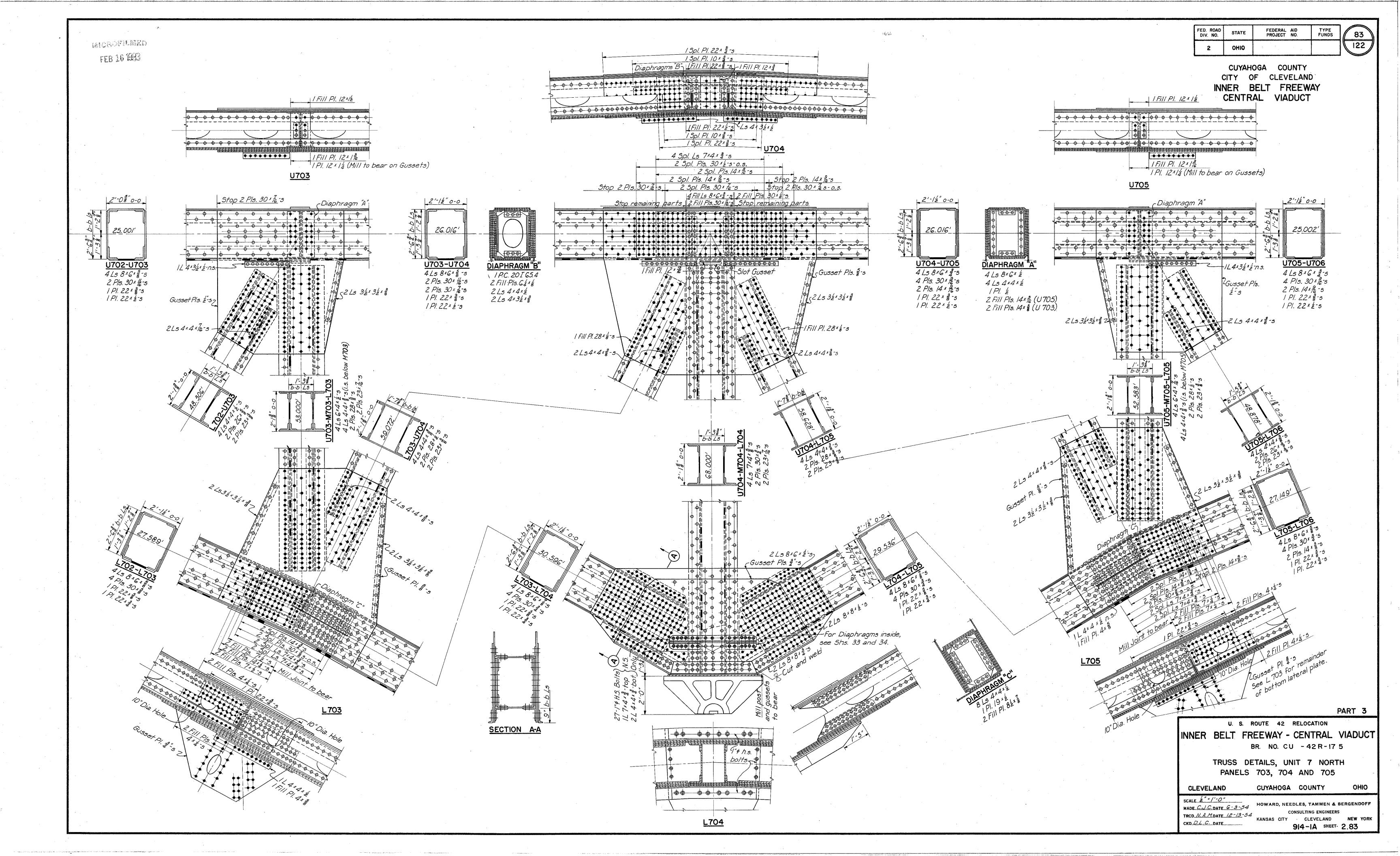
HOWARD, NEEDLES, TAMMEN & BERGENDOFF KANSAS CITY CLEVELAND NEW YORK CKD H.W.L. DATE 5-19-54 914-1A SHEET- 2.88

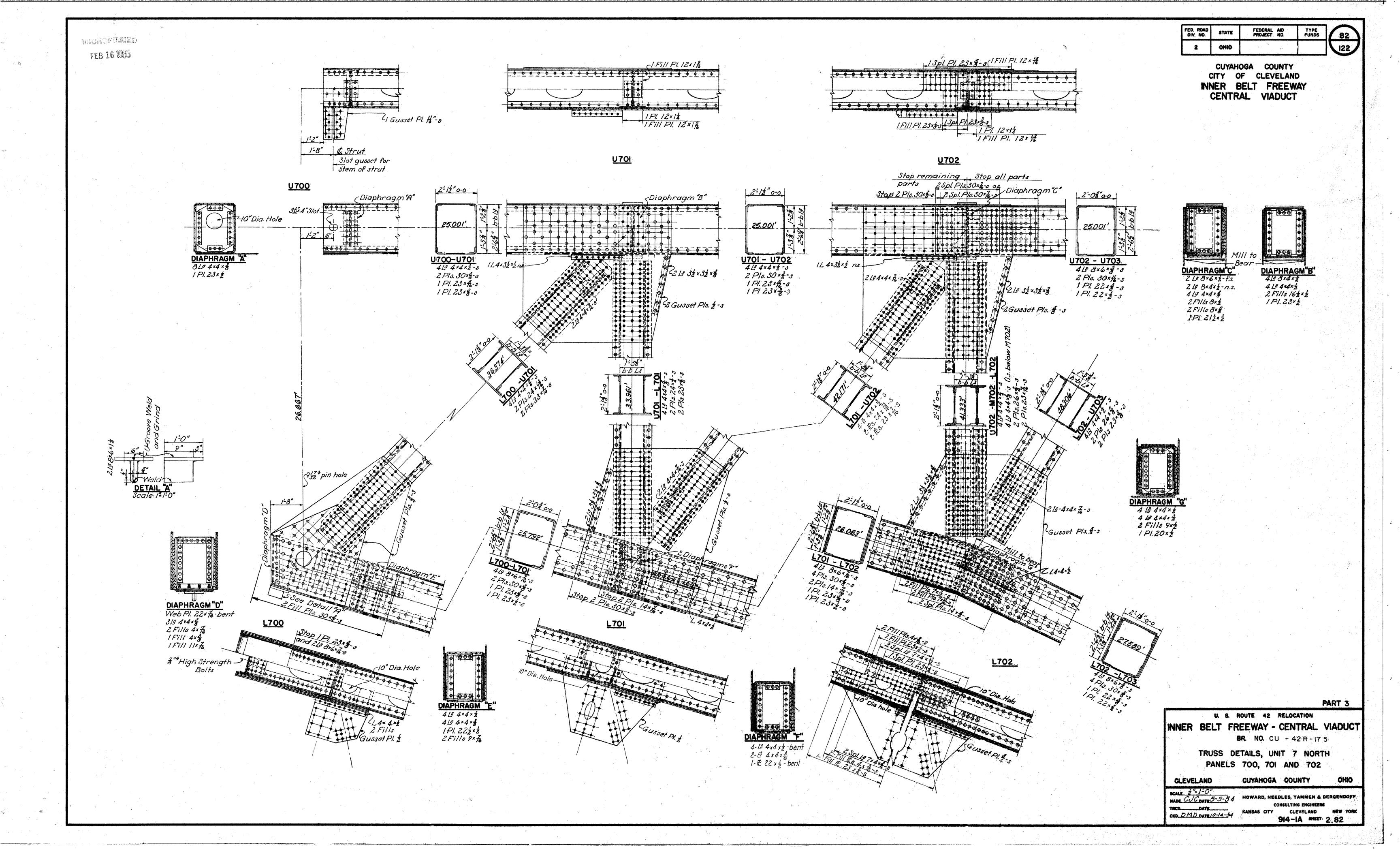












MICROPILINED FEB 16 1603

ED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	81
2	оню			122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

-			. , =-																															CENIR	AL VIA	ADUCT	
L	J					. , , , , , , , , , , , , , , , , , , ,			COM	1PRESSIC	N CHO	RD					**	-	·					,			Ţ	ENSION	CHORD	)		:					
] 3	MEM	ED L 700	L 701	L702	L 703	L704	L 705	L706	L707	L708	L709	1710	L711	L712	L 7/3	L714	L7/5	L7/6	L7/7	U700	U701 U702	U702	U 703	U704	U 705	U706	U707	U 708	U 709	U710	U711	U7/2	U.7/3	U714	U715 /	U716	U717
<u>  -</u>	<del></del>	1	D/ L70		3 <u>L704</u>	L705	L 706		L 708			L711		L7/3	L714	L 715	L 7/6	L 717	L 7/8	U701	U702	U703	U704				U708	<i>U 709</i>	<u>U 7/0</u>		0712	4713		0.715	<u>U 116</u>	<u>U717</u>	0 718
	Dead Load		- 1445		-2486	-2507	-2263	-2006	-/743	-1621	-1626	-1752	-2018	-2277	- 2521	- 2500	- 2041 - 1633	- [4.58	- 775	· P	+ 7 <i>38</i>	+ 1386	<i>+ 1836</i>	+ 2083 + 1666	+ /97/	+ 17.13	+ 1621 + 1297	+ 1510 + 1208	+ 1510	+ 1626 + 1301	+ 1723 + 1379	+ 1983 + 1586	+ 2096	+ 1849	+1398 +1118	+ 743 + 594	
غ ر د	2 0.8 Dead Load 8 Live Load + Imp. Tension	<u>-6/5</u>	- //56	- 1622	-1989	-2006	- 1810	- /605	- /3 <u>94</u>	-/297	-/301	- 1402	-1614	- 1822	- 2017	- 2000	- 1.6 33	- 1166	- 620	,	+ 590	+ 1109	+ /469	7 1666	+1511	+ 1311	+ 1297	+ 1200	+ 1208	+ 1301	1 13 19	+ 1300	71011	7 1400	+	+ 394	
	Live Load + Imp. lension			·	<u> </u>		<u> </u>	· · · · · · · · · · · · · · · · · · ·					ļ										ļ					. 5.10	. 7.0					(1, 4,22)	, 317		
4	1 Reduced LL+Imp.Tension						+ 146	+ 317	+ 473	+ 603	+ 603	+ 473	+ 317	+ 146	<u> </u>	Ε.					+ 200	+ 351	† 440	+ 549	+ 608	+ 646	+ ///	+ //8	+ 118	+ 7/6	+ 644	+ 601	+ 542	+ 433	+ 347	+ 190	
	Live Load + Imp. Comp.																						<u> </u>					2.40									
$\epsilon$	Reduced LL + Imp. Comp.	- 209	- 366	- 484	- 563	- 567	- '598	- 619	- 658	- 7.17	- 716	- 654	- 6/2	- 590		- 557	- 477	- 362	- 204	<u> </u>				- <i>133</i>	- 311	- 464 +1071	- 603	- 6/9	- 619	- 603	- 464	- 3//	- 133 + 898				·
	Reduced LL + Imp. Ten. x D(C)	) @			1	<u> </u>	+ 242	+ 526	+ 785 -1091	+1000	+ 1000 - 1187	+ 785	+ 526	+ 242	ļ						+ 332	+ 582	+ 729		+ /008	+1071	+ 1188		+1190	+1187	+ 1067	4 997	+ 898	+ 7/8	+ 575	+ 325	
18	Reduced LL + Imp. Comp. x D() Ratio = Line 4 Line I (Comp.) or Line I	F) = - 346	- 606	- 802	- 933	- 940	- 991		- 1091	-1188	- 1187	-1084	- 1014	- 978	- 926	- 923	- 791	- 600	-338					- 220	- 515	- 769			- 1028	-1000	- 769	- 517 - 0,16	- 220 - 0.06				
<u> </u>	$Ratio = \frac{Line 4}{Line 1 (Comp.)} or \frac{Line 6}{Line 16}$	en.)					-0.06	-0.16	- 0.27		- 0.37	- 0.27	- 0.16	- 0.06										- 0.06	- 0.16	- 0.27		-0.41	- 0.41	- 0.037	- 0.27	- 0,16	- 0.06				
10	0 L.L. Sidewalk - Tension						+7	+ 15	+ 23	+ 30	+ 30	+ 23	+ 1.5	+ 7							+ 9	+ 16	+ 22	+ 28	+ 31	+ 44	+ 50	+ 50	+ 50	+ 50	+ 44	+ 31	+ 28	+ 22	+ 16	+ 9	
1	I L.L Sidewalk - Comp.	- 9	- 17	- 24			- 3/	- 32				- 44	- 32	- 31	-, 29	- 29	- 24	- 17	- 9					- 6	- 15	- 23	- 30			30	- 23	- 15	- 6				
1.	2 Direct Design Stress 3 Reverse Design Stress	- 970	-1779	-2448	-2951	-2975	- 2832	- 2662	- 2529	-2535	- 25 <b>3</b> 8	-2530	-2660	-2831	-2972	-2952	-2448	- 1783	- 967		+ 931	+ 1707	+ 2220	+ 2604	+ 2616	+ 2486	+ 2535	† 2448	+ 2448	+ 2538	+ 2490	+ 2614	+ 2603	+2220	+ 1709	+ 928	
7.	3 Reverse Design Stress																																				
1.	4								7										-													-	4				<del></del>
7	5																																	1	,		
	SECTION Hole	s out ension		1																ļ														1			
	,		. 3					\$					<u> </u>				-									,											
	a Flange Angles	2 8x6x	16 8 x 6 x 7/	16 8 x 6 x 1/2	8 x 6 x 3/4	8 x 6 x 3/4	8 x 6 x 5/8	8 x 6 x 5/8	8x6x5/8	8 x 6 x 5/8	8 x 6 x 5/8	8x6x5/8	8x6x5/8	8 x 6 x <sup>5</sup> /8	8 x 6 x 3/4	$8 \times 6 \times \frac{3}{4}$	8x6x1/2	8 x 6 x 7/16	8 x 6 x 7/6	4 x 4 x 1/2	2 4x4x1/2	8x6x1/2	8x6x1/2	8 x 6 x 5/8	8 x 6 x 5/8	8 x 6 x 5/8	8 x 6 x 5/8	8x6x1/2	8x6x/2	8x6x5/8	8x6 x 5/8	8x6 x 5/8	8x6x3/8	1 8 x 6 x /2	8 x 6 x /2	4x4x/2	4x4x1/2
1	a Flange Angles b   St Web Plate	1 30 x 3	8 30 x 3/8	30 x <sup>3</sup> /8 22 x <sup>5</sup> /8 22 x <sup>3</sup> /4 **	30 x 3/4	30 x 3/4	30 x 3/4	30 x <sup>5</sup> ∕8	30 x 5/8	30 x 5/8	30 x <sup>5</sup> /8	30 x 5/8	30 x 5/8	30 x 3/4	30 x 3/4	30 x 3/4	30 x 5/8	30 x <sup>3</sup> /8	30 x 3/8	30 x 3/8	30 x 3/8	30 x 3/4	30 x <sup>3</sup> /4	8 x 6 x <sup>5</sup> /8 30 x <sup>9</sup> /16 22 x <sup>3</sup> /8	30 x 9/16	. 30 x 3/16	30 x 3/16	30 x 9/16	30 x 9/16	30 x <sup>9</sup> /16	30 x 2/16	30 x %16	30 x 9/16	30 x 3/4	8 x 6 x ½ 30 x ¾	30 x 3/8	30 x 3/8 23 x 5/6 23 x 3/8 *)
- 1	c Top Cover Plate d Bottom Cover Plate e Ist Inside Web Plate g 2nd Outside Web Plate	3 23 x 2	8 23 x 3/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22 x 5/8	22x5/8	22 x 5/8	22 x 5/8	23 x 3/8	23 x 3/8	23 x 5/16	6 23 x 5/16	22 x 3/8	22 x 3/8	22 x 3/8	22 x 3/8	22 x 3/8	22 x <sup>3</sup> /8. 22 x ½ *)	22 x <sup>3</sup> /8	22 x 3/8	22 x <sup>3</sup> /8 22 x ½ *)	22 x <sup>3</sup> /8	22 x 3/8	, 22 x 3/8	22 x 3/8.	22 x 3/8	23 x 5/16	23 x 5/16
ŀ	d Bottom Cover Plate	2 23 x 1/2 3	·) 23x/2 *)	) 22 x 3/4 **	) 22 x 3/4 * * )	22 x 3/4**)	22×3/4**)	22 x 3/4 * *)	22 x 3/4 * x)	22 x 3/1 * *)	22 x 3/4 * * )	22 x 3/4 * *)	22 x 3/4 * x)	22 x 3/4 * * )	22 x 3/4**	22 x 3/4 * *)	22 x 3/4 * *)	23x1/2*)	23x/2 *)	23x3/8 *.	) 23 x 3/8 *)	22 x 1/2*	) 22 x 1/2 *	) 22 x ½ * ) 14 x ½	22 x 1/2 *)	22 x 1/2 *)	22×2*)	22 x ½ *)	22x1/2*)	22 x /2 *)	22 x ½ * )	22×2*)	(* 5/x 25	(*3'x 55)	22 x /2 *) 1	23 x 3/8 * )	23 x 3/8 *)
İ	e 1st Inside Web Plate	2	14 x 3/8					14 x 3/8					14 x 3/8			1		14 x <sup>3</sup> /8						14, x 1/2	14 x1/2	14 x 3/8	14 x 3/8	14 x 38	14 x 3/8	14 x 3/8	14 x 3/8			1			
1.0	a 2nd Outside Web Plate	4	30 x 3/8	30 x 5/8	30 x 3/4	30 x 3/4	30 x <sup>3</sup> / <sub>4</sub>	30 x 5/8	30 x <sup>5</sup> ⁄8	30 x 5/8	30 x 5/8	30 x 5⁄8	1	30 x 3/4	30 x 3/4	30 x 3/4	30 x 5/8						30 x 3/8	30 x 9/16	30 x 9/16	14 x 3/8 30 x 9/16	- 30 x 9/16	30 x 9/16	30 x 9/16	30 x 3/16	30 x 9/16	30 x 9/16	30 x 3/16	30 x 3/8			
-	h 2nd Inside Web Plate	2										<u> </u>					, -						- · · · ·			,,,,		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					,				
İ													1																						,		
2	5 Length	ln. 3163	312.7	" 331.1"	331.1"	334.0"	325.8"	305.2"	305.2"	300"	300"	305.2"	305.2"	325.8"	334.0'	331.1"	331.J <sup>4</sup>	312.74	3/6.3"		·	1								,			,				
2	6 Min. Radius of Guration	10.6	10.92	" 331.1" 10.95	10.85	10.85	10.90	305.2"	10.90	10.90	10.90	305.2" 10.90	10.92	10.90	10.85	10.85	10.95	10.92	316.3"														,	( -	,		
2	7 Allowable Stress I he		19 620	19 580	19 570	19 560	19.590					19 640				<del>-</del>	19 580		19 590	24 000	24 000	24.000	24 000	24 000	24 000	24.000	24 000	24.000	24,000	24,000	24,000	24,000	24,000	1 24,000	24,000	24,000 * 49.19 40.50	24,000
7	8 Actual Gross Area	Sq.ln. 19,590 Sq.ln. 60.83	19,620 93.85	19,580 124.75	152 51	19,560 152.51	146.19	19,640 141.69	19,640 13 <b>1.</b> 19	19,650 131.19	19,650 131.19	131.19	141.69	19, 590 146.19	/9, 560 152,51	19,570 152.51	124.75	9.3.8.5	60.85	49-19	24,000 49.19	85.75	108.25	128.69	128.69	125.19	125.19	118.75	118.75	125.19	125.19	128.69	128.69	108.25	85.75	49.19	49.19
12	9 Net Area	50./0 54.28	93.47	124.75	19,570 152.51 152.51	152.51	146.19		131.19	131.19	131.19	131.19	141.69	146.19	152.51	152.51	124.75	93.47	54.28	40.50	40.50	73.63	93./3	110.57	110.57	107.57	107.57	102.13	102.13	107.57	24,000 125.19 107.57	110.57	110.57	93.13	73.63	40.50	40.50
3	77 Allowable Stress Lbs, 8 Actual Gross Area 9 Net Area 0 Actual Unit Stress Lbs,	<u>59./n.</u> 54.26 <i>(</i> 59./n. 17,870	93.47 19,000	19,620	19,360	152.51 19,510	146.19	141.69 18,790	19,290	19,350	131,19 19,350	131.19 19,290	/9,640 /41.69 /41.69 /8,790	146.19	19,510	152.51 19,360	19,580 124.75 124.75 19,620	19,620 93.85 93.47 19,000	19,590 60.85 54.28 17,870	10.00	23,000	24,000 85.75 73.63 23,200	24,000 108.25 93./3 23,840	24,000 128.69 110.57 23,550	23.650	24,000 125.19 107.57 23,110	23.570	24,000 118.75 102.13 23,970	23,970	24,000 125.19 107.57 23,600	23,150	24,000 128.69 110.57 23,610	23,550	23,840	24,000 85.75 73.63 23,200	23,000	
	// Material	5	1 5	,522	15,500	5	1 5	1 3	3	5	5	ς ς	1 5	,5,5,5	5	3,000	5,5,5,5	,	1 7 8		5 6	5	5	5	5	.5	5	5	5	5	S	S	S	S	s	S	S
<u></u>	1 laicilai		J 0	<u> </u>			ئ	J	J	J	,	J		, , , , , , , , , , , , , , , , , , ,		1	J	<i>J</i>	<u>U</u>	1 ,	ر ا			<u> </u>		<u> </u>	<u> </u>		<u> </u>		<u> </u>						

COMPRESSION WEB MEMBERS	TENSION WEB MEMBERS
U701 U702 M702 U703 M703 U704 M704 U705 M705 U706 M706 U707 U708 U709 U710 U711 U712 M713 U714 M714 U715 M715 U716 M716 U717 U718 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L706 L707 L708 L709 L710 L711 M712 L712 M713 L713 M714 L714 M715 L715 M716 L716 L717 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L706 L707 L708 L709 L710 L711 M712 L712 M713 L713 M714 L714 M715 L715 M716 L716 L717 L708 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L701 M702 L702 M703 L703 M704 L704 M705 L705 M706 L707 L708 L709 L700 L700 L700 M702 M703 L703 M704 L704 M705 L705 M706 L707 M708 L709 M708 L700 M708 L702 M703 M704 L704 M705 L702 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 L700 M706 M706 M706 M706 M706 M706 M706 M	U718   Z
-907 -1022 -1164 -896 -1031 -662 -1050 -331 -465 -529 -670 -262 -274 -125 -281 -267 -533 -674 -332 -467 -658 -1068 -897 -1032 -1026 -1169 -914 -81	1 -81   Dead Load   +1069 +1097 +870 +589 -42 +218 +464 +151 +182 +190 +158 +469 +219 -43 +587 +872 +1104 +1094
-726 -818 -931 -717 -825 -530 -840 -265 -372 -423 -536 -210 -219 -100 -225 -214 -426 -539 -266 -374 -526 -854 -718 -826 -821 -935 -731 -65	1 -65 2 0.8 Dead Load
	3 Live Load + ImpTension
+ 208     + 178     + 189     + 189     + 155     + 155     + 176     + 150     + 152     + 176     + 158     + 191     + 191     + 208     + 175	4 Reduced LL+ImpTension +294 +288 +222 +160 +340 +366 +312 +290 +247 +247 +290 +312 +386 +340 +159 +220 +284 +288
	5 Live Load + Imp Comp.
	-47 6 Reduced LL+ImpComp260 -220 -188 -221 -212 -213 -225 -191 -221 -259 - 7 Reduced LL+ImpTen.xD(CF) +487 +477 +368 -265 +564 +606 +517 +481 +410 +410 +481 +517 +606 +564 +264 +365 +471 +477
+ 345 + 295 + 313 + 313 + 257 + 292 + 249 + 252 + 262 + 262 + 317 + 317 + 345 + 290 + 252 + 262	
$\begin{bmatrix} -300 \\ -411 \\ -431 \\ -345 \\ -451 \\ -451 \\ -455 \\ -505 \\ -405 \\ -505 $	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$
	9 Ratio = Line 4 (Comp.) or Line 8   -8.11 -1.01 -0.41 -1.46 -1.16 -1.12 -1.42 -0.41 -1.01 -7.91   -7.
	-
-1120 -1241 -1436 -1072 -1268 -1132 -1517 -823 -1003 -886 -1080 -624 -557 -181 -565 -628 -889 -1083 -824 -1005 -1128 -1533 -1069 -1264 -1239 -1435 -1118 -14	13   Reverse Design Stress   +546   -3   -144   -54   -40   -135   -3   +546
	14 10 10 10 10 10 10 10 10 10 10 10 10 10
	SECTION Holes out for Tension
1 4 50 3 4 5 1 4 5 6 4 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 5 6 7 4 7 5 6 7	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\frac{1}{16}$ $\frac{1}{24}$ $\frac{3}{8}$ $\frac{1}{5}$ $$
$\frac{4 \times 4 \times \sqrt{8}}{24 \times \sqrt{16}} \frac{4 \times 4 \times \sqrt{8}}{36 \times 4 \times \sqrt{16}} $	58 4 x 4 x 38
$4 \times 4 \times \frac{3}{8} \qquad 4 \times 4 \times $	e Inside Angles 2
408"     496"     496"     636"     816"     816"     816"     631"     631"     504"     504"     448"     392"     392"     448"     504"     504"     631"     631"     636"     636"     496"     496"     496"     496"     408"     320"       7.69     7.93     7.71     8.54     8.25     9.10     8.80     8.57     8.21     7.95     7.65     7.70     7.70     7.70     7.65     7.95     7.65 <t< td=""><td>3" 320" 25 Length /n.</td></t<>	3" 320" 25 Length /n.
	7.70 26 Min. Radius of Gyration In.
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	10   14,560   27   Allowable Stress   Lbs/Sq./n   24,000
	32 39.19 28 Actual Gross Area Sq. In. 69.14 69.14 57.25 42.19 42.19 43.94 45.19 39.19 39.19 42.19 45.19 43.94 42.19 42.19 57.25 69.14 69.1
61.27 68.82 80.26 62.41 76.82 82.34 93.78 48.31 65.62 50.00 65.04 34.72 31.33 31.88 31.33 34.72 50.00 65.04 48.31 65.62 82.34 93.78 62.41 76.82 68.82 80.26 61.27 31.6	27 31.88 29 Net Area Sq./n. 56.89 56.89 46.75 34.69 35.94 37.69 35.07 32.44 35.07 37.69 35.94 34.69 34.69 46.75 56.89 56
18, 260 18, 040 17, 880 17, 200 16, 500 13, 750 16, 150 17, 050 15, 320 17, 720 16, 620 17, 980 17, 780 56.80 18, 020 17, 150 15, 330 13, 700 16, 350 18, 020 18, 020 17, 150 16, 480 18, 040 17, 880 18, 260 4, 50 18, 020 18,	60 4,520 30 Actual Unit Stress Lbs/Sq.in 23,820 24,040 23,000 21,360 15,750 22,250 23,930 17,500 17,500 17,650 24,030 22,250 15,750 21,300 23,000 24,040 23,980 C 31 Material S S S S S S S S S S S S S S S S S S S

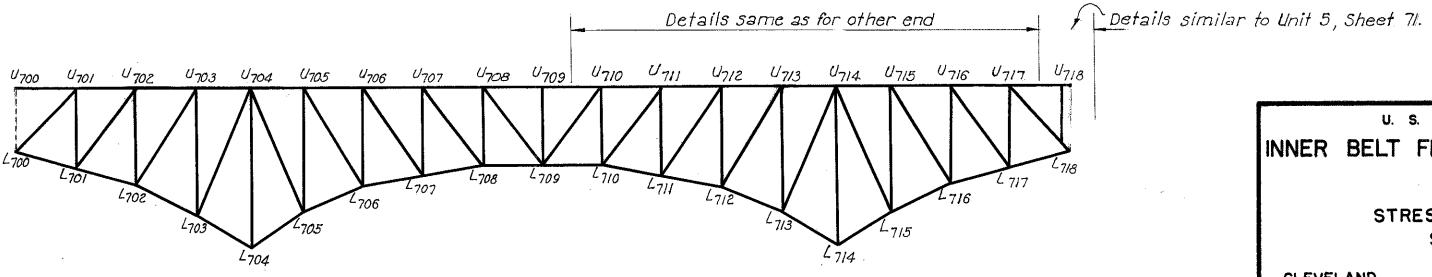
- \*) Handhole II" wide
- \*\*) Handhole 10" wide S = Special Steel C = Carbon Steel

CHORD

WEB MEMBER

18 c2 23

WEB MEMBER



Truss dimensions are shown on framing plan, Sheet 24.

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42 R-17 5

STRESS SHEET UNIT 7 SOUTH TRUSS

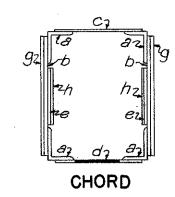
CUYAHOGA COUNTY CLEVELAND

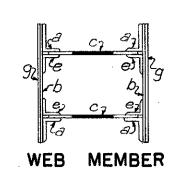
SCALE None

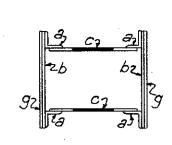
MADE  $\underline{H.W.L.}$  DATE  $\underline{5-17-54}$   $\underline{G.J.K.}$ TRCD  $\underline{\pounds.A.H.}$  DATE  $\underline{9\cdot15\cdot54}$ CKD  $\underline{E.L.}$  DATE  $\underline{\theta\cdot16.54}$ 

HOWARD, NEEDLES, TAMMEN & BERGENDOFF KANSAS CITY CLEVELAND NEW YORK
914-1A SHEET- 2.81

All dead and live load stresses are in kips. Line 29, net area for tension or effective gross area for compression. MCSOFILESD FEB 16 1983







FEDERAL AID PROJECT NO. 122 OHIO

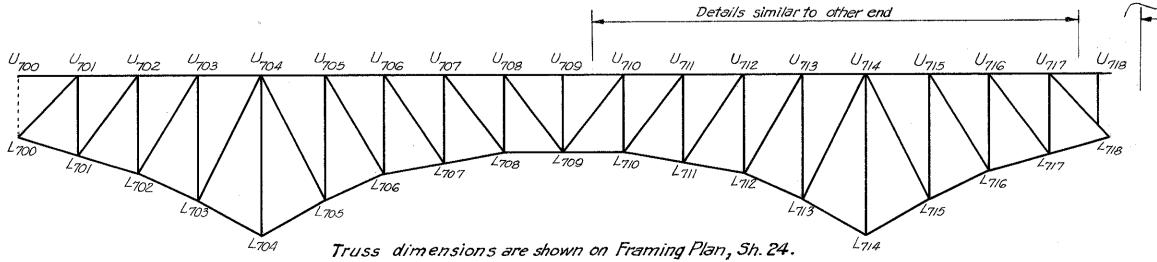
CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT

								CON	<b>MPRESSIO</b>	N CHO	RD												,	`		T	ENSION	CHORD								
MEMBER 4	L 700 L 701	L 701 L 702	L 702 L 703	L703 L704	L 704	L 705 L 704	L 706 L 707	L 707	L 708 L 709	L 709 L 710	L710 L711	L711 L712	L712 L713	L713 L714	L714 L715	L715 L716	L7/6 L7/7	L717 L718	U700 U701	U701 U702	U 702 U 703	U703 U704	U704 U705	U 705 U 706	U 706 U 707	U707 U708	U708 U709	U709 U710	U710 U711	U711 U712	U712 U713	U 713 U 714	U714 U715	1715 U U716	1716 U717	U717 U7
Dead Load	- 790	-1486	-2077		-2578	-2392	-2177	-1951	-1867	÷1892	÷1 <i>99</i> 5	<i>22</i> 37	-2460	-2649	-2631	-2142	-/536	- 819		+ 758	+ 1426	+ 1882	+ 2202	+ 2140	+ 1918	+ 1867	+ 1768	+ 1768	+ 1892	+ 1962	+ 2198	+ 2264	+ 1940		+ 786	
0.8 Dead Load	- 632	-1189	+1662	-2560 -2048	-2578 -2062	-1914		-1561	-1494	-1514	<i>-159</i> 6	-1790	-2460 -1968	+2119	-2105	-1714				+ 606	+ 1141	+ 1506	+ 1762	+ 1712	+ /534.	+ 1494	+ 1414	+ 1414	+ 1514	+ 1570	+ 1758	+ 1811	+ 1522	+ 1179	+ 629	
Live Load +Imp Tension																													******		<u> </u>		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			
Reduced LL+ ImpTension Live Load + ImpComp.						+ 161	+ 325	+ 473	+ 599	+ 599	+ 473	+ 325	+ 161							+ 205	+ 360	+ 448	+ 577	+ 641	+ 689	+ 767	+ 769	+ 769	+ 769	+ 693	+ 650	+ 586	+ 455	+ 367	+ 208	
Live Load + Imp Comp.																															<u> </u>					****
Reduced LL+ImpComp.	+ 214	- 377	<b>~ 494</b>	- 571	<i>+</i> 576	- 624	- 652	- 701	- 767	- 769	- 706	- 662	÷ 635	- 586	+ 581	- 502	÷ <b>38</b> 3	- 219					- 148			+ 5 <b>99</b>				- 465						
Reduced LL+ImpTen.x D(CF)e						+ 267	+ 539	+ 785	+ 993	+ 993	+ 785	+ 539	+ 267							+ 340	+ 596	+ 742	+ 956		+ 1141	+ 1271			1.	+ 1148	1		+ 754	+ 608	+ 345	
Reduced LL+Imp:-Comp.*D(CF)e Ratio=Line 4 Line 6 Line 1 (Ten.)	- 355	-625	+ 818	+947	- <i>9</i> 55	-1034	-1080	-1162	-1271	-1274	+1170	-1097	-1052	- 971	- 963	- 832	<b>~ 63</b> 5	- 363					- 245	<u> - 530</u>		- <b>99</b> 3			- 993		- 530					
Ratio= Line 1 (comp) or Line 1 (ten.)						-0.067	-0.149	-0,242	-0.321	-0.316	-0.237	-0.145	-0:065										÷0.067	-0.149	-0,242	-0.321	-0.347	-0.347	-0.317	-0.237	-0.146	~0.065				
LL Sidewalk - Tension						+ 8	+ 17	+ 25	+ 32	+ 32	+ 25	+ 17	+ 8						_	+ 8	+ 16	+ 21	+ 29	+ 32	+ 46	+ 53	+ 54	+ 54	+ 53	+ 46	+ 32	+ 29	+ 21	+ 16	+ 8	
LL Sidewalk -Comp.	- 9	- 47	- 24	- 29	<i>⊭</i> 29	- 32	- 33	- 47	- 53	- 53	- 47	<b>~</b> 33	- 32	- 29	¥ 29	- 24	- 17	- 9				•	- 8	- 17	- 24	- 32	- 33	- 33	- 32	- 24	- 17	- 8				
Direct Design Stress	- <i>996</i>	-1831	-2504	-3024	+3046	-2980	-2855	-2770	-2818	-2841	-28/3	-2920	-3052	-3/19	-3097	-2570	-1881	-1027		+ 954	+ 1753	+ 2269	+ 2747	+ 2806	+ 2721	+ 2818	+ 2742	+ 2742	+ 2841	+ 2764	+ 2867	+ 2811	+ 2327	+ 1803	+ 982	
Reverse Design Stress		,																						14							ļ <sup>1</sup>					
									,																						<u> </u>					
																															<u> </u>				,	
SECTION Holes out										·																					·					
Flange Angles 2	8x6x 7/16	8x6x 7/16	8x6x ₹	8x6x #	8x6x 7	8x6x ₹	8x6x ₹	8x6x §	8x6x \$	8x6x \$	8x6x ₹	8×6× ₹	8x6x \$	8×6× 7	8x6x 7	8x6x ₹	8x6x 7/16	8x6x 7/16	4x4x ½	4x4x ½	8x6x ₹	8x6x \$	8x6x ⅔	8×6× ⅓	8x6x 3	8x6x ⅔	8x6x 3	8x6x 3	8x6x ₹	8x6x ₹	8x6x 3	8x6x 3	8x6x \$\frac{5}{8}	8×6x ₹	4x4x ½	4x4x 2
	30x ₹	30x 3	30x ₹			30x 3	30x 3	30x 3/4	30x 3/4	30x ¾	30× ¾	30x ₹	30x 3	30× ⅔	30x 3/4	30x ⋅ 3	30x ₹	30x 3	30x ₹	30x ⅔	30x 11/16	30x 11/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 11/16 .	30x 11/16 3	30x ₹	30x å
	23x 🚦	23× ₹	22x \$	22x \$	22x \$	22x \$	22x 3	22x \frac{5}{8}	22x \$	22x \$	22x \$	22x \$	22x ₹	22x \$	22x \$	22x 5	23x #	23x 3	23x 5/16	23x 5/16	22x 3	22x 3	22x 3	22x 3	22x 3	22x 🖁	22x 3	22x 👼	22x 🖁	22x 🖁 2	23x 5/16	23x 5/1				
		23x ½*)	22x 3**	) 22x = **	) 22x 3*	*) 22x 3**	) 22x 3**	*) 22x 3**)	22% 3**)	22x 3**	22x 3**	22x 3**	22 x 3**	1) 22× 3**	) 22x 3**	) 22x 3**	) 23x ½*)	23× (+*)	23x = *	) . 23x 3*	) 22x ½*.	) 22x ½*)	22x ½*)	22x ½*)	22x ½*)	22x 2*	) 22x ½*)	22x 2*	22x ½*)	22x 3*)	22x ½*)	22x ½*)	22x ½*)	22x ½*) 2	23x 3*)	23x 3*.
Inside Web Plate 2		14x 7/16				14x 🛔							14x 3				14x 7/16						14x 9/16	14x 9/16	14x 9/16	14x 9/16	14x 7/16	14x 7/16	14x 9/16	14x 9/16	14x 9/16	14x 9/16				
2 Out side Web Plate 4		30x ₹"	30x ₹	30x 3	30x <sup>3</sup> / <sub>4</sub>		30x 3	30x 3	30x ₹	30x ⅔	30 × 3	30x ₹	30x ₹	30x ₹	30x 3	30x ₹	30x 3					30x 7/16					30x 9/16						30x 7/16			
2 Inside Web Plate 2																															<u></u> '					
																															<b></b> '					,
Length - In.	316.3"	3/2.7"	331.1"	367.1"	375.8"	325.8"	305.2"	305.2"	300"	300"	305.2"	305.2"	325.8"	375.8"	367.1"	331.1"	312.7"	316.3"													<b></b> '					
Min. Radius of Gyration -In.	10.63	10.84	10.90	10.80	10.80	10.8	10.9	10.9	10.90	10.90	10.9	10.9	10.8	10.80	10.80	10.9	10.84	10.63													<u> </u>					
Allowable Stress-Lbs. / Sq. In.	19,590	19,620	19,570	19,470	19,450	19,580	19,640	19,640	19.650	19,650	19,640	19,640	19,580	19,450	19,470	19.570	19,620	19,590	24,000	24,000	24,000 88.44	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000		24,000	24,000			24,000	24,000
Actual Gross Area -Sq. In.	60.85	95. <i>60</i>		158.67	158.67	156.69	146.19	146.19	146.19				156.69	158.67	158.67	131.19	95,60	60.85	49.19	49.19	88.44	114.69	136.76	136.76	136.76	136.76	133.26	133,26	136.76	136.76	136.76	136.76		88.44		49.1
Net Area-5q. In.	54.28	95.22	131.19	158.67			146,19	146.19	146:19	146.19	1	146.19	156.69	158.67	1			54.28	40.50	40.50	75.82		117.39	117.39		1 17.39	114.39	114.39	117.39	· ·			, ,	75.82	t t	40.50
Actual Unit Stress-Lbs./5g.In.	18,380		19,090	19,060		19,020	19,530		19,280		19,240	19,930 1.5		19,660	19,520	19,600	19,750	18,920		23,560	23,120	23,020	23,400	23,900	23,180	24,000	23,970	23,970	24,200	23,550	24,420 6.	23,950	23,610	23,780	24,250	
Material	6		c							e	•	6	9	8			9		9,	9	5	5	9	9	5	s	l 5	S	S	9	1 5	Š	s	S	S	·s

						·····						СО	MPRE	SSION	WEB	MEME	ERS									<u>, , , , , , , , , , , , , , , , , , , </u>			百								TENS	SION W	VEB M	MEMBERS	3				
U	701	02 M	702 L L702	U703 M703	M703 1.703	U704 M704	M704 L704	U 705 M 705	M705 L 705	U 706 M 706	M706 L706	U707	U708	08 L70	0710 19 L71	0 U711	U712	2 M712 2 L7	U713 2 M7	3 M713	3 U714 M7	M714 L7	14 M71	M715	15 U 716	7/6 LT	716 L'	7 U7. 717 L	8 718	MEMBER	L 700 U	0 L 70 1701 U	702 L 702 702 U 7	L 703 03 U 704	U 704 U L 705	705 U76 L706 L	06 U707 .707 L7	708 U 708 108 L 70	L 709 109 U 71	10 U711	L711 U712	L712 L713 U713 U7	14 U714 L 14 L715	1715 U716 L716 L717	U 717 L 718
	935 -1	241 -	1-184	- 899	-1054	- 877	- 780	- 237	- 381	- 463	- 605	- 200	- 25	5 - 12.	- 287	- 224	- 48	- 62	- 24	6 - 391	- 886	- 76	6 -191	7 -106	2 -106	i9 -12	12 - 9	268 -	89 /	Dead Load	+ //	103 +	126 + 88	3 + 766	+ 43	+ 121 +	398 + 8	32 + 16	54 + 2	05 + 113	+ 425	+ 129 + 4	2 + 775	+ 901 + 1161	1 + 1/56
		333 -	947	- 719		- 702	- 624	- 189	- <i>30</i> 5	- 371	- 484	- 160	- 20			<u> </u>							3 - 73	4 - 85	0 - 85	5 - 9	70 - 7	774	71 2	0.8 Dead Load				1	+ 34		1	5						+ 721 + 929	
																													3	Live Load+ Imp Tension															
						+ 176	+ 208	+ 203	+ 203	+ 167	+ 167	+ 188	+ /5	6	+ /53	+ 185	+ 16	+ 164	+ 20	2 + 202	+ 176	+ 21	0						4	Reduced LL+ImpTension	+ 3	300 +	<u> 289 + 21</u>	9 + 186	+ 332	+ 355 +	300 + 28	30 + 24	17 + 2	48 + 280	+ 300	+ 355 + 33	2 + 187	+ 222 + 291	1 + 305
																													5	Live Load + Imp Comp.															
	236 -	247 +	293	- 204	- 254	- 344	<i>- 3</i> 77	- 319	- 362	- 260	- 306	- 237	<u>~ 19</u>	5 - 4	- 198	~ 237	- 26	) - 300	- 31	9 - 366	- 344	<i>- 3</i> 7	16 - 20	5 <i>- 25</i>	6 - 25	0 -2	97 -	238 -	47 6	Reduced LL+ImpComp.					- 244	- <i>236</i> -	202 - 23	37 - 21	5 - 21:	3 - 232	- 197	- 235 - 24	4		` .
						+ 292	+ 345	+ 337	+ 337	+ 277	+ 277	+ 312	+ 25			+ 307			+ 33			<b>I</b>	18						7	Reduced LL+ImpTen. x D(CI		197 +	480 + 36	3 + 308	+ 550	+ 589 +	497 + 46	53 + 40			+ 497	+ 589 + 55	0 + 310	+ 368 + 483	3 + 506
-	392 -	110 -	486	- 338	- 421		+ 625				1	1		3 - 7	- 328	+ 393	- 43	- 50	- 52	9 - 606	- 570	- 62	3 - 34	0 - 42	4 - 41	5 ~ 4	92 -	3 <i>9</i> 5 -	78 8	Reduced LL+ImpComp.xD(C Ratio=Line 1 Comp) or Line 6	cr)e				- 404	- 391 -	<b>335</b> + <b>3</b> 9	<del>23 - 3</del> 5				- 390 - 40			
											- 0.28		- 0.	61	- 0.5	3 - 0.8	3 - O.:	4 - 0.2	6 - 0.	32 - 0.5	2 - 0.2	0 - 0.	27						9		7.)	****			- 5.67	- 1.95 -						-1.82 -5.8			
			*			+ 10	+ 10	+ 14	+ 14	+ 8	+ 8	+ 9	+	9	+ 9	+ 9	+ 8	+ 8	+ 1	4 + 14	+ 10	+ 1	0						. 10	LL Sidewalk "Tension	<u> </u>	13 +	13 + 1	0 + 8	+ 17							+ 17 + 1		+ 10 + 13	3 + 13
-	11 +	12 -	14	- 10	12	- 20	- 22	- 16	- 19	- 13	- 15	+ 11	- 1.	2 -	+ 12	- 11	- 13	- 15	5 - 10	5 - 19	- 20	- 2	2 - 1	0 + 1	2 - 1	2 -	14 -	9	1 //	LL Sidewalk - Comp.					- 17	- 16 -	10 - 1	12 - 1	12 - 12	2 + 12	- 10	- 16 - 1			,
-	151 -1	?55 +	1447	-1067	-1269	-1292	- 1271	- 734	- 924	- 815	+1006	- 564	- 53	9 - 173	- 570	- 583	- 83	-1024	- 74.	2 + 938	-1299	-125	8 -108	4 -128	6 -128	2 -14	76 -1	178 -	150 /2	Direct Design Stress	+ 13	392 +	394 + 107	9 + 929	+ 601	+ 703 +	830 +54	***************************************	54 + 589	9 + 565	<u> + 851</u>	+ 709 + 60		+ 1099 + 1425	5 + 1444
																													/3	Reverse Design Stress					- 387	- 301		89 - 11	0 - 26	26 - 306	,	- 266 - 38	7		
																									************				14																
				,																									15																
,								* 11													,	17.5								SECTION Holes	OUT														
		43	443	Curacid	Garden L	704. 5	7 5	64.746	E. 4. 7/10	- 40:40.3	4		3 4	3 4040	3 444	3 AxAx	3 4444	3 4-4-	3 200 0	466-1-7	16 Tudir	5 70010	5 6010	1 600	1 1000	} axa	- 3 ACA		3	a Flange Angles 2	4x4x	3 4x	x <sup>3</sup> 4x4x	± 4x4x ₹	4x4x 3	4x4x 3 4	x4x 3 4x4x	3 4x4x	<i>3</i> 4x4x	3 4x4x 3	4x4x 3	4x4x 3 4x4x	3 4x4x 3	4x4x ½ 4x4x ¾	4x4x 3
4	. 3	4x 4	26v 3	284 5	200/ 5	720× 3	20x 3	20- 4	20 1	26. 3	26v 3	24×4× 8	924x	2 24×	3 21v	3 24x 7/	16 262	5 484X	2 28	28v d	30%	3 30	5				24	× 3 24	3)	b I. Web Plate 3														26x \$ 74x 13/16	
23	3**1 234	7/15***22	27/18H	23 7/16**1	23×7/16**	23× 7/16**)	2347/16**	23 3++	234 2**1	220 3**	1 22 2**	) 23× 3**	) 23x 2	** 23× 3	*) 23x 3*	*) 23x 24	* 1 23× 3	*) 232 3	*) 23x 3*	*) 232 3	*)23x 7/16	**) 23×741	** 23x7/16	**) 23×7/6			5**) 23x	3**) 23x	2**)	c Cover Plates 2														23x = **) 23x 7/16**)	
-	8 / 27		4x4x 3	204 17 10 1	4x4x }		23× 1/10		4x4x 3		4x4x 3	1	224 8	/ <u>2.32. 8</u>	7 200 8	, , , ,	J 20% B	A - A -	3	4x4x	_			4x4	-1	1~1	3			e Inside Angles 2															
			4X4X g		4848 3				<u>4x4x                                  </u>		4X4X g	<b>-</b>							8		8			707/	8		<b>~</b>			a 2. Web Plate 3															
						T														-																		·						,	
	AOB!!	196"	496"	636"	636"	RIGH	816"	63/11	631"	504"	504"	448"	392	" 3921	302"	448"	504	504	631"	631	816"	816"	636	" <b>63</b> 6	" 496	u 496	" 40	28" 32	on 25	Length - In.															
	7.67			I	1	9.10	1	1	8.21	1	1	7.65	1	i i	i	7.65		7.67			9.10					9 7.7		,		Min. Radius of Gyration-II	7.														
15						16,300			1 .				,			0 18,420				L L	1		£ .			20 18,1	•		0.67	Allowable Stress-Lbs./Sg. 1		000 24,	000 24,00	24,000	24,000	24,000 24	,000 18,0	00 18,00	0 18,00	00 18,000	24,000	24,000 24,0	20 24,000	24,000 24,000	24,000
1,0	4.19 7	2 14	23 58	65.38	76.82		82.34	3		ì	65.13					42,19			54.47					8 76.8		4 83.5				Actual Gross Area - Sa. In			.14 57.2			1			1	i i	{ i	40.69 42.			72.14
		214	33.58	62:41	76.82	82.34			65.72							34.72			48.31				62.4				8 64.		<b>38</b> 29	Net Area-Sg. In.	59	2.52 59	52 46.7				7.69 32.	44 32.4	14 32.4	44 32.44	37.69	33.19 34.6	69 40.69	46.75 59.52	59.52
	,930 17			17,100	1	15.760	15 440	15 200	14.060	16,300	15,490		17 20	0 5 430	JA JA	0 16.800	16.6	0 15.80	0 15.37	****	15.760	15.26	0 17.35	0 16:74	0 17.8	00 17.6	50 18.3	50 4.	700 30	Actual Unit Stress Lbs. / 50	7. In. 23.	390 23,	420 23,00	22,830	17,340 2		020 16,6	80 17,100	10 181180	0.99 17,400	22,560	21,360 17,3	40 23,050	23,510 23,910	24,260 . 2
<u> </u>	5	3	S	S	S	S	5	.5,250	s	S	2	5	5	6	5	S	5	S	Ŝ	S	S	S	S	S	S	S	S		3/	Material	Ś	3	s	S	S	s s	s   E	C	С	ć	S	s s	5	s s	S

<sup>\*)</sup> Handhole || Wide \*\*) Handhole || O" Wide S= Special Steel C= Carbon Steel

All dead and live load stresses are in kips Line 29,- Net area for tension or effective gross area for compression.



Details similar to Unit 5, Sh. 70

PART 3

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R-17 5

STRESS SHEET UNIT 7

NORTH TRUSS

CLEVELAND CUYAHOGA COUNTY

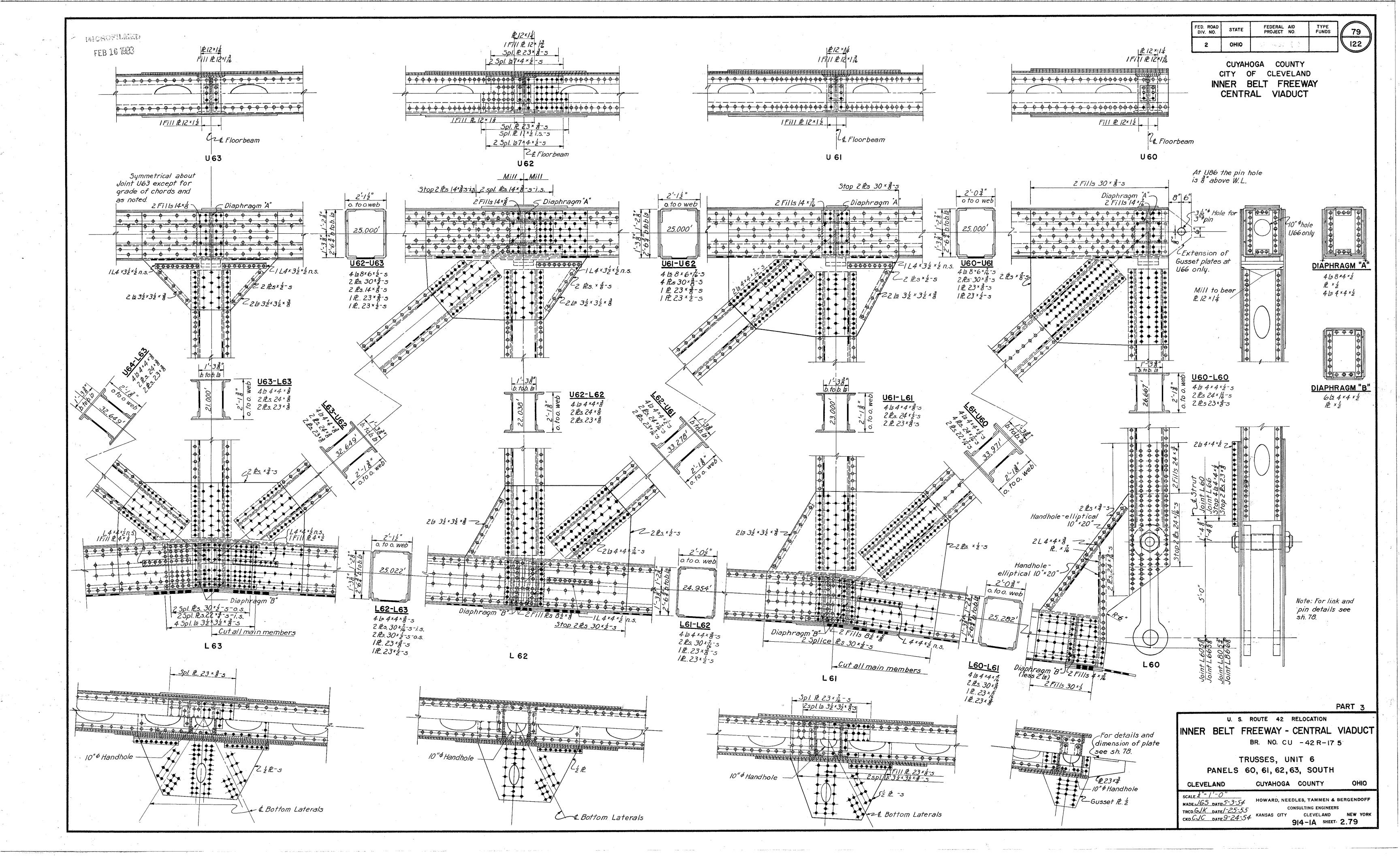
SCALE

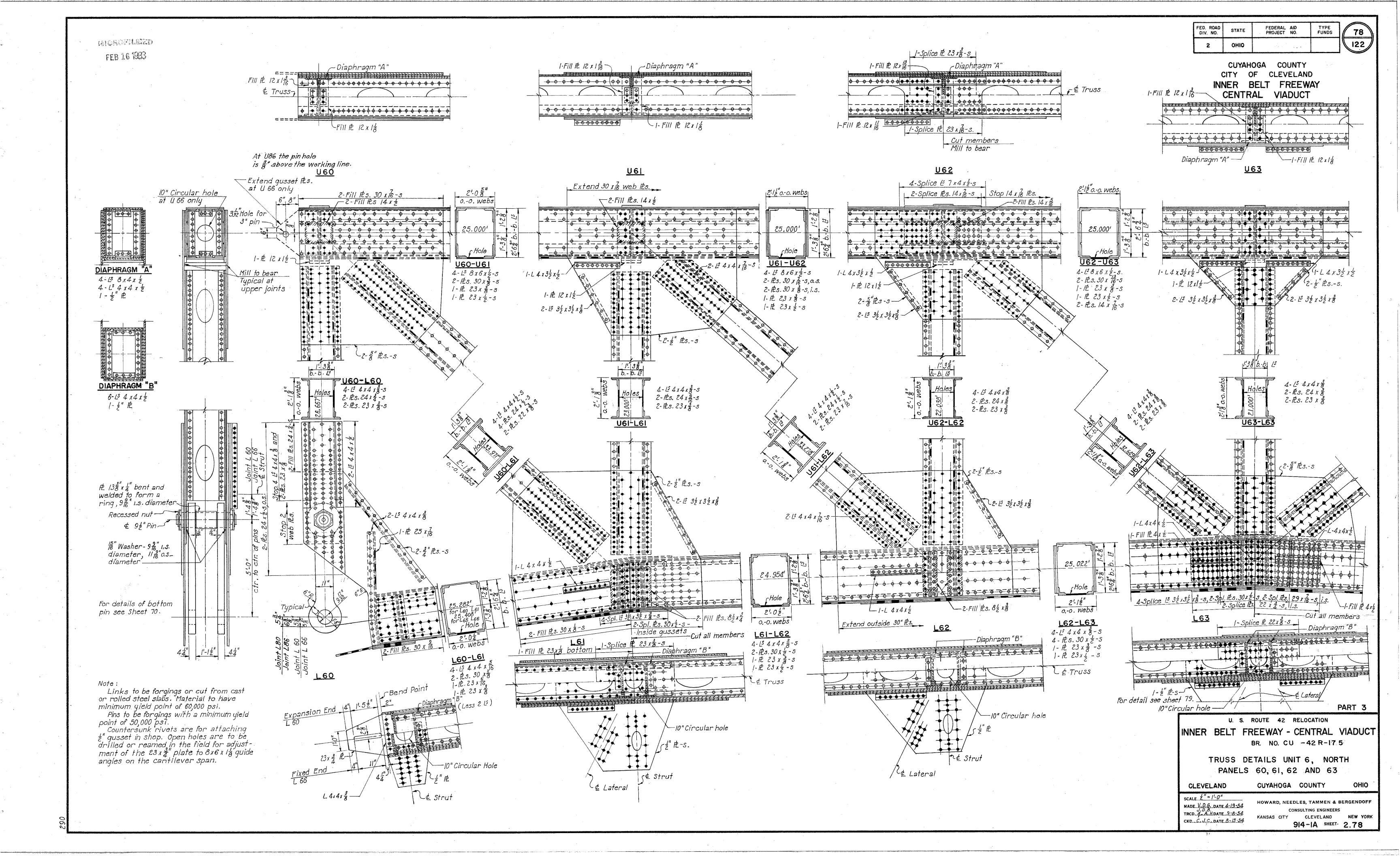
MADE T.W.L DATE 5-13-54

TRCD G.J.K DATE 8-2-54

HOWARD, NEEDLES, TAMMEN & BERGENDOFF KANSAS CITY CLEVELAND NEW YORK

CKD <u>E.L.</u> DATE 8-11-54 914-IA SHEET 2.80





MICROPULMED FEB 16 1993

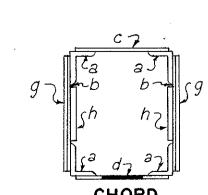
FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	77
2	оню	N. GALANIE		122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

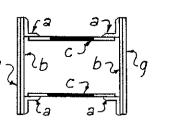
•	ENSION	CHORE	-sout	H TRUS	SS	C	COMPRE	SSION	CHORD -	SOUTH	TRUSS		NE.			Т	ENSION	CHORD	- NORT	H TRU	SS	C			CHORD-	- NORTH	I TRUSS	
L60 L61	L 61	L 62 L 63	L 63 L 64	L64 L65	L 65 L 66	U60 U61	U61 U62	U62 U63	U63 U64	U64 U65	U65 U66			MEMBER		L60 L61	L 61	2 63	L63 L64	L 64 L 65	L65 L66	U 60 U 61	U.61 U.62	U62 U63	U63 U64	U64 U65	U65 U66	, · .
0'		+1,242					<del></del>			-1,241			/	Dead Load		. 0		+1,290		+ 77/	0		-1,289	-1,524		-1,289	-770	
0	+ 594	+ 995	+ 955	+594						- 993			2	0.8 Dead Load		0	.1	+1,032	-		0			-1,219				
0		+ 375		+ 232	0								3	Live Load+ImpTe.	nsion	0		+ 390										
0	+ 232	+ 375	+375	+ 232	0								4	Reduced LL+ Imp Te		0		+ 390										
						-232	-375	-416	-416	-375	-232		5	Live Load + Imp C								- 241	-390	-433	-433	-390	-241	
						-232	-375	-416	-416	-375	-232		6	Reduced LL+Imp C	omp.							- 241	-390	-433	-433			
0	+385	+620	+620	+385	0								7	Reduced LL+ImpTen.	xD(CF)e	0	+400	+645	+ 645	+400	0							
						- 385	-620	-690	-690	-620	- 385		8	Reduced LL + ImpCom	p.XD(CF)e							-400	-645	-717	- 7/7	-645	- 400	
													9	Ratio = Line 4'	Line 6													
0	+ 9	+ 15	+ 15	+ 9	0					,			10	LL Sidewalk - Tensio	17	0	+ 10	+ 16	+ 16	+10	0			,				!
						- 9	-15	-18	-18	-15	-9		11	LL Sidewalk - Comp.								-10	-/6	-19	-19	-16	-10	
0	+988	+1,630	+1,630	+988	0	-988	-1,628	-1,883	-1,883	-1,628	- 988		12	Direct Design Stress		0	+1,027	+1,693	+1,693	+1,027	0	-1,026	-1.692	-1,955	-1,955	-1,692	-1,026	
										1			13	Reverse Design Stres				1										
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			,											Section	2							*						
4x4x5/16	4x4x3/8	4x4x3/8	4 x4 x 3/8	$4x4x^{3/8}$	4x4x5/16	8 x 6 x 7/16	8x6x7/16	8 8x6 x 1/2	8x6x1/2	8x6x7/16	8x6x 116			a Flange Angles	8 2	4x4x5/16	4x4 x 3/8	4 x 4 x 3/8	4x4x3/8	4x4x3/8	4x4x5/16	8x6x1/2	8x6x1/2	8x6x1/2	8x6x1/2	8x6x1/2	8x6x1/2	
						30 x 3/8								b Ist Web Plate				30 x 1/2										
23x 5/16	23 x 3/8	23x3/8	23 x 3/8	23 x 3/A	23x 5/16	23 x 3/B	23 x 3/8	23 x 3/R	23x3/8	23 x 3/8	23 x 3/8			c Top Cover Plate	ं है उ	23 ×5/16	23 x 3/p	23x 3/8	23 x 3/9	23 × 3/0	23 15/16	23 x 3/0	23 x 3/8	23 × 3/0	23 × 3/e	23 x 3/p	23,3/0	
23 x 3/8 +	23 x 1/2 *	23x1/2 *	23x1/2 *	23x1/2 ×	23 x 3/8 ×	23x1/2 *	23x 1/2 3	* 23x1/2 *	23x1/2 +	23 x 1/2 *	23x1/2 *			d Bottom Cover Plate	1 2	23 × 3/0 ×	23 1/2 3	23x1/2 *	231/124	23 1/2 4	23×36 ×	23 × 12 *	23 1/2 4	231/3 *	23/1/2 4	23 v 1/24	23 × 1/2 ×	
		30x1/2					30x3/8	202	20472	30 x 3/8	20.72			g 2nd Web Plate	70 4	20 x 70 x	LUX 12 X	30 x 1/2		LUXICX	LUA 10 H		30 x 7/16	2017E N	ZJATZ K	30x7/16	23,32 "	
		30 4 12	00112	· · · · · · · · · · · · · · · · · · ·			002 78	14 x 3/B	14x 3/8	30 x 18				h Inner Web Plate	8 7			JO X 72	30 % 72	:		1	30x 776	14 x 7/16	11 × 7/10	30% 776	<del>                                     </del>	
							<u> </u>	1, 7,0	1				•	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-   3 -									17 1/16	14x 716			
				· · · · · · · · · · · · · · · · · · ·																					<del>,</del>			
						300"	300"	300	300"	300"	300"		25	Length	/_						-	300"	300"	300"	300"	300"	300"	
								11.00		11.13			20	Min. Radius of Gyra	/n.					`		10.59						
18.000	24.000	24,000	24.000	24,000	18 000	16					19,630		27	Allowable Stress	Lbs/Sq./n.	18 000	21 000	24.000	21000	24.000	18 000			10.84				
43.79		82.32	_	52.32		+							20						· · · · · · · · · · · · · · · · · · ·	<del></del>							19,630	
36.60	<del></del>			43.69				96.75			60.85			Actual Gross Area	Sq. /n.			86.07		56.07				102.63	· · · · · · · · · · · · · · · · · · ·		64.13	· · · · · · · · · · · · · · · · · · ·
7		<del></del>								82.97			29	Net Area	5q./n.		46.94			46.94				102.25		90.00		
	22,010	20,500	23,300	22,610		10,200	73,020	13,400	13,400	19,020	18,200		30	Actual Unit Stress	L.US./3Q./n.	0	61,000	23,200	23,200	21,000	0	17,840	10,800	19,120	19,120	10,800	17,840	
<u> </u>	J J			<del> </del>			<u>J</u>	1 0	<u> </u>	1 3	3		31	Material		C	<u> </u>	٥	5	<i>J</i>		٥	) 3	3	3	3	<del>- 3</del> +	
	L	<u> </u>		<u> </u>		1)										<u> </u>	1		1		1	<u> </u>		<u> </u>				

TENSIC	N WEB		ERS - S	OUTH .		COMP	PRESSIO	N WEB	MEMB	ERS-S			NE			TENSI	ON WE	3 MEM	BERS - N			11		N WEB	MEMBE	RS - NO		
U60 L61	U61 L62	,U 62 L 63	L 63 U64	L 64 U65	L 65 U 66	U60 L60	U61	U62 L62	U63 L63	U64 L64	U65 L65	U66 L66		MEMBER		U60 L61	U61 L62	U62 L63	L 63 U64	L64 U65	L 65 U66	U60 L60	U61 L61	U62 L62	U63 L 63	U64 L64	U 65 L 65	U66 L66
+1,009	+665	l .	+298	1	1	-763	-556	- 303	-120	- 303	-556		1	Dead Load		+1,044	+ 693	+307	+ 307		+1,044	-789	-586	-326	-/37	-326	-586	-856
+ 807	+ 532	+ 238	+ 238	+ 532	+807	-611	-445	-242	- 96	- 242			2	0.8 Dead Load		+ 835	+ 554		+ 246		+ 835	-631	-469		-110	-261	-469	-685
+ 315	+ 231	+ 149	+ 149	+ 231	+315			+15		+15			3	Live Load + Imp Tens	sion	+ 328	+ 240		+ 155		+328			+13	1.4"	+13		
+ 3/5		+ 149			+ 315			+ /5		+15			4	Reduced LL +ImpTen		+ 328	+240	+ 155			+328			+13	:	+/3		
	-20	- 55		-20		-223	-/68	-105	-48	-/05	168	-229	5	Live Load + Imp Co.	mp.		-21	-57	-57	-21		-232	-175	-109	-50	-109	-/ <i>75</i>	-239
	-20	-55	<sup>-</sup> 55	-20		-223	-/68		-48	-/05	-/68	-226	6	Reduced LL+ImpCoi			-21	-57	<b>ー</b> 57	-21		-232	-175	-109	-50	-109	-/75	235
+522		+247	+247	+383	+522			+ 25		+25			7	Reduced LL + ImpTen. x L		+ 542	+398	+257	+257	+398	+ 542	**		+22		+22		
	-33	-91	-91	-33		-370	-278	-/74	-80	-/74	-278	-374	8	Reduced LL+ImpComp x			-35	-94	-94	-35		-384	-290	-181	-83	-181	-290	-389
	-0.030	-0.185	-0.185	-0.030				-0.020		-0.020			9	Ratio= Line (Comp) or Line	Line 6 e / (Ten)		-0.030	-0.186	-0.186	-0.030				-0.018		-0.018	7	
+ 12	+9	+5	+5	+9	+12								10	LL Sidewalk - Tensio		+ 13	+9	+6	+6	+9	+ 13							
		-2	- 2			-10	-7	-4	-/	-4	-7	-10	11	LL Sidewalk - Comp.			-0.4	-2	-2	-0.4		-9	-7	-4	-/	-4	-7	-9
+1,341	+ 924	+ 490	+490	+924	+1,341	-991	-730	-420	-177	-420	-730	-1,046	12	Direct Design Stress	;	+1,390	+961	+ 509	+509	+961	+1,390	-1,024	-766	-446	-194	-446	-766	-1,083
													/3	Reverse Design Stres	S													
·											,																	
																<u> </u>	<u> </u>											
1 1 1/-	1 . 0 . 11	4 4 31	1 1 2/			4 4 /	3/		3.					Section	9,0				ļ							_		
4 X4 X 72	4X4 X12	4X4X 1/8	4x4x48	4 x 4 x 1/2	4x4x1/2	4x4x1/2	4x4x78	4x4x3/8	4x4x-1/8	4x4x3/8	4x4x 3/8	4 x 4 x 1/2		a Flange Angles	<u> </u>	4x4x1/2	4x4x1/2	4x4x3/8	4x4x3/8	4x4x1/2	4x4x12	4x4x <sup>3</sup> /8	4x4x 1/8	4x4x3/8	4x4x 3/8	4x4x3/8	4x4x <sup>3</sup> /8	4x4x 3/8
24 X 116	24X 116	24x3/8	24 X 3/8	24x 1/16	24x7/16	24 x 1/16	24x 1/2	24 x 3/8	24x 3/8	24x 3/8	24 x 1/2	24x 1/16		b Ist Web Plate	₹ 3	24 x 1/2	24 x /2	24 x 1/8	24 x 3/8	24x 1/2	24 x 1/2	24 x 3/4	24 x 4/16	24 x 3/8	24 x 3/8	24 x 3/8	24x 9/16	24 x 3/4
20 × 7/1-	23×116* *	C3X78**	23×78**	23×716**	23×1/6 **	23×78* *	LJ X 7/8**	LJX78 * *	C31/8**	23x38**	23 x 3/8**	23x 1/8***		c Cover Plates	0 2	22×3/8 * *	23×1/16 * *	23x % * *	23x3/8 **			23 x 3/8 * *	23x3/8 **	23×3/8 * *	23x3/8 **	23x3/8 **	23x 3/8 **	23x % * *
24 × 7/16					24 × 7/16									g 2nd Web Plate	\$ 3	24 x 1/2					24 x 1/2							
															2	<u> </u>												
<del>-</del>							· · · · · · · · · · · · · · · · · · ·								-   6	ļ												
	·—···									`					11/2	<u> </u>	ļ											
						320	276	261	252	261	276	220	25	Length	/_							320	276	26.1	252	261	274	220
-				<u> </u>		760	760	7 70	770	770	760	7.60	25	Length Min. Radius of Gyratio	/n.		<u> </u>	•					276 7.56	264 7.70	252 7.70	264 7.70	276 7.56	320
24 000	24 000	18 000	18 000	24,000	24,000	19 180	19 300	14 700	1.70	14 700	19 390	19 180	27	Allowable Street		<del></del>	21 000	10 000	10 000	21 000	21 000				1.10			
									20 10	39 10	45 10	57 75	20	Allowable Stress Actual Gross Area								19,150			20.10	14,700		
56.50	39.01	32.44	32 44	39 /1/	56.50	56.20	39 52	3/ 88	31 88					Net Area			50.38		39.19	50.38				39.19	39.19		48.19	<i>57.19</i>
23.740	23.690	15.100	15 100	23 690	23,740	17.620	18 960	13 170	5,550	13 170	18 960	18 620	30		Lbs./Sq.In.							57.19			31.88		42.79	57.19
5	5	C	6	5	5	5	5	G G	<i>C</i>	C	5			Material	LUS./3Q.111.	5	5	0,070	10,070		c	5		13,330	0,090	13,990		0,340
		<u> </u>			† <del>-</del>			-			J		51	moter tal		3	<u> </u>			5			5	<u> </u>	U	U	5	3
l				l		<u> </u>	<u></u>	L	L		<u> </u>	<u> </u>	<u> </u>	<u> </u>		11			1		<u> </u>	l						

S = Special Steel G = Carbon Steel \* = //"Hole

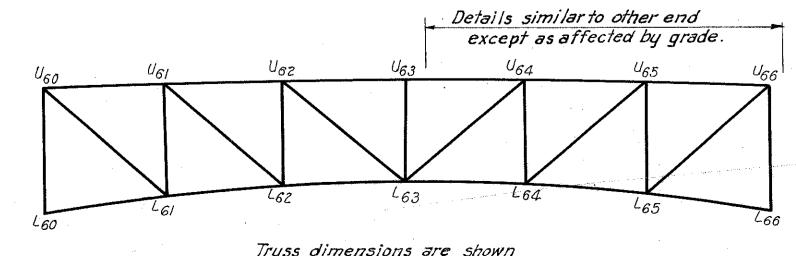


All dead load and live load stresses are in kips.
Line 29,- Net area for tension or effective gross area for Compression.



WEB MEMBER

\*\*=10" Hole



Truss dimensions are shown on Framing Plan, Sh. 23.

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R-17.5

STRESS SHEET UNIT 6

NORTH AND SOUTH TRUSSES

CLEVELAND

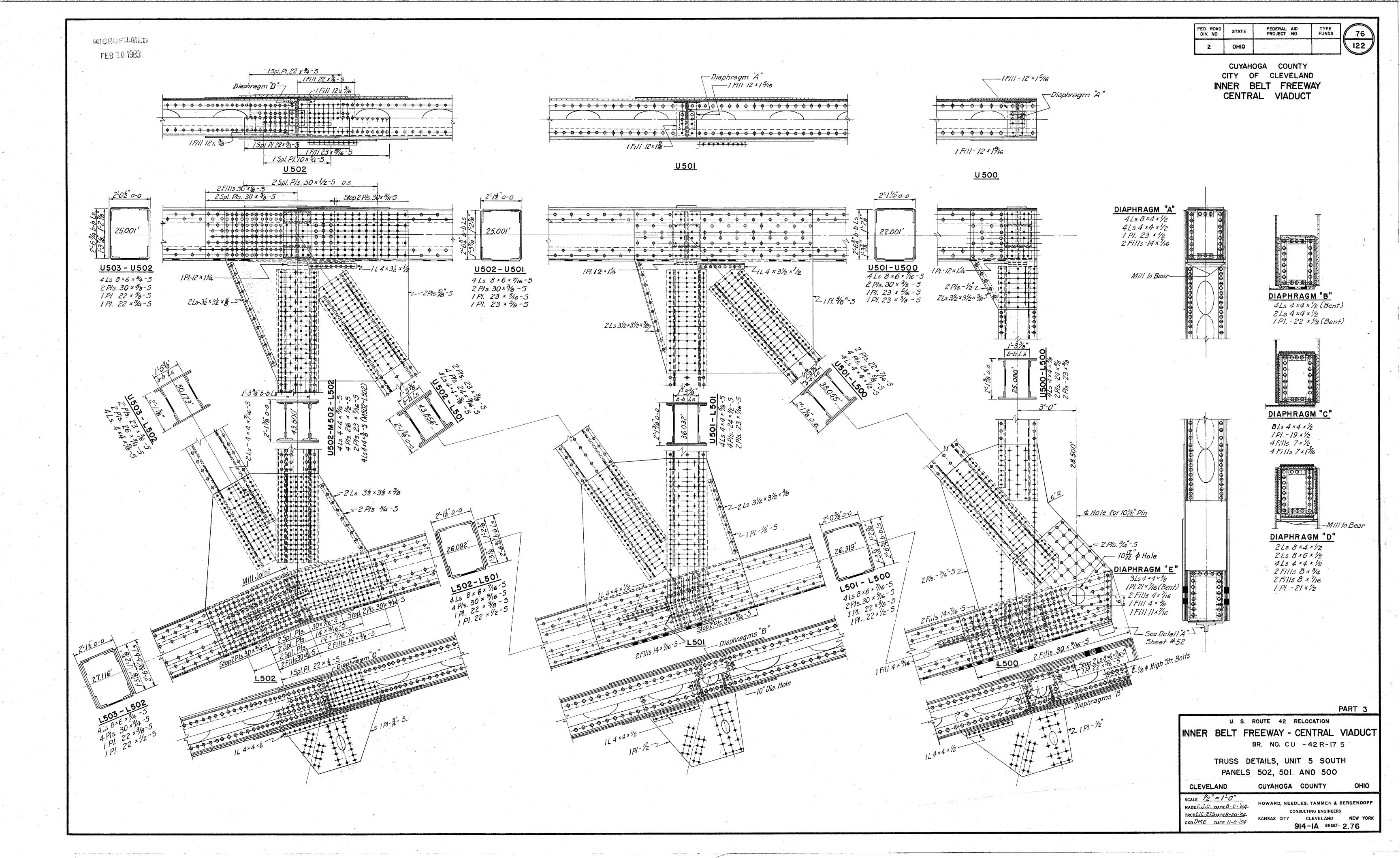
CUYAHOGA COUNTY

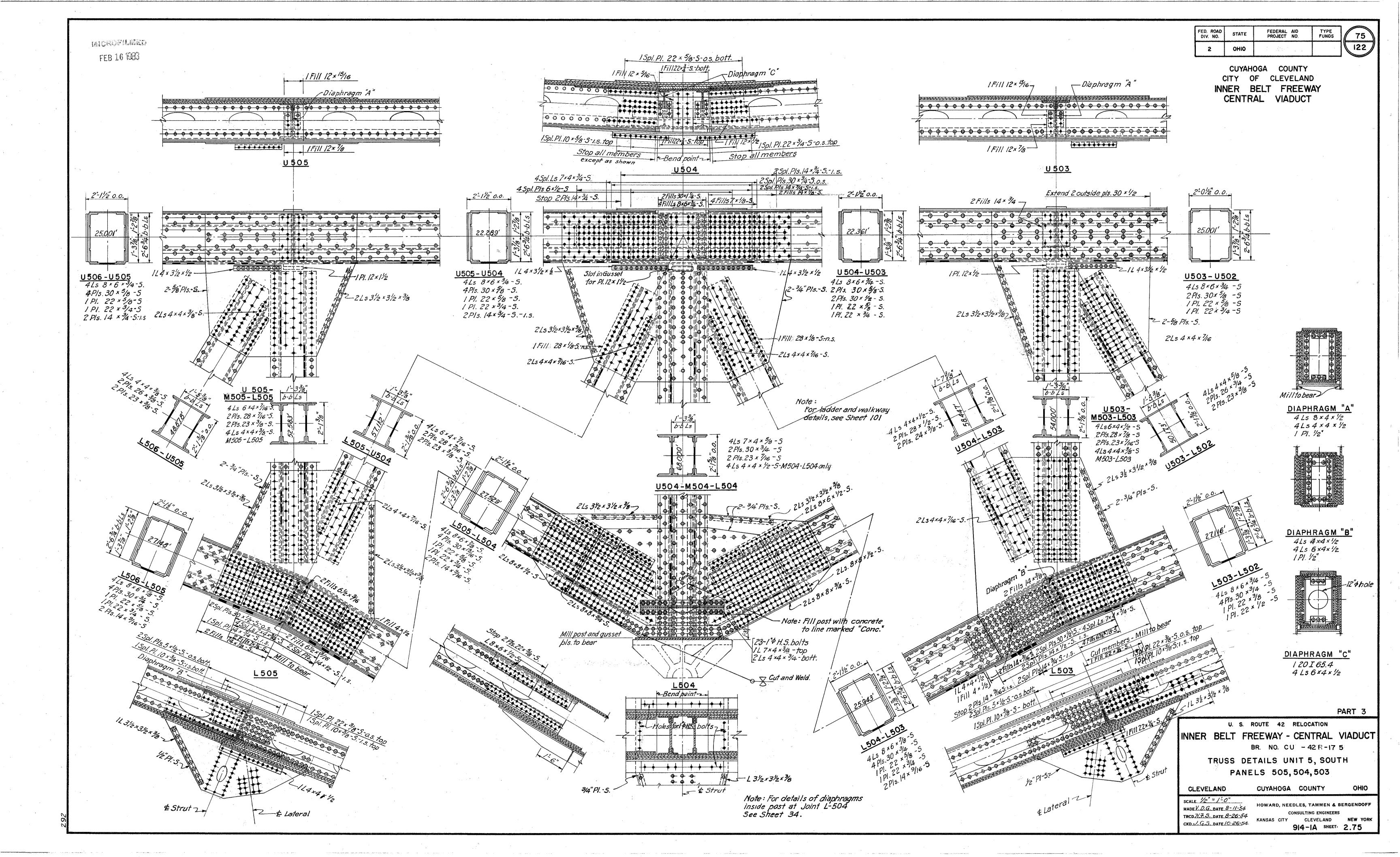
SCALE None MADE <u>D.M.E</u> DATE <u>5-6-54</u> A.M. TRCD <u>7.7.5.</u> DATE <u>9-9-54</u> CKD <u>M.M.L.</u> DATE <u>5-19-54</u>

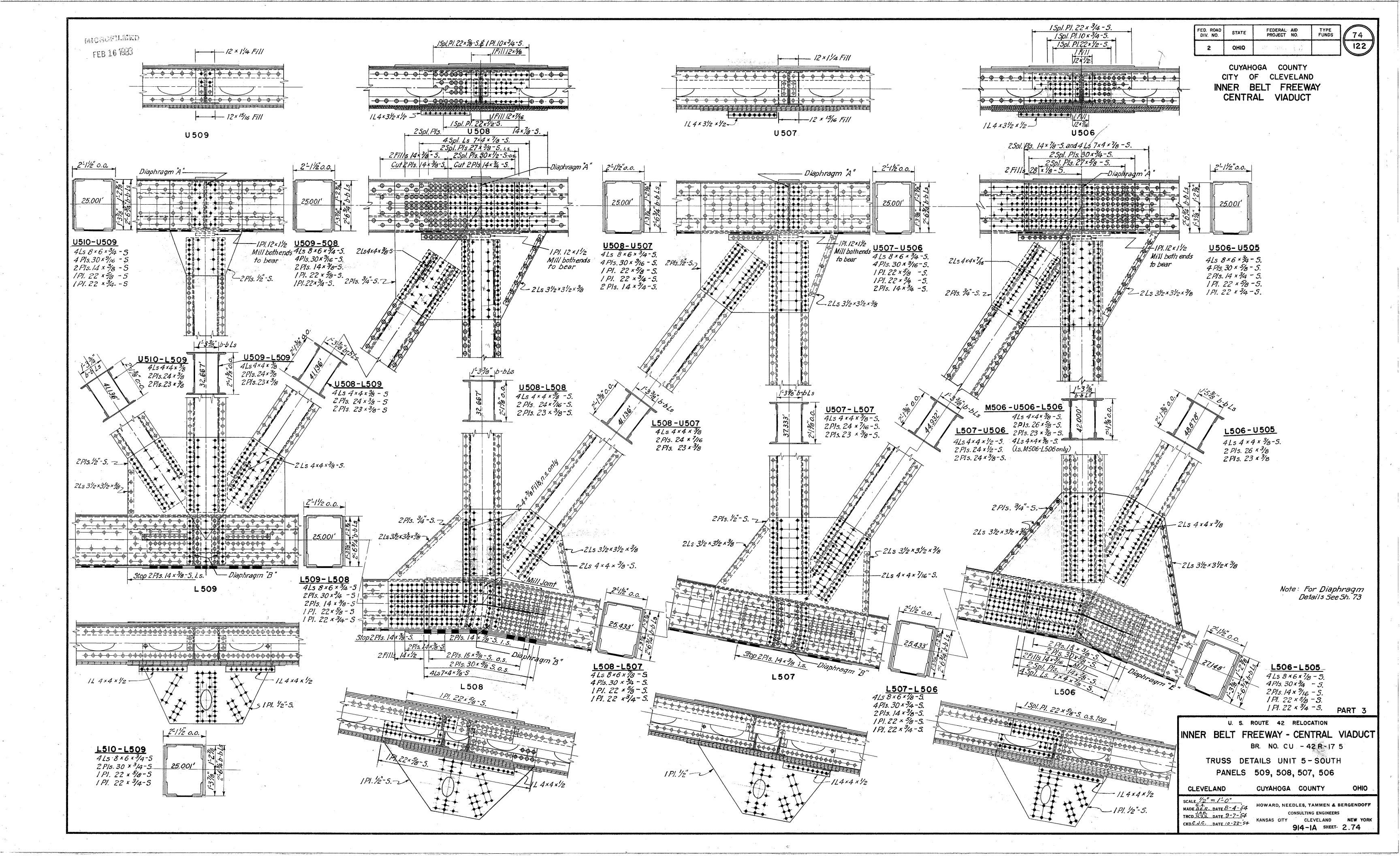
HOWARD, NEEDLES, TAMMEN & BERGENDOFF KANSAS CITY CLEVELAND NEW YORK 914-14 SHEET- 2.77

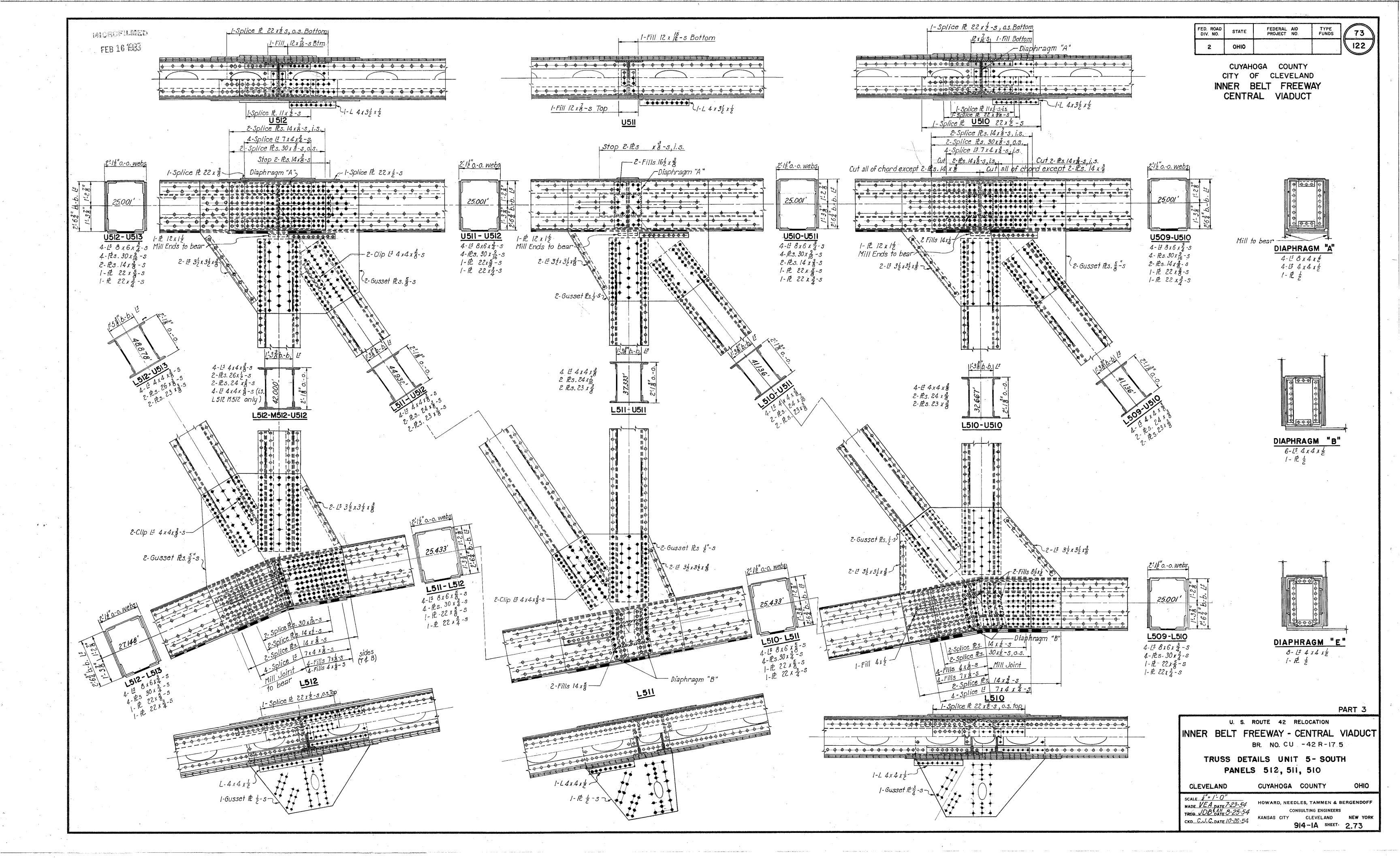
PART 3

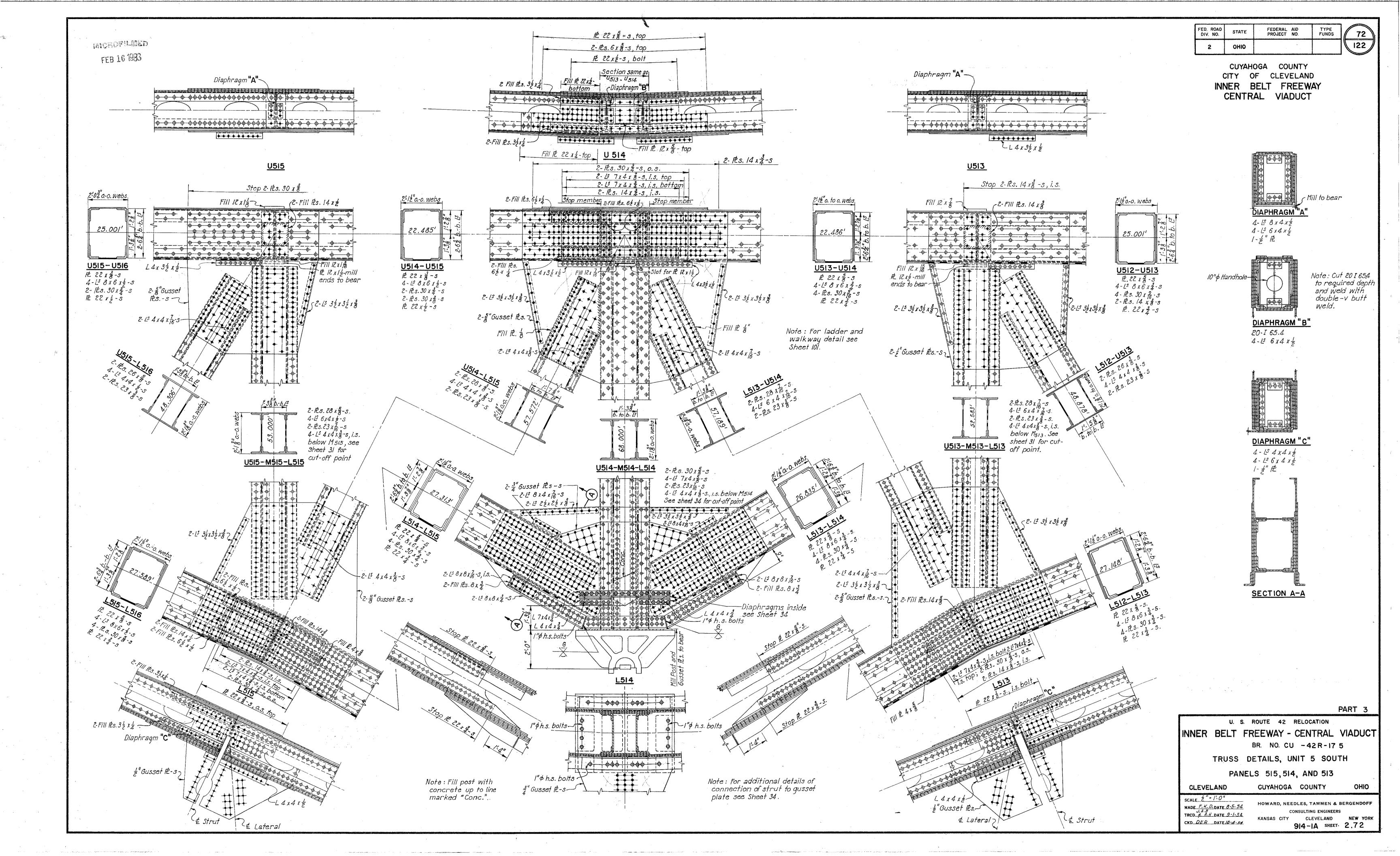
OHIO

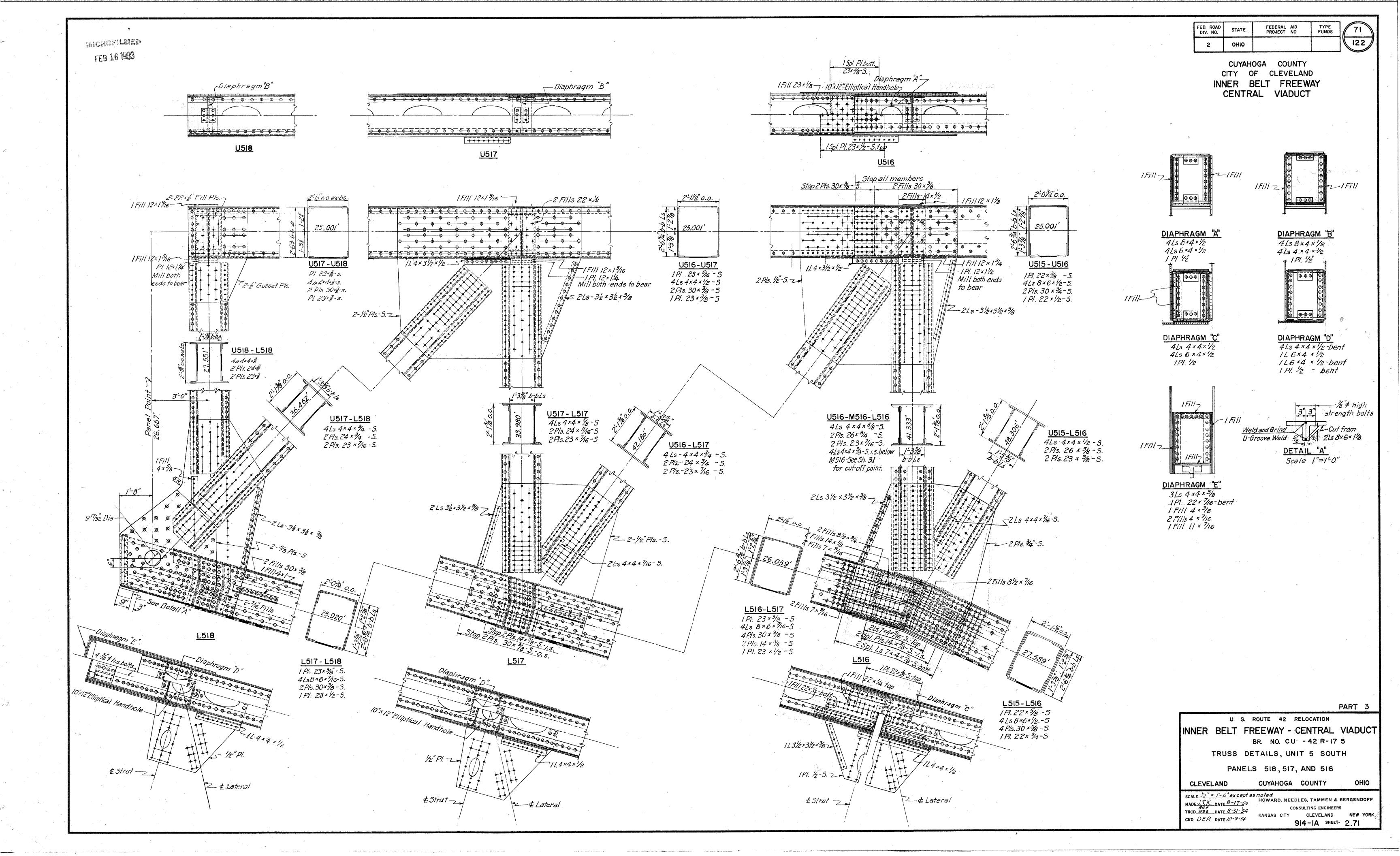


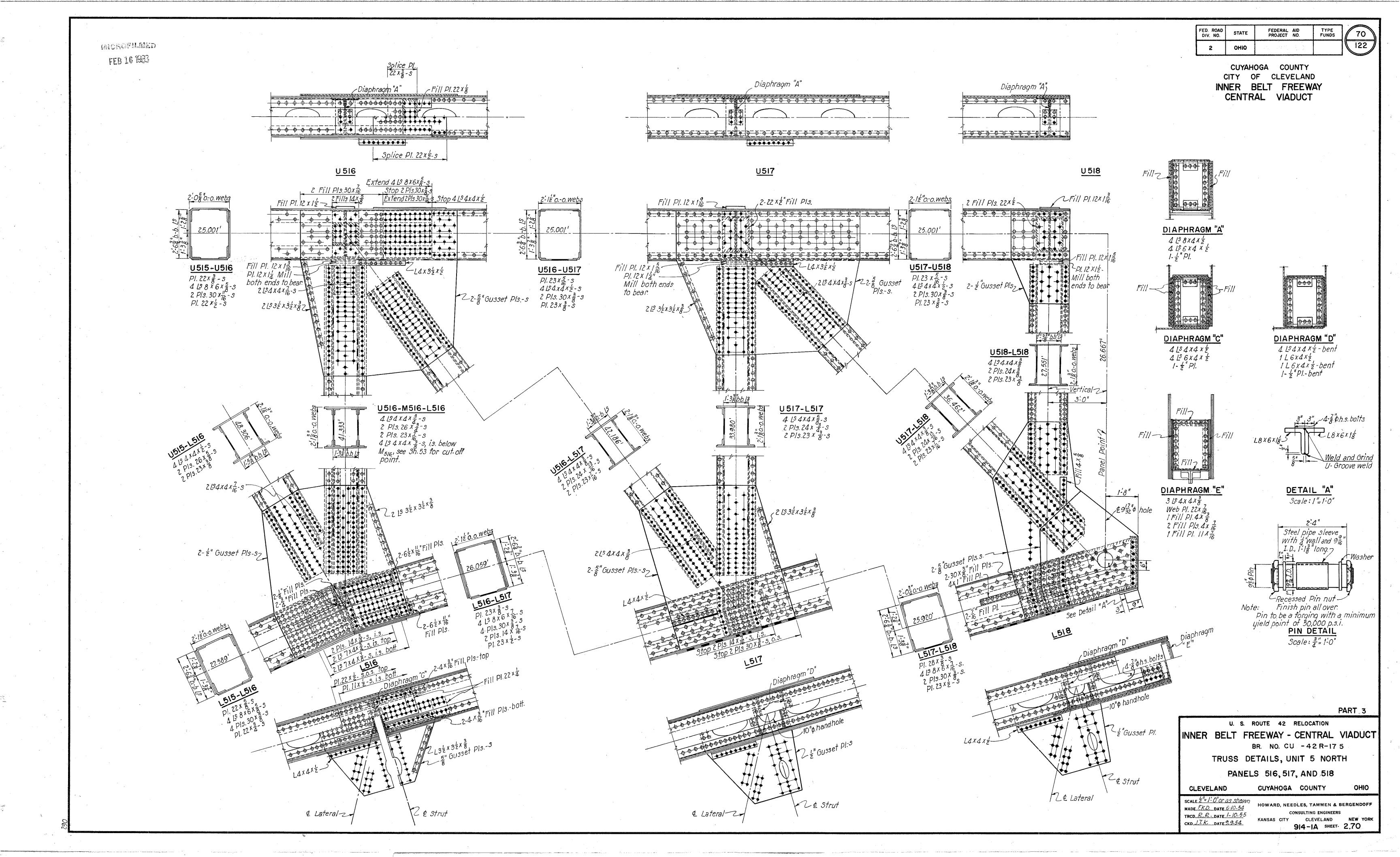


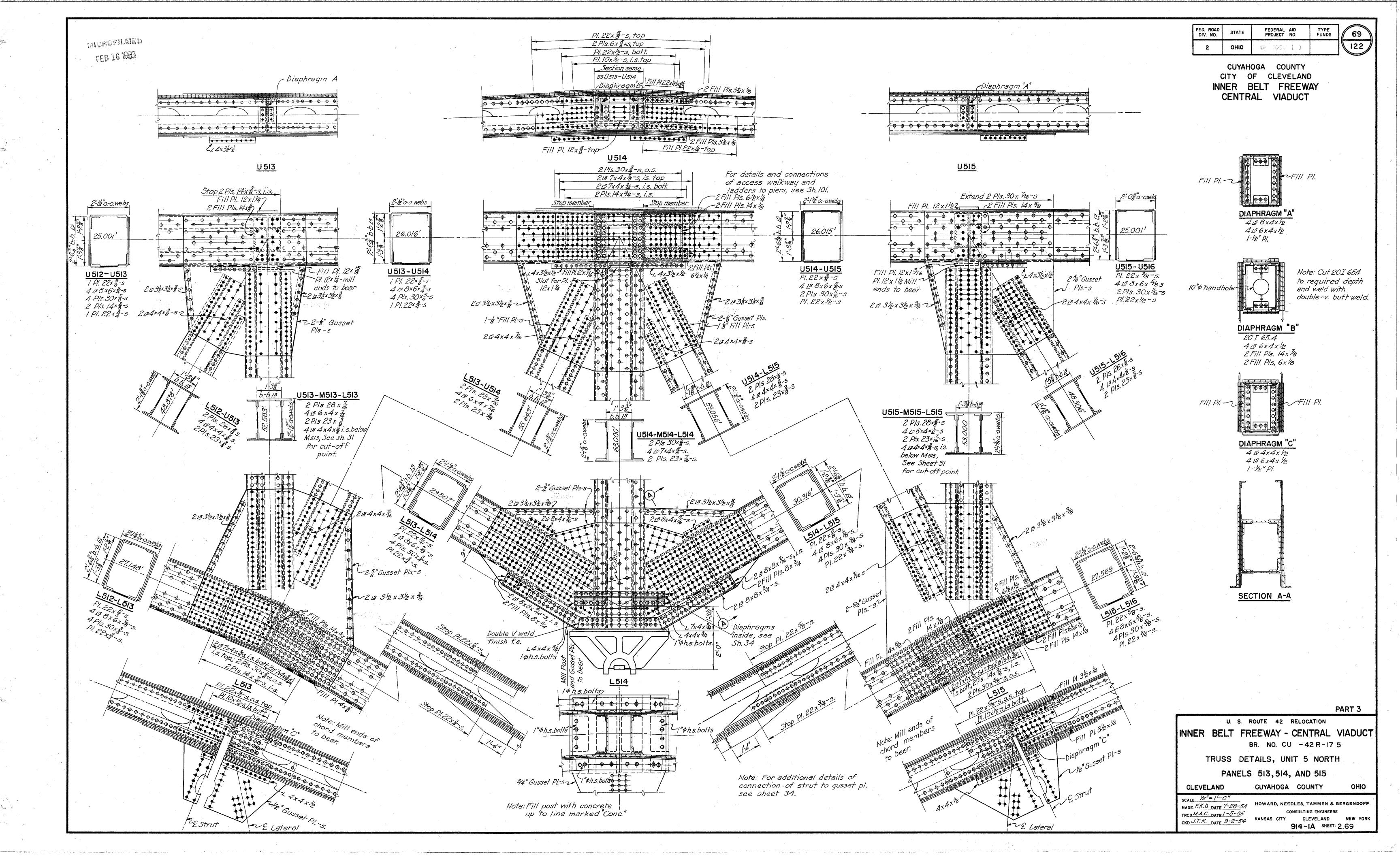


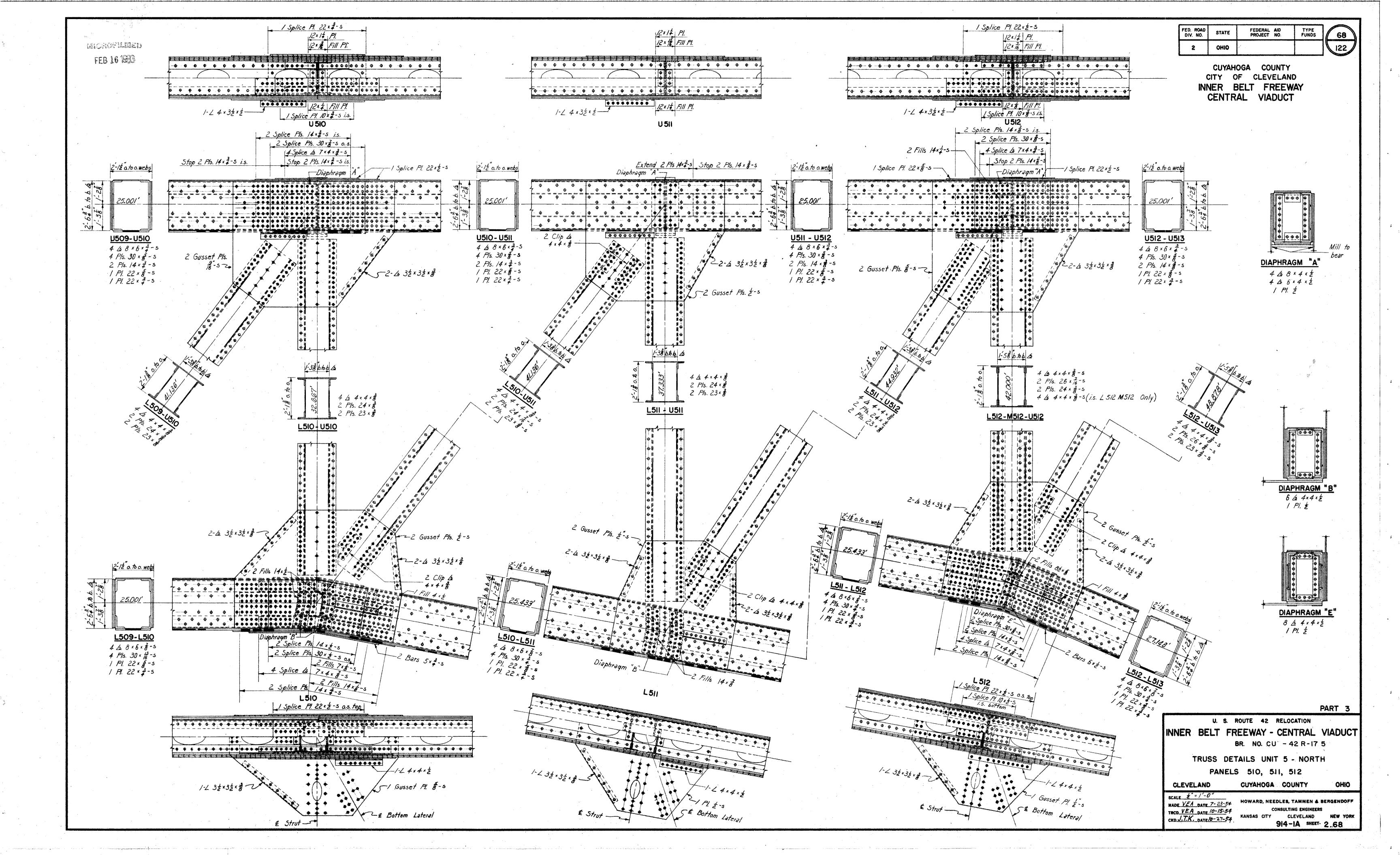


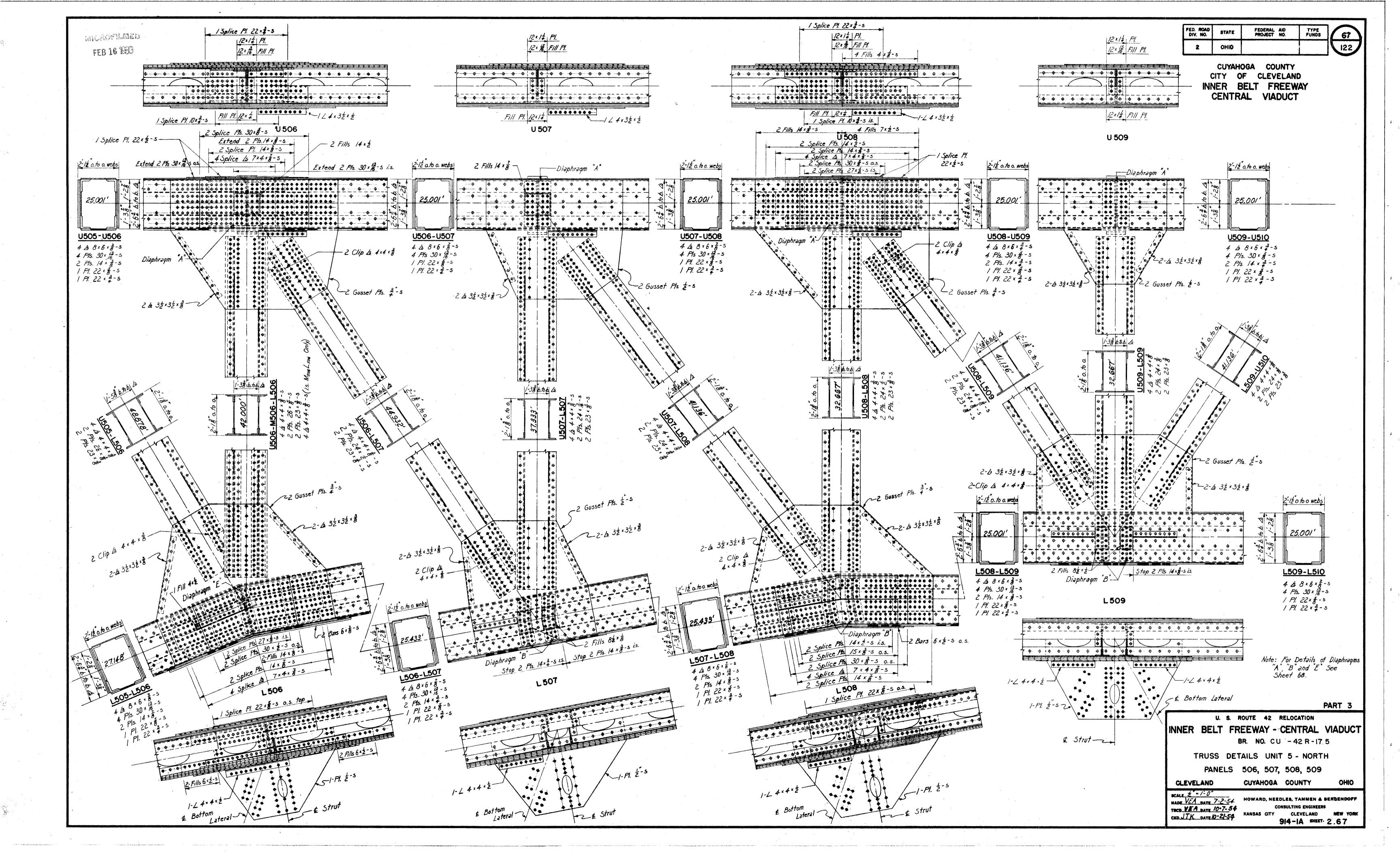


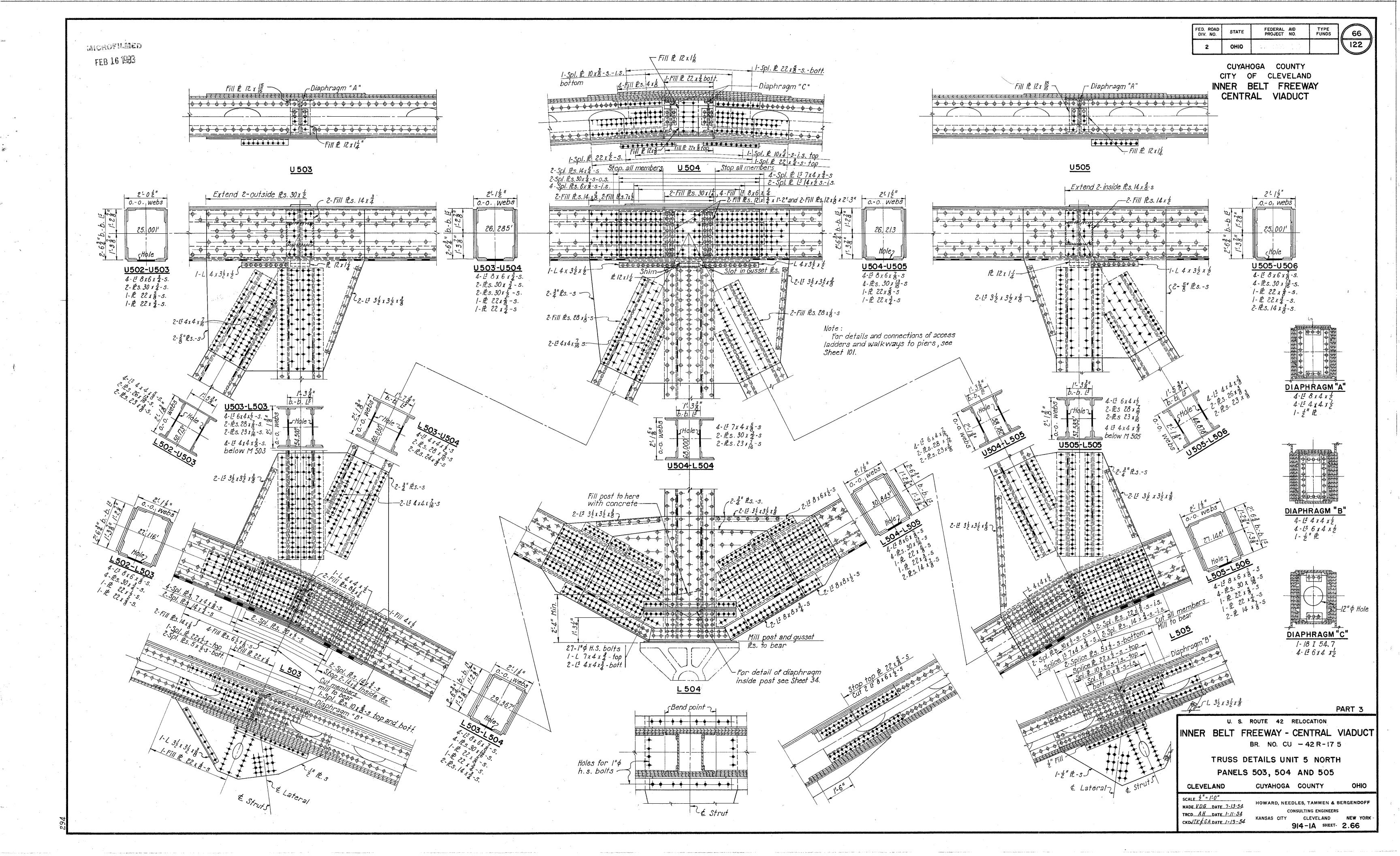


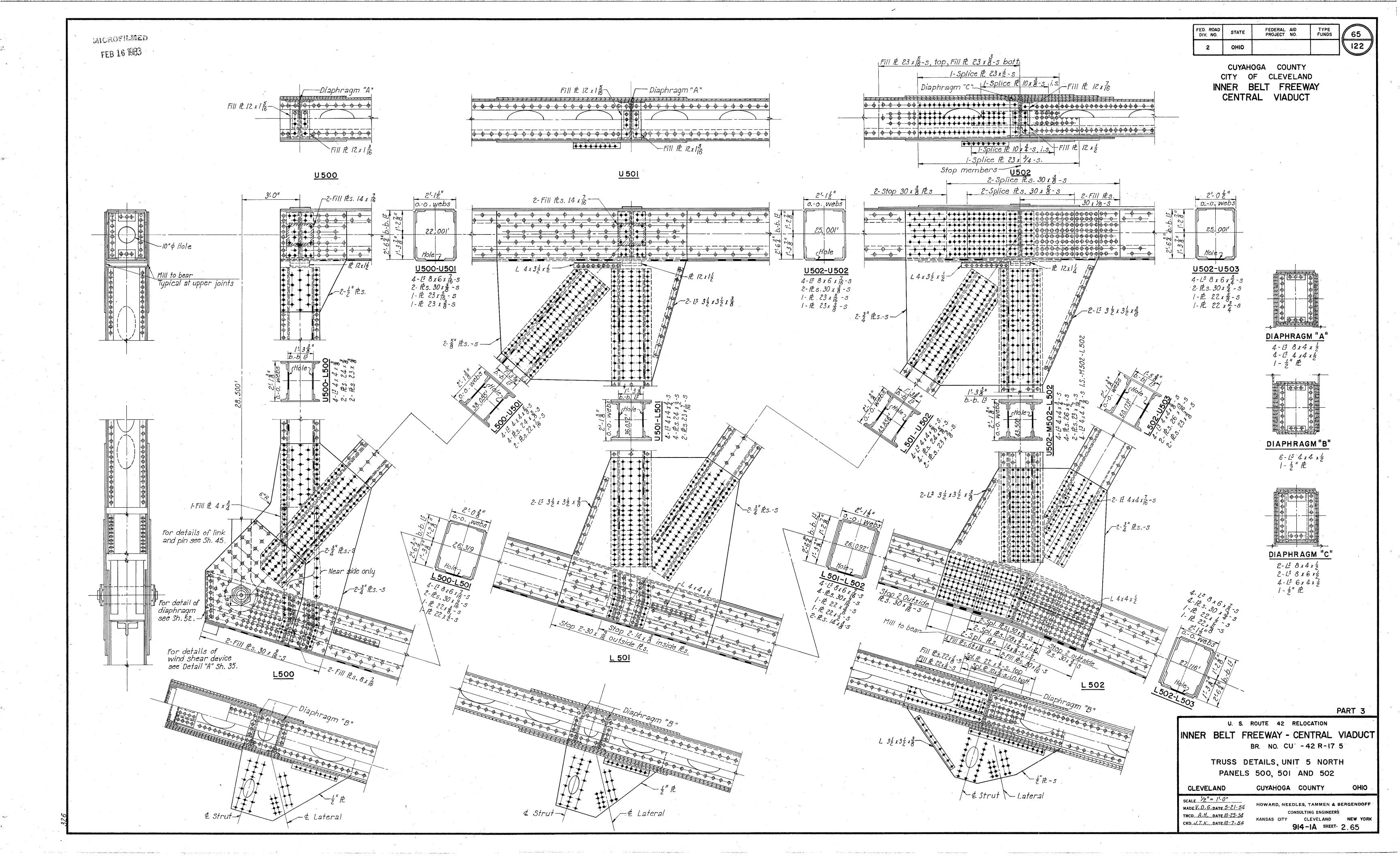












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FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	64
2	оню			122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT

																																		CENT	KAL VI	<u>AUUU I</u>	
					•	,			CON	MPRESSIO	N CHO	RD			· · ·									•			1	rension	CHOR	D							_
	MEMBER	L500	L501 1 502	L502 / 503	L 503	L 504	1 505 1 506	L 506	L 507	L 508	L 509	L 510	L 511   512	L512 1513	L5/3 / 5/4	L514	1.515	L516	L 517	U500 U50	U 501 U 502	U502 U503	U503 U504	U504 U505	U505 U506	U 506 U 507	U507 U508	U 508 U 509	U509 U 510	<u>И 510</u> И 5   I	U511 U 512	<u>U512</u> 2 U516	U513 3 U514	U514 U515	U515 U516	บ5/6 บ5/7	U5.
Dead Lead		<i>≥ 974</i>	- 1789	± 2479	± 3028	= 31/7	± 2900	- 2667	- 2392	- 2247	- 2055	- 2048	÷ 2205	- 2369	- 2549	- 2527	- 2065	- 1476	- 785	1 000		+ 1714	+ 2286	+ 2670	+ 2621	+ 2352	+ 2247	+ 2037	+ 2037	+ 2055	+ 2014	+ 2167	+ 2181	+ 1871	+ 1416		
O.8 Dead Load				- 1983			- 2320		~1/914	- 1798	- 2033 - 1644	- 1638	- 1764	- 1895	- 2039	- 2022		- 1181				+ 1371	1	+ 2136	+ 2097		+ 1798			+ 1644	+		<del></del>	+ 1497	+ 1133		
Live Load + ImpTension	7	1											•							#	T 140	T 13/1	1 1923	Y 2130	7 2037	T 1996	1 1,30	7 3.002									
Reduced L L + ImpTensie							+ 146	+ 318	+ 473	+ 603	+ 603	± A73	+ 318	+ 146						1	+ 210	+ 367	+ 467	+ 590	+ 655	+ 677	+ 740	+ 728	+ 728	+ 728	+ 648	+ 608	+ 549	+ 440	+ 35/	+ 200	
Live Load + ImpComp.			······································				1 .40	, ,,,	1 7.5	7 333		710							'																		
Reduced L L + Imp. Comp.		<i>~ 221</i>	- 383	- 507	÷ 594	+ 610	- 644	+ 667	- 690	- 739	- 728	- 658	- 619	- 598	- 567	- 563	- 484	- 366	- 200					- 133	- 311	- 464	- 603	- 620	- 620	- 603	+ 464	- 311	- 133				
Reduced L L + ImpTen					337		+ 242	+ 526	+ 785			+ 785	+ 526	+ 242							+ 348	+ 608	+ 774	+ 978	+ /085	+ 1122	+ 1226	+ 1206	+ 1206	+ 1206	+ 1074	+ 1008	+ 910	+ 729	+ 582	+ 332	
Reduced L L + ImpComp.		- 366	÷ 635	- 840	- 984	- 1011	- 1067	- 1105	- 1143	- 1224		- 1091	- 1025	- 991	- 940	- 933	- 802	- 606	- 346					- 220	- 517	- 769	- 1000	- 1028	- 1028	- 1000	- 769	+ 517	<i>→ 220</i>				
Ratio= Line 4 or Line I (Comp.) or																								- 0.05	- 0.12	- 0.20	- 0,27	+ 0.30	- 0.30	- 0.29	+ 0.23	- 0.14	- 0.06				
L L Sidewalk-Tension							+ 7	+ 15	+ 23	+ 30	+ 30	+ 23	+ 15	+ 7							+ 11	+ 19	+ 26	+ 34	+ 37	+ 50		+ 55	+ 55	+ 54	+ 46		+ 28	+ 22	+ 16	+ 9	
L L Sidewalk-Comp.		÷ 11	= 20	- 28	- 34	+ 35	- 37	- 38	= 51	I I	- 54		- 32	- 31	- 29	∡ 29	- 24	£ 17	- 9					<u>~</u> 6	+ 15	- 23	- 30	- 31	- 31	- 30	<i>→</i> 23	- 15	- 6				
Direct Design Stress		- 1156	- 2086	- 2851	- 3440	- 3540	- 3424	- 3277	- 3108	- 3078	- 2904	- 2776	- 2821	- 2917	- 3008	2984	- 2478	- 1804	- 983		+ 1105	+ 1998	+ 2629	+ 3/48	+ 3219	+ 3054	+ 3080	+ 2891	+ 2891	+ 2904	+ 2731	+ 2773	+ 2683	+ 2248	+ 1731	+ 943	
Reverse Design Stress																		-			.20					,											
																																					ļ
	······································																		J <sup>3</sup>																	······································	-
*	Holes Out																							<u> </u>													<b>-</b>
SECTION	for Tension		271 m - 1 1 1	- 1 · 1 · 2			<u>Sera i </u>	<u> </u>		1	mar a t	gwie g	<u> </u>	le i i	100 1 2 d	48.74.7	1232	Bala sali				<u> </u>			and the same										<u> </u>		<del> </del>
a Angles	2	8x6x 7/16	8x6x 7/16	1			8x6x 7		8x6x 8	1 1	8x6x ₹		8x6x \$		8x6x 3	8x6x ₹	1		1 ''		16 8x6x 7/16		8x6x ₹	8x6x 2	8x6x 1	8x6x 4	8x6x 3	T	8x6x ₹				8x6x <sup>3</sup> / <sub>4</sub>				+
b I . Web Plate	4	30x 9/16	30x 9/16	30x ₹		30x 13/16	6 30x <del>3</del> 22x <del>3</del>	30x <sup>3</sup> / <sub>4</sub> 22x <sup>5</sup> / <sub>8</sub>	30x ₹ 22x ₹	30x ¾ 22x ¾	30x ₹	30x <del>3</del> 22x <del>§</del>	30x 3	30x 3 22x 3	30x ⅓ 22x ∯	30x ₹	30x \$\frac{2}{8}	30x ⅓ 23x శ	30× ≩ 23x ≩	30x ₹	30x }	30x ₹	30x ₹ 22x ₹	30x ₹ 22x ₹	30x \$	30x 9/16 22x ‡	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16	30x 9/16 22x \$	30x 3	30x 3/4		
C Top Cover Plate	3	22x 3	22x 💈	22x 3	22x ½	22x \$	22x 2	22x 3	22x 3	22x \$	22x 🖁	22x ∯	22x §	22× #	22x 🐐	22x \$	22x 🖁	23x 🗿	23x 3	23× 5/10	6 23x 5/16	22x \$	22x 3	22x 3	22x \$	22x 3	22x 3	22x 8	22x <del>2</del>	22x 3	22x #	22x #	22x #	22x 3	22x 3	23x 5/16	23
d Bottom Cover Plate		22x ½*)	22x ½*/	22x ½**)	22x 2**	22x x**	) 22x ¾**.	) 22x 1**	) 22x 3**/	) 22× ¾**)	22x 2**)	22x 4**)	22x 3**)	22x 3**)	22x ±**)	22x 3**)	22x 4**		23x ½*)	23x 3*)	23x **)	22x = **)	22x 4**)	22x 2**)	22x2**/	22x 4**/	22x 2**)	22x 4**/	22x 2**)	22x 4**)	22x 2**)	22x 2**)	22x 2****	22x 3*)	22x 3*1	23X 🚰 )	23
e I. Inside Web Plate					14x 9/16	14x 9/16	14x 9/16	14x 🚡		14x 3/8		,						14x ⅔						14x 3	14x 3	14x 3	14x ₹	14X #	14x 3	14x }		14x 3					+
f Inside Web Plate	4		30.000	20.3	20 3	70 1011	0 20 3	2 3	20 3	1 3	26.7	26 3	200 3			20 3		70 3				1	30x ½	30. 5	30 €	30v 0/16	30x 9/16	30 0/16	30x 9/16	30x 9/16	30x 9/16	30 0/16	30x 9/16	30.3			-
g 2. Outside Web Plate h 2. Inside Web Plate	2		30x 9/16	30x ₹	30x 7	30x 13/16	6 30x ₹	30x <sup>3</sup> / <sub>4</sub>	30x ₹	30x 3	30x ₹	30x ₹	30x ₹	30x 3	30x 3	30x 3	30x 💈	30x #	•	1			JUA Z	JUA 8	JUA 8	JUN 3/10	304 3/10	JUN 3/10	JUN 3/10	JUN 3710	JUN 3/10	302 3710	1 300 3/10	Jun 8	<del>                                     </del>		+
Length	/ <i>p</i>	3/5,5"	313.2"	275 411	311.8"	260.74	225 0#	205 20	205 20	200"	20011	200 211	2/0E 0#	22F 0#	222 574	220 04	331 1"	310 7"	217 22	1																	
Min. Radius of Gyration	/n	10.61	10,91	10.86	10.8	10,72	325.8" 10.8	305.2" 10,78	305.2" 10.78	300" 10.85	300" 10 <b>.</b> 85	305.2" 10.90	305.2" 10.90	325.8" 10.85	L	329.0"	l l	312.7"	1	1																	1
Allowable Unit Stress	Lbs./Sq./n.	19,600	19,620	19,590	19,620	19,480	19,580	19,630	19,630	19,650	10.83 19,650	19,640	19,640		10.85 19,590	10.85 19,580	10.96	19,620	19,590	24,000	24,000	24,000	24 000	24,000	24,000	24.000	24,000	24.000	24,000	24,000	24,000	24.000	24,000	24:000	24,000	24,000	1
Gross Area		71,22	104.97	144.01	174.42	181,400		169.17	158.67	163.01	152,51	146.19	146.19	19,590 152.51	152.51	152.51	124.75	93.85	60,85	57.91	57.91	100,01	24,000 130.01	158.51	158.51	24,000 151.01	151.01	24,000 140.51	140.51	140.51		140.51	130.01		85.75		
Net Area	5q. /n.	67.85	104.97	144.01	174.42	181.92	174.42		158,67	163.01	152,51	146.19	146,19		152.51	į.	124.75	93.47	1	49,72		85.64	111.64				129.64	•		120.64	1		111.64		73,63		
Actual Unit Stress	Lbs./Sq.In.		1120	110	19,720 0.5%	/	19,620		19,600	18,860	19,030	19,000	19,300	1	19,720 0.75		19,860	19,300 0	18.100	1	22,220	23:300	23.600	23,120	23,600	23,560	23.770	23.980	23.980	24.100	24,450 0.	23.000	1	1 1/8%	23,520	,	
Material	200./04.111	.,,020	. J. G. G.	12,000 0.	0.	19,400	1.7,020	19,330	15,000	70,000	19,030	13,000	13,300	19,120	12,120 0.	13,300	13,000	13,300 0.	. 10,100	# -		22,300	7.000	20,720	20,000	1 2	6.5,770	5,500	E.J. 300	27,700		1	1 (	7			1

											~		CC	MPRE	SSION	WEB	MEMB	ERS															Ш		ļ				TF	ENSION	WEB N	MEMBE	.RS	21		
U504 L509	L510	L 5/2	L513	U500 U	501 U.5 L.501 N	02 M3	502 U	1503 M503	M 503 L 503	U504 M504	M 504 L 50	U 505 1 M 50	05 M 505	U506	M 506	5 U507	U 508	U509	U 510	0.511	U 512 1 M 51	M512	12 U 513 12 M.	513 / 5	U514 N3 M5	M514	5/4 U 5/5 5/4 M 5/	M 515	115 U 516 115 M 516	M 516	U517 5 1 517	U518 7 1 518		MEMBER	1/2	500 L 501 U 501 U 50	L 502 102 U.5	0.3 (1.50)	04 L5	U 506 i06   507	U 507 U L 508	U508 L 509	1.5/1 U.5 U.5/2	14 U.5 L.5/5	515 U516 L516 L51	U517 1 L518
- 256 + 29	÷ 70	+ 28	- 203						<i>- 128</i> 5				8 - 362	- 54	- 690	~ 27	- 406	- 126	- 154	8 - 8	- 372	51	13 + 16	66 + 30	0 - 5	14 - 9	006 - 90	24 - 1038	8 - 1038	- 1180	- 924	- 82	1 De	ead Load		+ 1420 + 140	05 + 112	18 + 739	9 + 5	95 + 485			++ 276 +	590 +	880 + 1118	3 + 1107
- 205 + 23			<del></del>		- 950 -					1			2 + 290		9 - 552			1			) - 298		10 - 1						0 - 830					8 Dead Load		+ 1/136 + 1/2					1 1	1	·	1	· i	
						1011	7,720	<u> </u>	- 1020	400				7	- J-42			1	1.5%					27	<u> </u>		1.		<u> </u>		1			Live Load + ImpTension												
+ 340 + 247	+ 290	+ 365	+ 340							+ 203	+ 162	? + 194	4 + 194	+ 15	3 + 158	+ 176	§ § 151		+ 158	3 + 190	) + 170	) + 17	70 + 19	95 + 19	5 + 2	210 + 10	80							Reduced L L + ImpTension		+ 323 + 30	<i>)</i> 6 + 25	0 + 184	4 + 36	65 + 3 <i>12</i>	+ 290	+ 253	+ 312 +	173 +	222 + 28	1 + 294
			e e						·																								5 L	live Load + ImpComp.			·									**;
<u>- 265 - 225</u>	- 240	- 225	÷ 263	# 50	- 254 -	266 -	304	+ 233	- 282	- 355	~ 401	- 325	5 - 370	- 26	3 - 319	4 24	- 199	- 48	- 197	- 24	- 268	3 - 31	19 - 3	25 + 370	0 + 3	52 4 3	96 - 20	<b>18</b> ~ 260	0 - 248	3 - 296	- 231	- 50	6 Re	Reduced L L + ImpComp.						23 - 191	1					
+ 564 + 410	,												2 + 322						+ 262	+ 315	1 + 282			24 + 324	4 + 3									Reduced L L + ImpTen. xD (CF	· · · · · · · · · · · · · · · · · · ·	+ 535 + 50	<u> </u>	4 + 305		05 + 517	1			_287 +	368 + 477	<u> + 487</u>
- 439 - 373	<del></del>	<b>- 373</b>		- 83	- 421 -	441 -	504	<i>- 38</i> 6	- 467				9 - 614								- 444		9 - 5		4 ~ 5	84 - 6		15 - 431	<u>1 - 411</u>	- 491	- 383	3 <b>→ 8</b> 3	8 Re	Reduced L.L. + Imp. +Comp. xD (CF	F) <sup>e</sup>					70 - 316						
- 1.33 - 7.8											- 0,15		*******	- 0.2			- 0.37							17 - 0.6		41 - 0.								Ratio= Line 4 or Line 6			1.0			35 - 0.39						
+ 16 + 14	+ 12	+ 17	+ 16							1		1 + 14	1 + 14	+ 4	+ 8	+ :	) + 9		+ 10	) + 11	+ 10	) + 1	1	15 + 15		1	i i			<del> </del>				L Sidewalk-Tension		+ 16 +	16 + 1	3 + 6					" · • •	-6 +	10 + 1	+ 13
- 20 - 14 - 664 + 447	- 14	+ 17	- 19		- <u>13</u> =		- 16	+ 12	- 14	- 19		- 16	6 - 18	- 2	1000		+ 13	- 182	1 + 12	- 1	- 12	- /		16 - 18		19 + 2			2 - 12 3 <b>-</b> 1253		1122	- 150		L Sidewalk-Comp.		. 1507	47 . 13	45 , 005		16 - 10				700	1002 . 126	1 1200
				- 150	* 1384 -	1400 =	1046	+ 1317	4 1509	+ 1094	- 1364	- /3/	/ <del>* 944</del>	- 89.	* 1090	- 634	- 000	- 100		+ 256		90	+ 6	<del></del>	2 7 101	14 - 140	02 - 101	0 - 12/3	5 - 1255	7 1443	- 1133	730		Direct Design Stress		+ 1687 + 164	11 + 134°	5 + 902	2 + 69	<u> 18 + 919  </u>	+ 629	+ /12	+ /32 +	<u> </u>	1082 + 1382	+ /386
+ 179 + 364	+ 43/	- 368	+ 308																+ 1/	+ 230	<u>'                                    </u>		+ (	07									10 146	Reverse Design Stress					1 2							
																																	15													
							<i>'</i>																					,						SECTION Hole	es Out Tensian											
x4x 7/16 4x4x }	4x4x ¾	4x4x 3	6x4x 7/16	AxAx 3	4x4x \$ 4x	4x 3 4	4x4x <sup>3</sup> / <sub>2</sub>	6x4x ⅓	6x4x ±	7x4x \$	7x4x \$	6x4x 7/	16 6x4x 7/1	6 4x4x	4x4x 3	4x4x 2	4x4x 3	4x4x 2	4x4x 3	4x4x	4x4x 3	4x4x =	6x4x 7/	/16 6x4x 7/	/16 7x4x	§ 7x4x	5 6x4x	1 6x4x	\$ 4x4x ₹	4x4x #	4x4x \$	4x4x 3	a	Angles		4x4x ½ 4x4x	3 4x4x	\$ 4x4x \frac{1}{2}	½ 4x4x	3 4x4x ½	4x4x 3	4x4x 3	4x4x 🚦 41	x4x ₹ 4x	x4x ½ 4x4x	4x4x 3
29x 7/16 24x 3	24x 7/16	26x ₹	28x 7/16	24x 3	24x ½ 2	26x ±	26x ½	28× ±	28x }	30x 3	30x 2	28x 7/1	6 28x 7/10	26x 8	26x 3	24x 7/1	5 24× 7/16	24x	24x 3	24x 7/	16 26x 2	∮ 26x ½	28x 7/	16 28x 7/	/16 30x	5 30x	\$ 6x4x \$ 28x	5 28x	5 26x 3	26x 2	24x 11/16	6 24x 3	Ь	I. Web Plate	8	24x \$ 24x 9/1							24x 🗿 2		26x \$ 24x	/ 24x ₹
23x 3**) 23x 3**)	23x 3**)	23x ₹**)	23x ₹**)	23x 3**) 25	x 7/16** 1 23x	7/16+123	× 7/16** 12	23x 7/16**)	23x 7/16**	23x 7/16**	1) 23x 7/16*	*) 23x 3**	r) 23x 音***	) 23x ⅔**	) 23x 3**	) 23x }**	) 23x 3**	) 23x 3**	) 23% (2**)	23x g <sup>2</sup> **	) 24x 3**	) 24x 3**	r) 23x ₹	**) 23x }*	*) 23x 7/16	5**) 23x 7/16	6** 23× 7/16	**) 23x 7/16	6** 23x 7/16*	*) 23x 7/16**	•) 23×7/16**	23x 3**)	c	Cover Plate	2 2	?2x 7/16**) 23x }*							23× 3**1 23>	x 3**) 23x	x 3**) 23x 7/16*	* 23× 7/6**)
	-						1x4x 3	·	4x4x 3		4x4x		4x4x		4x4x 8	!						4x4x	3	4x4x	3	4x4x	3 8	4x4x		4x4x			e	Inside Angles	2											
					24x ½	26x ±	26x ½			•																							g	2. Web Plate	3	24x 3 24x 9/1	6									
																																			<del></del>						<del></del>					
685.3"	493.6"		686.3		432.0" 5		522"	648"	648"		816"			504					392"			504"				816	* 636'	636	" 496"	496"	408"	320"		LENGTH	ln.											
8,61	7.65		8.61					8.47		9.10	8.76	8,61	8.22	7.8.	7.58	7,65	7,65	7.70	7.70	7.65	7.86	7.58	8.6	1 8.2	2 9.13			8.25	5 7.93	7,71	7,69	7.70	1 1	Min. Radius of Gyration	ln.											
17,080 18,000		1			18,490 1		1	17,140	17,140	16,000	16,000	17,290	0 17,290	17,96	77,960	18,42	18.790	14,350	14,350	14,140	17,960	17,960	7 17,2	90 17,29	0 16,05	0 16.0		17,270	0 18,090	18,090	18,710	14,570	1	Allowable Unit Stress Lbs.	/5q./n.	24,000 24,00									4,000 24,000	
50.97 39.19	42.19	40.69					96.58	the second secon	90.82				7 62.41		`	1					47.94					30 86.2		3 76.82			62.82	39.19		Gross · Area	5q. /n.	85.50 82.1	19 67.19	9 53.50	I	69 49. <b>50</b>	1 ' 1	. 1	<u>39, 19</u> 42			69.14
43.49 32.44	35,47				77.82			79.38	90.82		297.30			49.90	64.94					35.47	41.27	59.38	3 43.4			0 86.	24 61.78	160		70	61.27	31.88	<del>                                     </del>	Net Area	3 <i>q.</i> //7.	72.25 68.9	4 54.6	<u>3 44.00</u>	<u>00 33,19</u>		1				46.75 56.89	56. <b>89</b>
15,290 13,770t	13,190	19,4001	14,200	4,700	17,810 17	7,210   1	7,030	16,590	16,600	13,300	16,080	16,970	0   14,860	17,926	16,880	18,25	19,250	5,700	14,490	13,540	18,260	16,060	15,8	20 14,05	0 14,23	16,26	0 0 17,430	ó. 16,58	0 18,220	o. 18,030	18,500	4,700	30	Actual Unit Stress Lbs.	/Sq./n.	23,340 23,89	0 24,580	20,500	10 21,03	30 22,980	17,920	21,950	23,180   22	.020   23,	3,120 24,330 7	24,330 0
5 C	S	S	S	<u> </u>	S	5	S	S	<u> </u>	<u> </u>	S	<u> </u>	<u> </u>	S	S	<u> </u>	5	C	C	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u>  S</u>	1 5	S	S	<u> </u>	l S	S	C	31	Materia:		S   S			<u> </u>			S	<u> </u>	<u>5</u>	<u> </u>	15

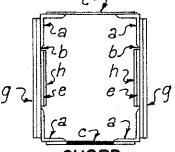
S C S S

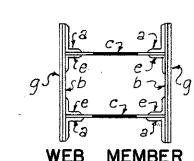
NOTE:

\*) Handhole II" Wide

\*\*) Handhole IO" Wide

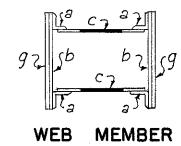
S= Special Steel
C= Carbon Steel
&= 3 Holes out of 24" webs \$\frac{4}{28}\$" webs

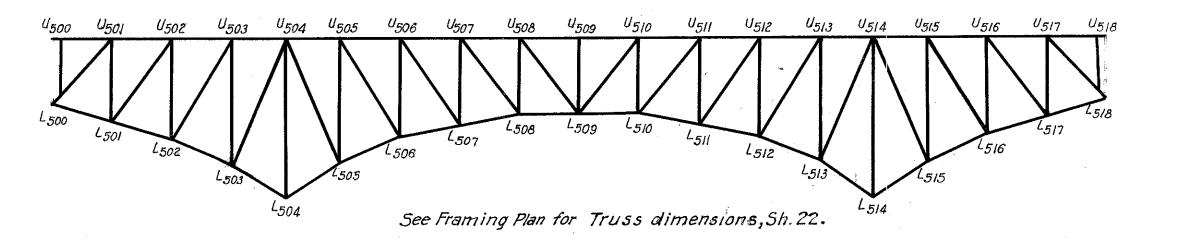




All dead load and live load stresses

are in kips. Line 29,- Net area for tension or effective gross area for compression.





PART 3

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU -42 R-17 5

> STRESS SHEET UNIT 5 SOUTH TRUSS

CLEVELAND

CUYAHOGA COUNTY

HOWARD, NEEDLES, TAMMEN & BERGENDOFF CONSULTING ENGINEERS

SCALE NONE

MADE H.W.L. DATE 5-7-54

G.U.K.

TRCD 4 M.L. UDATE 8-26-54

CKD DFR. DATE 9-27-54 KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET- 2.64

MICAOFILMED FEB 16 PR3

FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	63
2	ОНЮ	1 14.0		122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

									•																									Open 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1000 i	
							· · · · · · · · · · · · · · · · · · ·		60	MPRESSI	ON CH	ORD					······································											TENSION	CHOR	D	Í					٠	
[	MEMBER	L500 L50/	L 501 L 502	L 502 L 503	L 503	L 504 L 503	L 505 5 L 50t	6 L 506	L507 L 508	L 508 L 509	L 509	L 510	L 5/1	L 5/2	L 5/3	L514	L 5/5	L 516 1 517	L 517	U500 U50	U501 U501	U 502 U 50	U503 3 U50	U504 11505	U505 U506	U 506 U 507	U 507 U508	U508 U509	U509 U510	U510 U5//	U511: U512	<u>U512</u> 2 <u>U51.</u>	U513 U514	U514 U515	U515 U516	1516 	U517
ead Load	<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>	- 1043	- 1907	- 2629	- 3229	- 3302	- 3162	- 2965	- 2711	- 2585	- 2348	- 2286	- 2392	- 2501	- 2604	- 2586	- 2104	- 1510	+ 806	9.00	+ 999	+ 1827	+ 2424	+ 2911	+ 2914	+ 2665	+ 2585	+ 2353	+ 2353	+ 2348	+ 2248	+ 2350	+ 2302	+ 1907	+ 1449	+ 773	
.8 Dead Load		- 834		- 2103							- 1878	- 1829	- 1914		- 2083	# 2069		- 1208	- 645	1	+ 799		+ 1939	+ 2329	+ 2331	+ 2132	+ 2068	+ 1882	+ 1882	+/1878	+ 1798			+ 1526		+ 618	
ive Load + ImpTension				2.00	4300					1.000						7 270				1																	
educed L L + lap. Tension	)		<u> </u>				+ 161	+ 325	+ 473	+ 599	+ 599	+ 473	+ 325	+ 161			1	'			+ 229	+ 397	+ 503	+ 650	+ 723	+ 743	+ 807	+ 791	+ 791	+ 788	+ 693	+ 641	+ 577	+ 448	+ 360	+ 205	
ive Load + ImpComp.	. ,																				1 1,41,4	1	1 3-3	,													
educed   L + ImpCamp.		- 240	+ 414	- 544	- 637	- 652	- 707	- 736	+ 756	- 806	- 788	- 706	- 652	- 624	- 576	~ 571	÷ 494	<i>⊬</i> 377	- 214	<b>1</b>				- 149	- 319	÷ 466	- 599	- 613	- 613	- 599	- 466	- 3/9	- 149				
duced L L + ImpTen. x	D (CF) E	2-10				1	+ 267	+ 539	+ 785	+ 993	+ 993	+ 785	+ 539	+ 267	1 3.0						+ 380	+ 658	+÷ <i>833</i>	+ 1077	+ 1/198	+ 1231	+ /337	+ /3//	+ 1311	+ 1306	+ 1148	+ 1062	+ 957	+ 742	+ 597	+ 340	
		- 398	- 686	- 902	- 1056	- 1081	- 1172		- 1253	-1336	- 1306	- 1171	- 1081	- 1034	÷ 955	- 947	- 818	- 625	÷ 355					- 247	- 529	- 772	- 993	- 1016	+1016	- 993							
educed L L + lmp. +Comp. x Line 4 atio= Line ((Comp.) or -	Line 6 Line I (Ten.)					·	- 0.05	+ 0.11	- 0.17	-0.23	- 0.26	+ 0.21	- 0.14	- 0.06		,								- 0.05	- 0.11	- 0.17	- 0.23	+ 0.26	- 0.26	- 0.25	- 0.207	- 0.136	- 0.06				
U. Sidewalk-Tension							+ 8	+ 17	+ 25	+ 32	+ 32	+ 25	+ 17	+ 8							+ //	+ 19	+ 26	+ 38	+ 47	+ 52	+ 59	+ 58	+ 58	+ 57	+ 49	+ 42	+ 33	+ 21	+ 16	+ 8	_
L Sidewalk-Comp.		- 11	- 20	- 28	- 34	~ <i>3</i> 5	- 42	- 48	<b>-</b> 53	~ 59	<b>-</b> 57	- 50	- 43	- 36	- 29	- 29	- 24	- 17	<b>-</b> 9					- 8	- 17	- 24	+ 32	<del>- 33</del>	<b> 33</b>	- 32	- 24	÷ 17	- 8				
Direct Design Stress		- 1243	- 2232	- <i>3033</i>	- 3673	- 3758	- 3744	- 3640	- 3475	+ 3463	- 3241	- 3050	- 3038	- 3071	-3067	- 3045	+ 2525	- 1850	- 1009		+ 1190	÷ 2139	+ 2798	+ 3444	+ 3576	+ 3415	+ 3464	+ 3251	+ 3251	+ 3241	+ 2995	+ 2984	+ 2832	+ 2289	+ 1772	+ 966	
Reverse Design Stress			*																										·,			,,,,,			4		
																																			1		4—
																																			+		_
	Holes Out																																	***************************************			
SECTION	for lension	managaman walla																		711									· .						1		
a Angles	2	8×6× 7/16	8x6x 7/16	. 8x6x 8	8x6x 8	8x6x ₹	8x6x ₹	8x6x ₹	8x6x ₹	8x6x 7	8×6× 2	8x6x <sup>7</sup>	8x6x 8	8x6x 2	8x6x 7	8×6× 7	8x6x ₹	8x6x 7/16	8x6x 7/16	8x6x 7/16	8x6x 7/16	8x6x 3	8x6x ₹	8×6× 7	8x6x 7	8x6x 7	8x6x 7	8×6× 3	8x6x 3	8×6× 3	8x6x 3	8x6x 3	8×6× 3	8×6× ₹	8x6x \$	4×4× 1	
1. Web Plate	4	30x 9/16	30x 9/16	30x ₹	30x 13/16	5 30x 13/16	30x 13/10	6 30x 13/16	30× 13/16	30x 13/16	5 30x 13/16	30x 3	30x ₹	30x ₹	30x 3/4	30x ₹	30x ∯	30x ⅔	30x ₹	30x ₹	30x ₹	30x 3	30x ₹	30x 13/16	30x 13/16	30x 13/16	30x 13/16	30x ∰	30x \$	30x ₹	30x ₹	30x ₹			30x 11/16		
Cover Plate	2	22× 3/8	22x 3	22x ½	22x 5	22x ₹	22x \$	22x ∯	22x \$	22x \$	22x §	22x \$	22x ₹	22x \$	22x 💈	22x ≩	22x 👼	23x 3	23x 3	23x 5/16	23x 5/16	22x \$	22x \$	22x ₹	22x \$	22× §	22x \$	22x ₹		22x \$						40.00	
Bottom Plate	2			22x =**)	22x 3**)	22x 3**)	22x ∄**)	22x 3**)	22x ¾**)	22x ¾**)	22x 3**)	22x 3**)	22x 3**)	22x ¾**)	22x 3**	22x 3**	) 22× ¾**)	$23x \frac{1}{2}*)$	23x ½*)	23x 3*)	23x 🕺*)	22x 3**)			22x 3**)	22x 3**)	22x 3**)	22x 2**)	22x =***)	22x 3**)	22x 3**)	221( 3**)	22x 3**)	22× ±*)	22× ±*)	23× (*)	12
1. Unside Web Plate	2		14x 3		14x 3													14×16						•	14x 3			14x 🛔		14x 3	14x 💈						
Inside Web Plate	4	· .	<u> </u>		1:1:	1 4 1 1 1 1	1:1	·	A. A. A. A. C.	, 1 10	. 11.77			**																							
2. Outside Web Plate	4	,	30x 9/16	30x ₹	30x 13/16	30x 13/16	30x 13/16	6 30x 13/16	30x 13/16	30x: 13/16	30x 13/16	30x 3	30x ¾	30x ₹	30x 3	30x ₹	30x ₹	30x 3					30x ½	30x 13/16	30x 13/16	30x 13/16	30x 13/16	30x ₹	30x ₹	30x €	30x ₹	30x ₺	30x ₹	30x 7/16	4		+
2. Inside Web Plate																													·								+
ength	12.	3/5.8 "	3/3.3*	325.4"	353.4"	369,8"	325.77"	305.20"	305.20"	300.0"		305.2"	<i>305.2</i> "	325.8"		365.2"	331.1"	318.0"	316.3"								<u> </u>						<u> </u>		<del></del>		-
ndius of Gyration	/n.	10.61	10.48	10.90	10.60	10.51	10.51	10.60	10.80	10.80	10.80	10.80	10.80	10.80		10.80	10.90	10.84	10.63												<u> </u>						+
Howable Unit Stress	Lbs / Sq. In.	19,590	19,590	19,590	19,490	19,430	19,560	19,620	19,630	19,650	19,650	19,630	19,630	19,580			19,570	19,600	19,590	24,000		24,000		24,000	24,000	24,000	24,000	24,000 158.51	24,000	24,000	24,000	24,000		24,000			
oss Area	Sq.In.	71.22	115.47	154.42					176.67			158.67		158.67			131.19		60.85	)		107.51		166.17	176.67	166.17	166.17	158.51	158.51		148.01		137.51	114.69	88.44		
et Area	5q./n.	<i>6</i> 7. <i>8</i> 5	115.47	154.42	187.17	190.67	190.67	187.17	176.67	176.67	166.17	158.67		158.67		158.67	131.19	95.22	54,28	49,72		92.14		142.80	151.80		142.80	136.14	136.14		127.14		118.14				+
ctual Unit Stress	Lbs. /5q.In.	18,320	19,330	19,620	19,600 0	19,700 0	19,640	19,450	19,650	19,600	19,500	19,220	19,150	19,350	19,340	19,200	19,220	19,370	18,590		23,930	23,200	23,600	24,100 0.	<sup>23</sup> ,550	23,920	24,250 %	23,880	23,880	23,800	23,600	23,450	23,950	23,200	23,400	23,850	+
terial		ء ا	9	- g	- 5	9	0	۱ ،	c	١ ٥	9	9	1 5	۱ ۹	8	S	5	S	S	II s	S	5	S	l s	S	S	S	S	l s	S	S	S	S	- S	S	.5	

	····		·		· · · · · · · · · · · · · · · · · · ·						, ,	'			MODÉC (			45405	<u> </u>				· · · · · · · · · · · · · · · · · · ·									4		1.1							·T1	ENICION	. WED	MEMO	EDC		**************************************	**************************************
									4					CO	MPRES	SION W	AFR M	MEMBE	<del>KS</del>															<u> </u>			<u> </u>	,			15	TNSION	WE B	MEMB	LKO			
U 504 L 502	L 509 U 51	10 L 510 U51	11 L512 11 U	2 L 513 1513 U514	4 L 500	U 501 L 501	U 502 M 502	M 502 L 502	U 503 M 503	M503 L503	U 504 M 504	M504 L504	u 505 M 505	1 505 L 505	J 506 L M 506	506 U S L 506	507 L 507	508 U L 508	509 U510 L509 L	510 L	11   U.5 .511	12 M 5 M 512	512 U L 512	513 N M 513	1513 L513	U 514   1 M 514	M514 L514	u 515 M. M515	515 U 5 L 515	516 / M 516	M 516 U L 516	517 L517	1518 - L518 -		MEMBER		L 500 U501	L 501 U 502	L 502 U 503	L 503 3 <u>U 50</u> 4	14 <u>L 50</u>	16 L 50	0507 17 L 50	8 L 509	U5/2	514 L515	15 UE L 5/6	17 U 5/8 L 5/7 L 5/8
- 148	+ 9	9 - 16	7 +	94 - 133	- 88	- 1269	+ 1330	<i>4 1473</i>	- 1189	+ 1335	- 896	- 698	- 132	- 277	- 507	- 649 -	- 241 -	430	- 123 -	18 -	1 -	284 -	426	÷ 52	- 197	- 715	+ 615	- 900	1046 +	1049	- 1192	- 948	- 85	I Dea	d Load		+ /521	+ 1491	+ 1198	+ 967	* 6	5 + 477	7 + 130	+ 381	+ 185	+ 762	- 885	1140 + 1137
+ 118	- 04	7 - 13	4 +	75 - 106	- 70	- 1015	- 1064	- 1178	- 951	- 1068	- 717	- 558	- 106	- 222	- 406	- 519	- 193 -	344	- 98 -	94 +	1 -	227 -	341	- 42	+ 158	- 572	- 492	- 720 -	· <i>8</i> 37 -	839	- 954	- 758	- 68 2	2 0.8	Dead Load		+ 1217	+ 1193	+ 958	+ 774	÷ 5					+ 610 +	708	912 + 910
										,								***************************************															3	3 Liv	e Load + ImpTension								ŕ		,		*	
+ 332	+ 24	5 + 27	9 + 3	355 + <i>332</i>	'						+ 170	+ 213	+ 207	+ 207	+ 164	+ 164 +	+ 185 +	/53	4	165 +	209 +	184 +	184	. 212	_ 212	184	± 218						12		luced L L + Imp-Tension		+ 347	+ 319	+ 258	+ 208	+ 355	, + 30C	+ 279	+ 256	+ 300	+ 186	. 219	289 + 300
																										•	•								e Load + ImpComp.													
252	- 228	3 + 26	4 - 2	248 - 252	- 52	- 271	- 276	+ 317	- 237	- 278	- 347	- 378	- 319	- 362	- 260	- 306	- 237 -	204	- 45 -	195 - 2	237 -	260 -	306	÷ 319	+ 363	- 344	- 377	- 204 -	- 254 -	247	- 293	- 236	- 52 6		luced L L + ImpComp.						- 241	- 197	7 - 232	213	- 222	***************************************		
+ 550	+ 400	5 + 46	2 + 5	589 + 550							+ 282	+ 353	+ 343			+ 272 +	+ 307 +			274 +		305 +				+ 305	+ 362								luced L L + ImpTen. xl	)(CF)e	+ 575	+ 529	+ 427							+ 308 4	· 363 ·	479 + 497
- 418	- 378	3 - 43	8 - 4	411 - 417	- 86	- 450	÷ 458	- 526	÷ 393	+ 461	+ 575	- 626	- 529	- 600		- 507 -	393	338		323 - 3	393 -			- 529		- 570		- 338 -	. 421 -	410	486	_ 30/	_ 86 8								- 400				<b>- 3</b> 68			,
- 2.24				.78 - 2.50								- 0.31		- 0.75		- 0.25 -	0.17	0.36			209 -			- 4.08		- 0.26	,						9	9 Rat	luced L L + ImpComp. ) io= Line 4 comp.) or	Line 6 Line / (Ten.)					- 59.1		1 - 1.78		- 1.20			
				17 + 17							+ 11					+ 8 +				10 +				+ /5		+ 12	+ 12							10 LL	Sidewalk - Tension		+ 16	+ 16	+ 13	+ 10	+ 17	+ 12	1 + 12	+ 16	+ 14	+ 8 +	+ 10 +	13 + 13
- 18	- 14	4 - 1.	4 -	18 - 18	- 1	- 13	- 14	- 16	- 12	+ /5	- 20	- 22	÷ 16	- 19	- 13	+ 15	- 11 -	13	- 1 -	12 _	11		/5	- 16	_ 19	_ 20	_ 22	- 10 -	. 12 .	12	* 14	11	+ 1 1	H LL	. Sidewalk - Comp.						- 17	- 10	) - 12	- 12	+ 12			
- 554	<u>~ 39</u> 5	9 - 586	6 - 5	504 - 541	- 157	+ 1478	- 1536	÷ 1720	- 1356	÷ 1544	<i>→ 1312</i>	- 1206	÷ 651	- 841	- 85O	1041	597 -	695	- 174 - 4	129 - 4	405 -	671 -	863	- 587	- 778	- 1162	- 1139°	- 1068 -	1270 -	1261	- 1454	- 4160	- 155	12 Dire	ect Design Stress		+ 1808	+ 1738	+ 1398	+ 1:129	+ 422	. + 869	9 + 578	+ 746	+ 659	+ 926	+ 1081 +	1404 + 1420
				531 + 461		, , , ,						1	+ 176							104 + :				+ 325									1.00		erse Design Stress						+ 600	<i>j</i>	- 250		- 68		,	
							1.5																											14														
																																	, i	15														
								,						, .																				,	SECTI <b>O</b> N	Holes Ou for Tensio	<i>†</i>									, <u> </u>		
6x4x 7/16	AxAx	3 AxAx	3 4x4	4x 3 6x4x 7/1	5 4x4x 3	∆x4x ¾	4x4x 3	4x4x 3	6x4x ‡	6x4x ½	7x4x \$	7x4x 5	6x4x ±	6x4x \$	4x4x 3	4x4x 3	AxAx 3	4x4x 3	1x4x # 4x4	1x <sup>3</sup> Δx4	4x 3 4	4x4x 3 4	4x4x 3 6x	4x 7/166	4x 7/15	7x4x }	7×4× 5	6x4x ½ 6	Svav #	AVAY 3	4×4× <del>3</del>	1414 3	1-1-3		Outer Angles	2	4x4x \$	4x4x \$	4x4x \$	4x4x \$	4x4x 3	4x4x /	3 4x4x 3	Axax 3	4x4x 3	AxAx & A	x4x #	1×4× } 4×4× }
28x 7/16		3 24x 7/1	6 26	x <del>3</del> 28x 7/1	6 24x 3	24x ½	26x ½	26x ½	28x 7	28x 7	30x 3	30x ₹	28x 7/16	28x 7/16	26x \$	26x \$ 2	4x 7/16	24x ±	1x4x <del>}</del> 4x4 24x <del>}</del> 24	x 3 24	x 3 26x	7/16 26	x 7/16 2	Bx 7/16 2	3x 7/16	30x ≸	30x \$	28x \$	28x \$			24x 3	24v 4	b	1. Web Plate	•	24× \$		26× 13/16	9 28x 9/16	6 26x 3	24x	24x	24x 3	24x ±	28× ±	26x ₹ 24	x 113/16 24x 13/16
										23×7/16**	2327/16**1	23×7/16**)	23×7/16**)	23×7/16**1	23x 4**)	23x 3**) 2	3× 3**)	3v 3**)	av 3**) 23x	3**) 23x	3** 22	x 3**) 24)	× 3**) 2	3x 2***	23, 3**)2	29×7/16**	27.7/16**	23×7/16**) 23	v7/40+* 22	~7/6++)2	3×7/6**)	3+*1	270-3**)	c	Cover Plate	2	22x7/16*	* 22x 3**	) 23x 3**)	24x 3**	) 23x 3**	*) 23x 3*	*) 23x 3**	) 23x 3**)	23x 3**) 2	23x 3**) 23	x 3**) 23	×7/16**) 23×7/16**)
					,,			4x4x 3		4x4x 3	,, , , , , ,	20,11,10	20,7,10 /	4x4x 3		4x4x 3	*** / -	* 1	3 8 1 234	8 /		4	x4x 3		4x4x }				1×4× 3		4x4x 3	8 / 6																*
·						24x ±	26x ½																			,								a	2. Web Plate	. 3	24x \$	24x #										
										:		****																														, ,						
705.1"	493.6	" 493,6	586	.5" 705.1"	3.42"	432.0"	522"·	522"	648"	648"	8/6"	816"	63/"	631"	504"	504"	448"	392"	392" 39	2" 44	8"	504"	504"	63/"	631**	816"	816"	636"	636"	496"	496"	408"	320"	25 Len	ngth:	In.												
- 8.61			5 7.9	93 8.61	7.70	7.63	7.92	7.75	8.47	648** 8.22	816" 9.10	816" 9,10	8.63	8.26	7,83	7.58	7,65	392" 7,60	7.70 7.	70 7.	8" . 70	504" : 7,89	7.59	631" 8,61		9.13	9.13	8.54	8.25	7,99					. Radius of Gyration	ln.												
13,320				480 13,320			17,910	17,910		17,140	16,300	16,300	13,530		17,960	17,960 1				350 14,	160 1		7,970			16,330	16.330	17,270	7	8,120	18.120	18.700	14 560			Lbs./5q./n.	24,000	24,000	24,000	24,000	18,000	0 24,000	18,000	24,000	18,000	24,000 2	4,000 2	4,000 24,000
50.97			1 40	.69 50.97					79,38			82.30	54.88	66.32	53.69	65.13	42.19				.19		56.13			74.80	74.80				83.58	64.19	39.19	28 Gra	oss Area	Sq. In.	88.94	87.44				9 45.19		1 .		49 19 5	4	72.14 72.14
44.67	3	8 34.71	32.	.82 44.67		81.14			79.38			82.30	48.18	66.32				38.52	31.88 31	.88 31					62,04	71.20	71.20				83.58	64.19	31.88		Area	Sg. In.	74,69			47.00	33.19	9 37.69	32.44	1 32.44				59.52 59.52
12.390		0 16,900	) 15.3	330 12,090		18,200	18,020 06%	17,940	17,090	17,000			13,500	12,690		16,030 1			5,450 13,	150 12,	700 18	8,010 1			2,520	16,320	16,000		6,520 1		17,400	18,070	4,860	30 Act		bs./Sq./n.	24,200 08	23,650				o. 23,050	17,82	0 23,000	17,500	22,760 2		3,580 23,850
C	C	S	Ś	C	c	5	S	s	S	S	\$	S	C	С	S	S	S	S	c	$c \mid c$	. [	s	S	C	Ċ	s	S	S	s	S	S	S	C	31 Ma	terial	<del></del> .	S	S	s	S	l c	s	C	5		s	S	5 S

NOTE \*) Handhole II" Wide

\*\*) Handhole IO" Wide

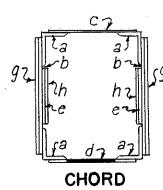
S= Special Steel

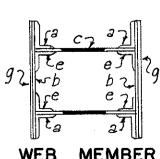
C= Carbon Steel

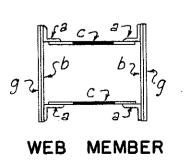
# 3 Holes Out of 24" Webs

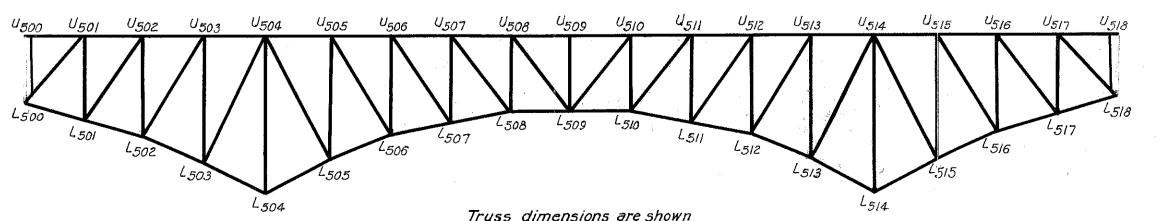
4 Holes out of 26" and 28" Webs

All dead load and live load stresses are in kips Line 29, Net area for tension or effective gross area for compression.









Truss dimensions are shown on Framing Plan, Sh. 22

PART 3

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU -42R-17 5

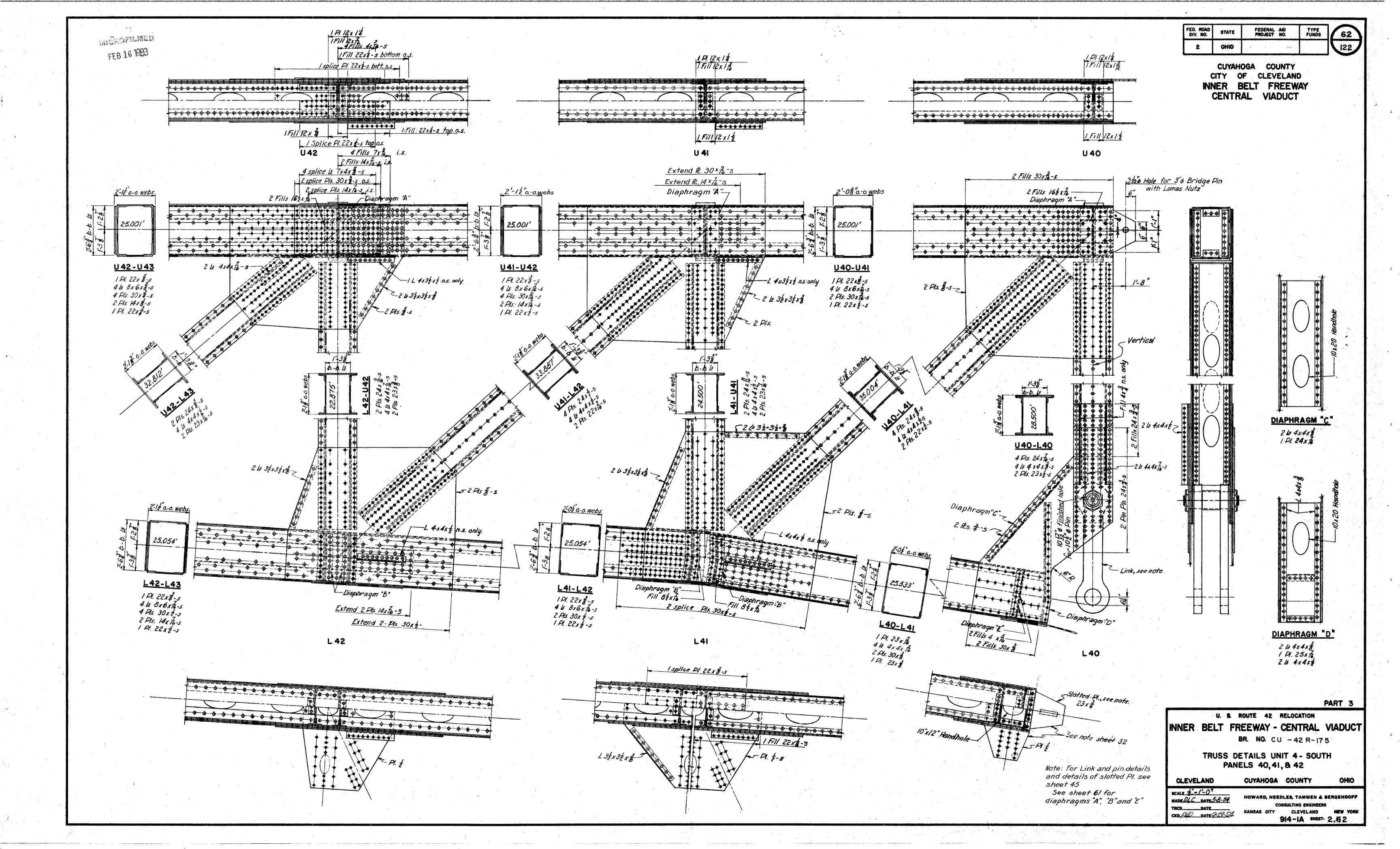
> STRESS SHEET UNIT 5 NORTH TRUSS

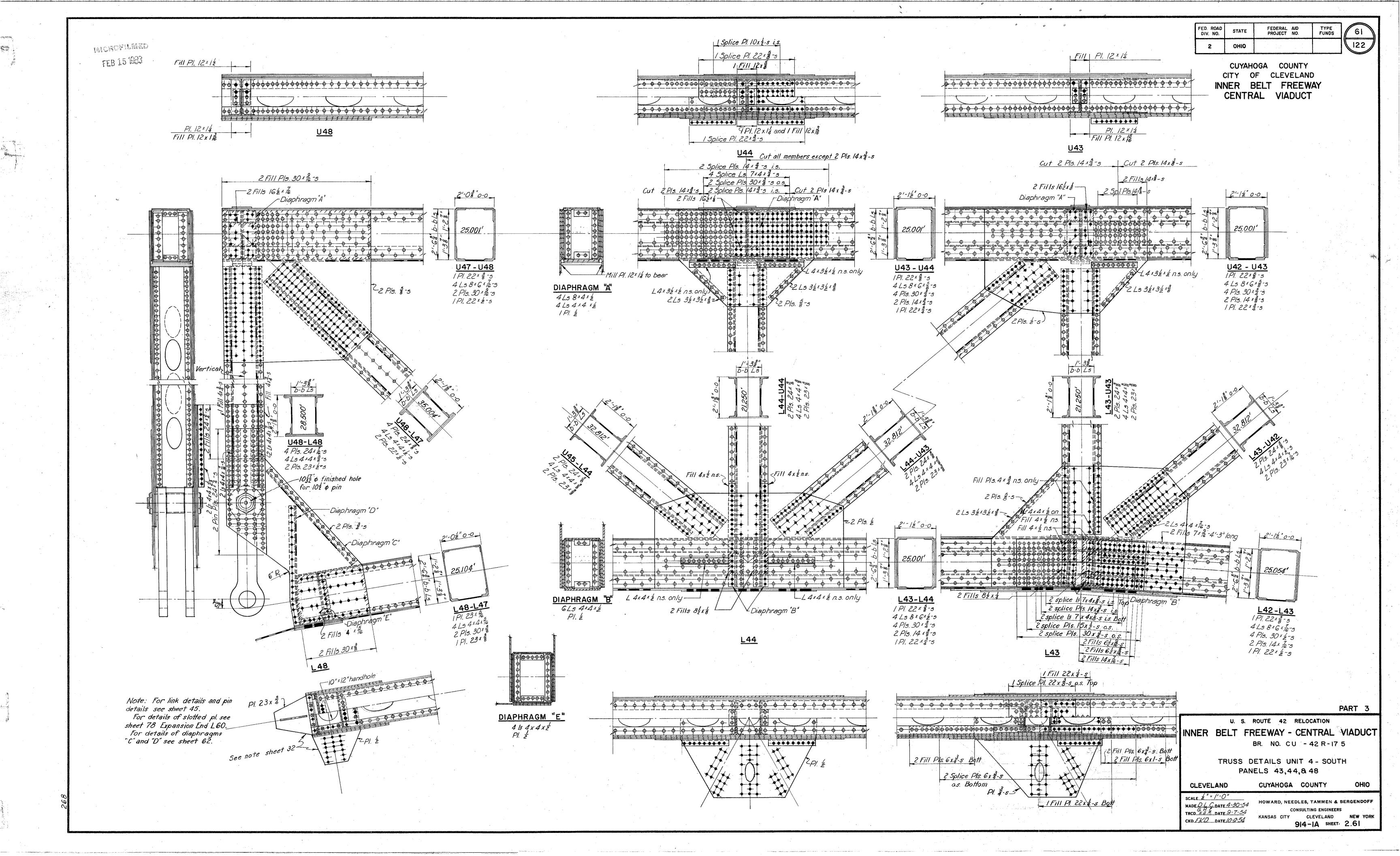
OHIO CLEVELAND CUYAHOGA COUNTY

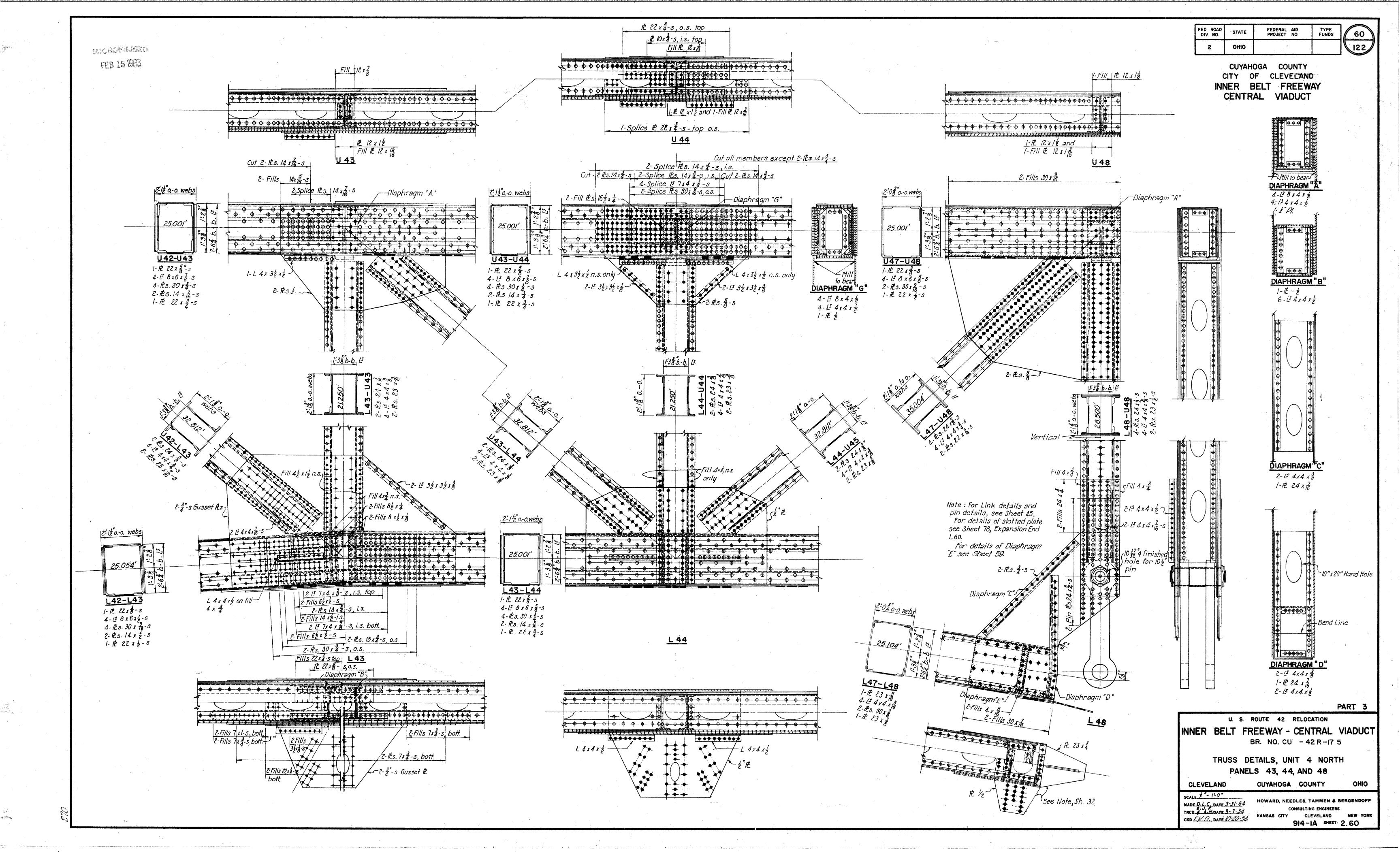
scale *Nome* MADE <u>H.W.L.</u> DATE <u>5-6-54</u>
G.J. K.
TRCD <u>4 M.L.</u> DATE <u>8-26-54</u>
CKD <u>P.L.C.</u> DATE <u>8-27-54</u>

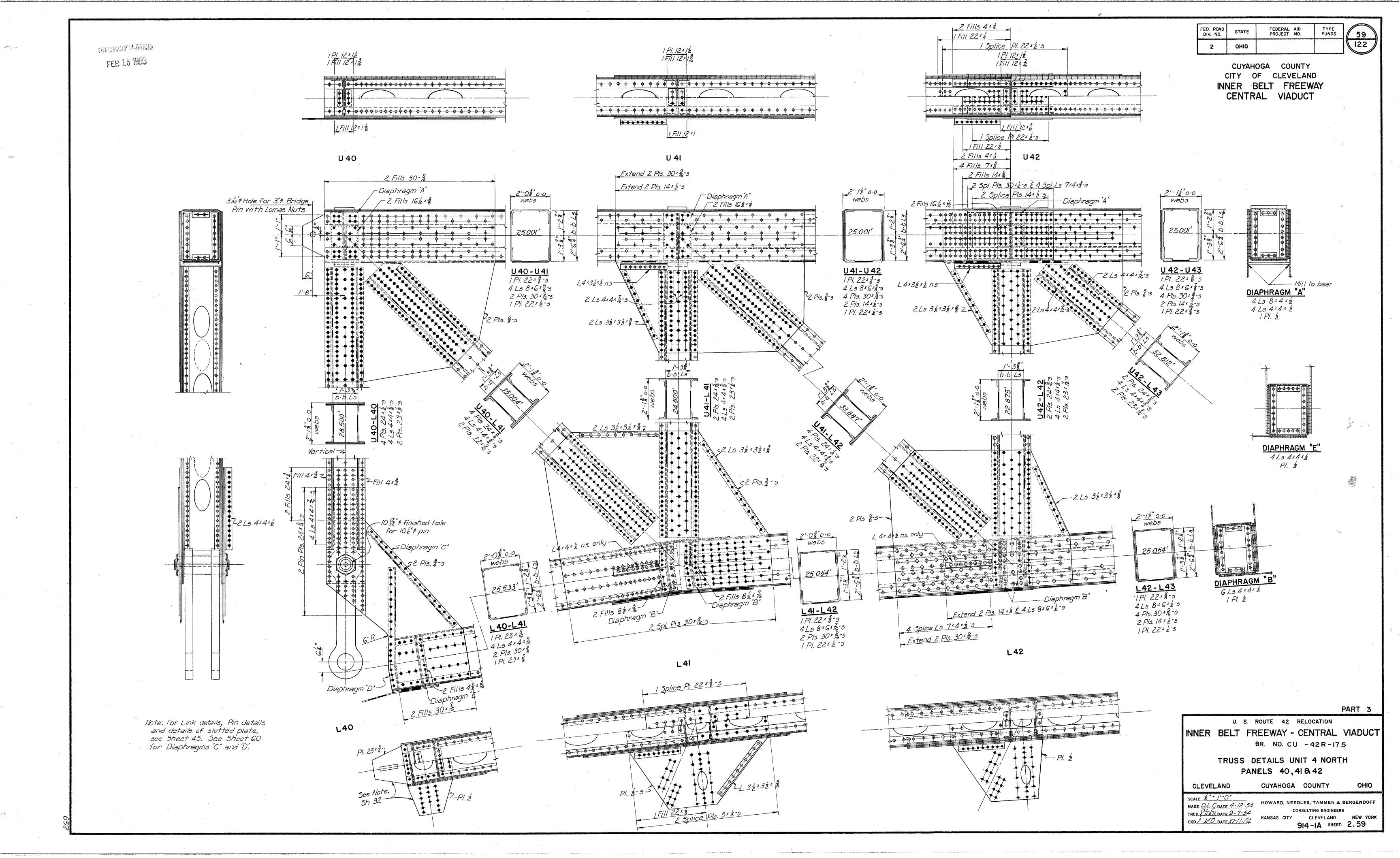
HOWARD, NEEDLES, TAMMEN & BERGENDOFF

KANSAS CITY CLEVELAND NEW YORK 914-1A SHEET 2.63









FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	6
2	оню			

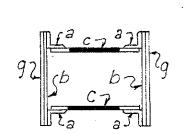
CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

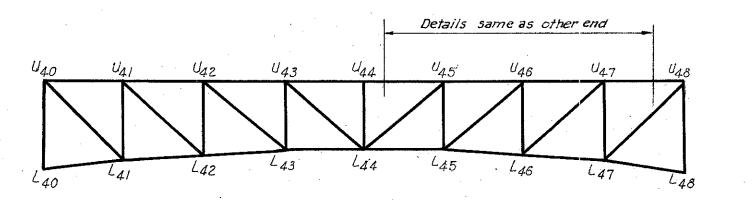
N CHO	RD-SOU	JTH TI	RUSS				C	OMPRES	SION	CHORD -	- SOUTH	TRUS	<u> </u>	<u></u> ш	1				• .	TENSIO	N CHO	RD- NO	RTH T	RUSS				1	COMPRE	SSION	CHORD-	- NORTH	TRUS	
42 L43	. 43 L 44	.44 L45	L45 L46	L 46 L 47		U 40 - U41	U41 U42	U42	U43	U44	U45	U46		_   S		MEMBER	L40	) L41	L	42 1.	43 4	.44	L 45   46	L46	L 47	U40		U42 1143	U43	1 44	U 45	U46	U47	ا م
					0		/- 1861	- 2509	- 2681			<del> </del>	- 1013	<del>,</del> ,	Лоза			***************************************		+ 2028	+ 2729	+ 2729	+ 2028	+ 1101	0	- 1098	- 2023	- 2729	- 2916	- 2916	- 2729	- 2023	- 1098	+
+ 1492	+ 2007	+ 2007	+ 1492	+ 812	0	÷ 811	- 1489	- 2007	- 2145	- 2145	- 2007	- 1489	- 811		1		.								0	1				I ' ' '				
													,	il "		•									***************************************	_								
+ 470	+ 620	+ 620	+ 470	+ 262	0													0 +	288	+ 518	+ 682	+ 682	+ 5/8	+ 288	0									
				· · · · · · · · · · · · · · · · · · ·						<u> </u>																								_
						→ <i>2</i> 59	- 469	± 620	- 643	- 643	- 620	- 469	- 259	6						` ;						- 285	- 5/7	- 682	- 708	- 708	- 682	- 517	- 285	
+ 780	+ 1027	+ 1027	+ 780	+ 434	0	400	ana	1007	1000	1.000	1007	770	430	7				0 +	478	+ 858	+ 1131	+ 1131	+ 858	+ 478	0					4.75				_
	,	····				- 430	÷ 7/9	+ 1027	- 10bb	÷ 1066	- 1021	* 119	* 430	8	Redu	Line 4 on Line 6									,	<i>- 473</i>	<u>- 856</u>	<u>- 1131</u>	<i>- 1173</i>	1173	<u> + 1131</u>	- 856	~ 473	+
+ 21	+ 29	+ 29	+ 21	+ 11	0		ļ												/2	. 22	. 31	, 31	. 33	, /2						+				+
7 bm 7						- 11	- 21	- 29	- 31	- 31	- 29	- 21	- 11	11	1		<u> </u>	<u> </u>	13	+ 43	+ 31	+ 31	+ 23	+ 13	U		// Tab	31	30	1			. 10	+
+ 2293	+ 3063	+ 3063	+ 2293	+ 1257	0		<del> </del>		· · · · · · · · · · · · · · · · · · ·			·						0 . ,	372	+ 2504	T 557E	1 93/5	± 2504	± 1372	0	· · · · · · · · · · · · · · · · · ·			1 .					+-
								<del>-</del>						111				. 7		7 2,304	T 3343	<del>+ 3343</del>	7 2304	T +3/2		1303	2-450	1 3343	3340	3340	3343	2420	1,000	+
														14	7,072									· · · · · · · · · · · · · · · · · · ·									-	
														15																				
														16																				$\bot$
	,									<del></del>				17																				_
															S																			
	8x6x ½	8x6x ½	8x6x 7/16	8x6x 7/16	4x4x 5/16	8x6x 7/16	8x6x 7/16	8x6x ₹			8x6x 8	8x6x 7/16	8×6× 7/16		a F	ge Angles	2 4x4	x 5/16 8x8x	7/16 8	8x6x ±	8x6x ∰	8x6x \$	8x6x ½	8x8x 7/16	4x4x 5/16	8x6x \$	8x6x ₹	8x6x ₹	8x6x 7	8x6x 7	8x6x ₹	8x6x ₹	8x6x ₹	
					30x 3/8	30x 9/16	30x 9/16	30x 3/4	30x 3	30x 3/4	30x 3.	30x 9/16	30x 9/16		b 1	Web Plate	4 30	( <sup>3</sup> / <sub>8</sub> 30x	9/16 3	30x 9/16	30x ¾	30x 3/4	30x 9/16	30x 9/16	30x ⅓	30x 9/16	30x 9/16	30x ¾		30x 3				
22x \$	22x \$	22x §	22x 3	22x 🕏	23x 5/16	22x 💈	22x 🗿	22x \$	22x \$	22x 著	22x 3	22x 3	22x 🖁		c Ta	Cover Plate	3 23	c 5/16 22×	3 6	22x 💈	22x ₹	22x 5	22x3	22x 3	23x 5/16	22x 3	22x 🖁			22x 5	22x \$	22x 3	22x 3	
22x 2*1	22x 3**1	22x 2**)	22x ½*)	22× ½*)	23x **)	22x ½*)	22x ½*)	22x 3**)	22× 3**)	22x 3**)			22x ½*)				2 23	$(\frac{3}{8}*)$ 22x			22x 3**)	22× ¾**)	22x ½*)	22x ½*)	23x ∄**)	22x ½*)	22x ½*)		22x 3**)	22x 3**)	) 22x 3**)	22x ½*)	22x ½*)	
									30x 3	30x ∄					1 <b>-</b>	· · · · · · · · · · · · · · · · · · ·	_4								·r.				30x 3	30x 3	30x 3			-
4X // /O	141 8	14X g	14X 7/16				14x //16	14x g	14x <del>3</del>	14x 3	14x #	14x 7/16			h h	de Web Plate	2			14x ½	14x 🕏	14x g	14x ±		,		14x ½	14x 7/16	14x 3	14x 3	14x 7/16	14x ½		
			-																	-			,											_
						200	300	200	200	200	200	220	200	20	7 <b>1</b> 00.878								······································							-				-
						300	300	300	300	300	300	300	300				·						····			300	300	300	300	300	300	300	300	+
24,000	24,000	24,000	24,000	24.000	18,000	19,630	19.620	19.640	19 630	19.630	19 640	19 620	19 630	27	7 Alda	To Street Lbs. 150	7. /17. 10	000 24	000	24 000	24 000	24 000	24 000	24.000	Is mo	19:630	10 620	19.640	19.640	10 640	10 610	10 630	10 620	-
				i	1	11	1	1	E :	· ·	,	1 ' ;	1 1	28	3 Ant.									1		11								+
								1						29	Ale+	a So		3.60					•			11		<del></del>		i i		1		+
					0			1					1 :			Unit Stress Lbs. 150		0 22									19,400	19.570	19.700					+
S	S	S	S	<u> </u>	С	S	5	S	S	S	S	s						<u>c</u> 1	S	S	S	S	S	S	C	s	Š	S	S	S	S	S	S	
1						ll		1		-	1	1	I	11	1		11									1		1	1	1	-1	1		7
4 4 x 2 1	2 L 43  + 1865  + 1492  + 470  + 780  + 21  + 2293  6x 7/16  30x \(\frac{1}{2}\) 22x \(\frac{3}{2}\) 27/16  4,000  09.72  94.35	2	2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	2	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 1 43 4 44 145 146 146 147 47 48 49 141 041 142 48 48 48 146 147 148 148 148 148 148 148 148 148 148 148	2	2	2 L 43   44   45   45   46   47   46   47   46   47   46   47   47	1.43	Color   Colo	1.43	2   1.65   1.65   1.66   1.67   1.67   1.67   1.66   1.67   1.67   1.66   1.67   1.67   1.66   1.67   1.67   1.66   1.67	2   1.   1.   1.   1.   1.   1.   1.   1	1	1.5	Fig.   1.50	Control   Cont	## MEMBER   1/9   1/8	2   1.00	Control   Cont	## 1	## MEMBER 15 19 16 17 18 19 16 19 17 18 19 18 19 19 19 19 19 19 19 19 19 19 19 19 19	MEMBER   10   10   10   10   10   10   10   1

TE	NSION	WEB M	EMBERS	- SOUT	H TRU	SS			COMP	RESSION	I WEB	МЕМВЕ	RS - S	OUTH 1	RUSS		ш	······································			TE	NSION	WEB N	MEMBERS	S- NOR	TH TRU	SS			COMPF	RESSION	WEB	MEMBER	RS - NOR	TH TR	USS
U40 L41	441 L41	2 U42 L43	U43 L44	L44 U45	L 45 U46	L 46 U47	L 47 U48	U40 L40	U41 L41	U42 L42	U43 L43	U44 L44	U45 L45	U46 L46	U47 1.47	U48 L48		MEME	3ER	U40 L41	U41 1 12	U42 1.4.5	143 144	L44 U45	L 45	L'46 U47	L47 1148	U40,10	U41 / 11	442 112	443 143	U44 111	U45 L45 U	46 406 4	47 (47	148 148
+ 1418	1	+ 850	1	1				11."		A								nd Load		+ 1538		+ 926	1	1		i .	1	i 1		1			- 306	. 1	1	
+ 1/35	+ 921	→ 680	+ 182	+ 182	+ 680	+ 921	+ 1/135	+ 918	- 718	÷ 537	- 214	- 102	- 214	+ <i>5</i> 37	- 718	- 862	2 0.8	3 Dead Load	,	+ 1231	i .'			I .		1		! !		1 1			- 245	į. ·		
																		e Load + Imp. +Tension	<u> </u>																	
+ 364	+ 3/6	+ 263	+ 160	+ 160	+ 263	+ 316	+ 364			+ 9	+ 35		+ 35	+ 9			11 1	luced L L + imp. =Tens	ion	+ 401	+ 348	+ 289	+ 176	+ 176	+ 289	+ 348	+ 401			+ 9	+ 39		+ 39	+ 9		
																		e Load + ImpComp.					<u> </u>							·					·	
. 602		+ 28				- <del></del>		- 269							<del>- 228</del>	- 264		tuced L.L. + ImpComp					- 109				·	<i>- 296</i>	<del>-</del> 251	1		<u>+ 51</u>	+ 1/9		<u>* 251</u>	- 290
+ 603		+ 436					+ 603			+ 14	+ 58		→ <u>58</u>					tuced L L + Imp.⇒Ten.		11 1	1		+ 291		į.	1	1			1	+ 64			+ 16		
******	- 10	- 45	* /55	+ 135	- 45	- 16		÷ 445	377	+ 303	- 178	<del>* 77</del>	<u> </u>	+ 303	- 377	<i>- 437</i>	8 Rec	luced L L + ImpComp.	.xD(CF) 6	<u> </u>	- 19	• /52	- 181	<u> - 181</u>	- 52	- 19		- 491	<u> </u>	- 333	- 196	÷ 85	- 196	- 333	- 4/5	- 481
. 16	1 14	1 84	, ,				1 50	<b> </b>		,			<u> </u>					vio= Line 4 Line   (Comp.) o . Sidewalk-Tension	Line / (Ten.)		. 320															
T 10	T 14	+ <u>                                    </u>	+ 4	- 4	+ 11	+ 14	+ 10	- 13	11	_ A	+ 1		+ 1		<u> </u>	, 13		. Sidewalk-lension . Sidewalk-Comp.		+ 18	+ 15	+ 12	+ 6	+ 6		+ 15	+ 18			÷ 8	+ 1		+ 1		+ 12	
+ 1754	+ 1459					+ 1459	+ 1754	~ 1376	- 1106	848	_ 306	- 120	- 305	- 8/8	- II	1312	12 0:	ect Design Stress		. 1012	, JEGE	1022				, 1505	1012									
							7 7,04	- 15/0	- 1700			- 160	- 520	- 040	- 1100	7/3/2		erse Design Stress		+ 1913	+ 1090	+ 1233	+ 495	+ 495	+ 1233	+ 1030	+ 1913	- 149/	+ 1217	<del>- 938</del>	<i>→ 44</i> 5	+ 209	- 445	- 938	- 1217	÷ 1427
								,									14	croc bopign on coo									· · · · · · · · · · · · · · · · · · ·									
						.,											-15																-			
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1																			Hales out				:				,				,					
	44.	الم الموادية	43	43	4 4 . 1						3	3		<u> </u>			<del>   </del>	SECTION	for Tensio	11 1			1,			`										
The state of the s	1	4x4x ½	4X4X 8	4x4x 3 24x 3	4x4x <del>2</del>	4x4x ½	4x4x 2	4x4x ğ	4x4x ½	4x4x 7/16	4x4x #	4x4x 8	4x4x 8	4x4x 7/16	4x4x ½	4x4x 3	a	Flange Angles		4x4x 3/4	4x4x <sup>3</sup> / <sub>4</sub>	4x4x 3	4x4x }	4x4x 💈	4x4x 3	4x4x 3	4x4x 3	4x4x \$	4x4x 3	4x4x ±	4x4x 🕺	4x4x 3	4x4x ₹	4x4x ½	Ax4x §	4x4x §
24x \frac{5}{8} 22x \frac{1}{2}**)		24x <del>§</del> *) 23x 7/16**)	24% 8	24X 8	24X *	29X 2	24x 8	24x //16	24X 11/16	24x 9/16	24x #	24x g	24 x #	24x 9/16	24x 11/16	24x 7/16		I st Web Plate	3	24x \$	24x ½	24x ₹	24x 🖁	24× 3	24x 🖁	24x ½	24x \$	24x ½	24x 11/16	24x 9/16	24x 3	24x 3	24x 3 2	4x 9/16 2	24x 11/16	24x ½
24x \$	24× 1	1/252 1/10-1	25x 3 /	234 8 7	Z3X 1/10**	24V L	24x 5	244 7/16	23X //16+1	23X 5 T	23X 8++)	∠3x ह**)	23X #**/	23x 8**)	23x //16**	<b>.</b> .	11 1	Cover Plates	2	22x 9/16**)		23x 7/16**	) 23x ( 3+*)	23x =**)	23x 7/16**				23x ±**)	23x 7/16**)	23x <u>3</u> **)	23x #**)	23x **) 2	3x 7/16**) 2	?3x ***)	
- 570-8	27A 2					24x 2	24x g	24X 1/16	<u> </u>							24x 7/16	g	2 nd Web Plate	<u></u>	24 x 💈	24x ½					24x ½	24x \$	24x ½								24x \$
												,		<del>                                     </del>	<del>                                     </del>		#						+	<del> </del>	1	+										
																									<del> </del>							· · · · · · · · · · · · · · · · · · ·				
															·												<u> </u>									
								342	294	274,5	<i>2</i> 55	<i>2</i> 55	255	274.5	294	342	25 Le	ength	In:									342	294	274.5	255	<i>2</i> 55	255	274.5	294	342
·								7.59	7.59			7.70						n. Radius of Gyratio	n //7.									7.55	7.68	7.66	7.70	7.70	7,70	7.66		7.55
		24,000	18,000	18,000	24.000	24,000		19,060			14,720	14,720	14.720	19,400	19,310	19,060	27 A	lowable Stress	Lbs./5q. ln.	24,000	24,000	24,000	18,000	18,000	24,000	24,000	i	19,050		19,410	14,720		14,720	3	19,320	
87.00		56.38						73,44				39.19						tual Gross Area	5q. ln.	95.26	80.26	63.14		39,19	63.14	80.26	95, <i>26</i>	79.44	64.44	53,38	39.19	39.19	39.19		64.44	
73:50	61.75	1	1	1	46.88	1	73,50	/73,44	/57,483				/3/.88		/57 (83		29 Ne		Sq.ln.	79.51	66.51	1	32,44		51.64	1	79.51			48.17	31.88	31.88				79.44
23,870	23,630	24,030	13,950	13,950	24,030	23,630	23,870	18,730	19,140	19,000	12,410	5,640	12,410	19,000	19,140	17,870		tual Unit Stress	Lbs./5q. ln.	24,070	23,980	23,870	15,250	15,250	23,870	23,980	24,070	18,860	19,350	19,470	13,960	6,550	13,960	19,470	19,350	17,960
1 3	<u> </u>	3	<u> </u>	- C	<u> </u>	5	5	<u> </u>	S	<u> </u>	<i>C</i>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	\$	31 Ma	iterial	· · · · · · · · · · · · · · · · · · ·	S	S	S	c	<u> </u>	S	S	5	S	S	<u> </u>	C	<i>c</i>	<u> </u>		<u> </u>	3
	1		1	1		L.			<u> </u>							```									. €											

PART 3

All dead and live load stresses
are in kips
Line 29, - Net area for tension or
effective gross area for compression.





For truss dimensions see Framing Plan, 5h. 21

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R - 17.5

> STRESS SHEET UNIT 4 NORTH AND SOUTH TRUSSES

CUYAHOGA COUNTY CLEVELAND

SCALE None

MADE D.M.E. DATE 5-7-54

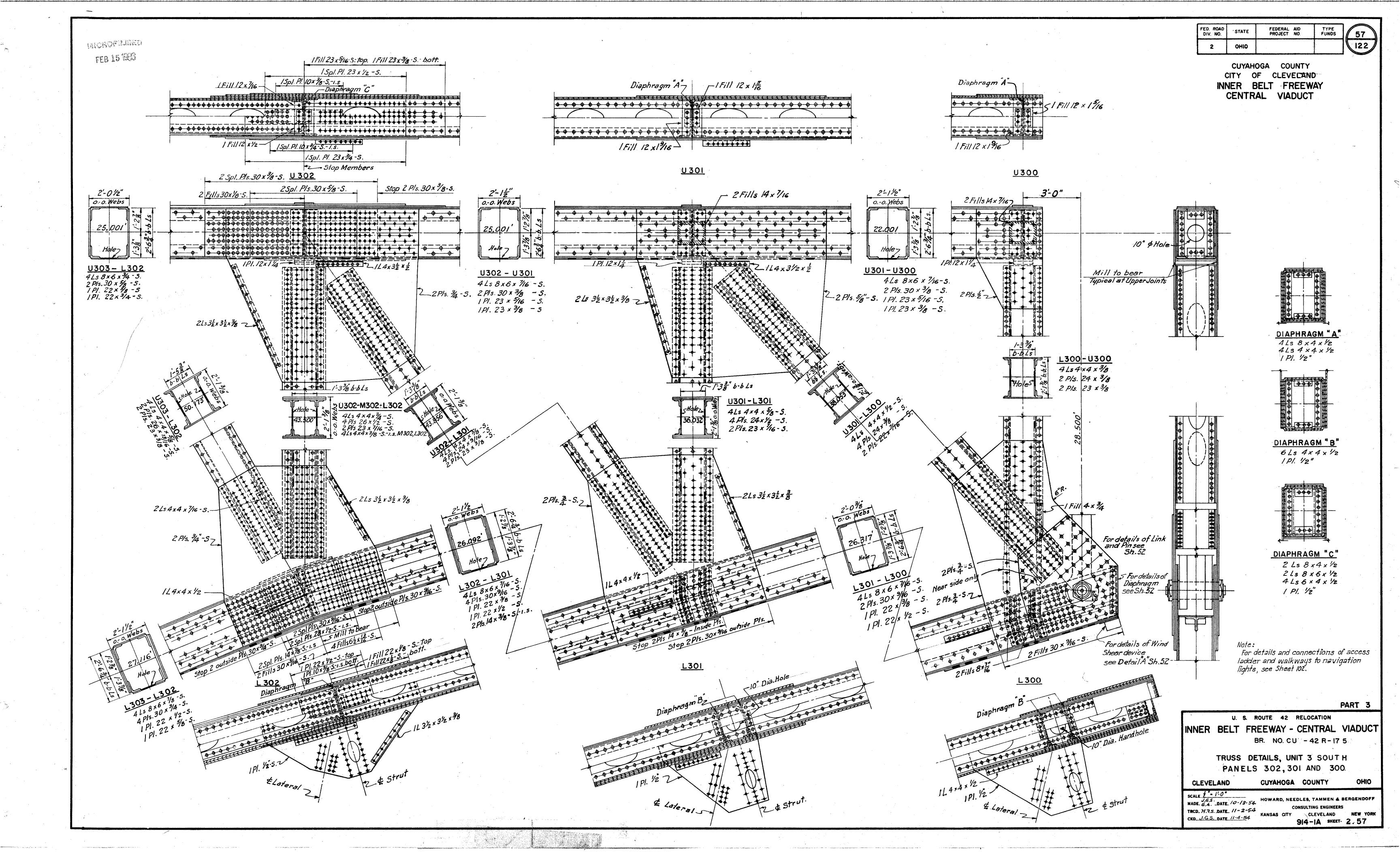
TRCD M.M. J. DATE 8-24-54

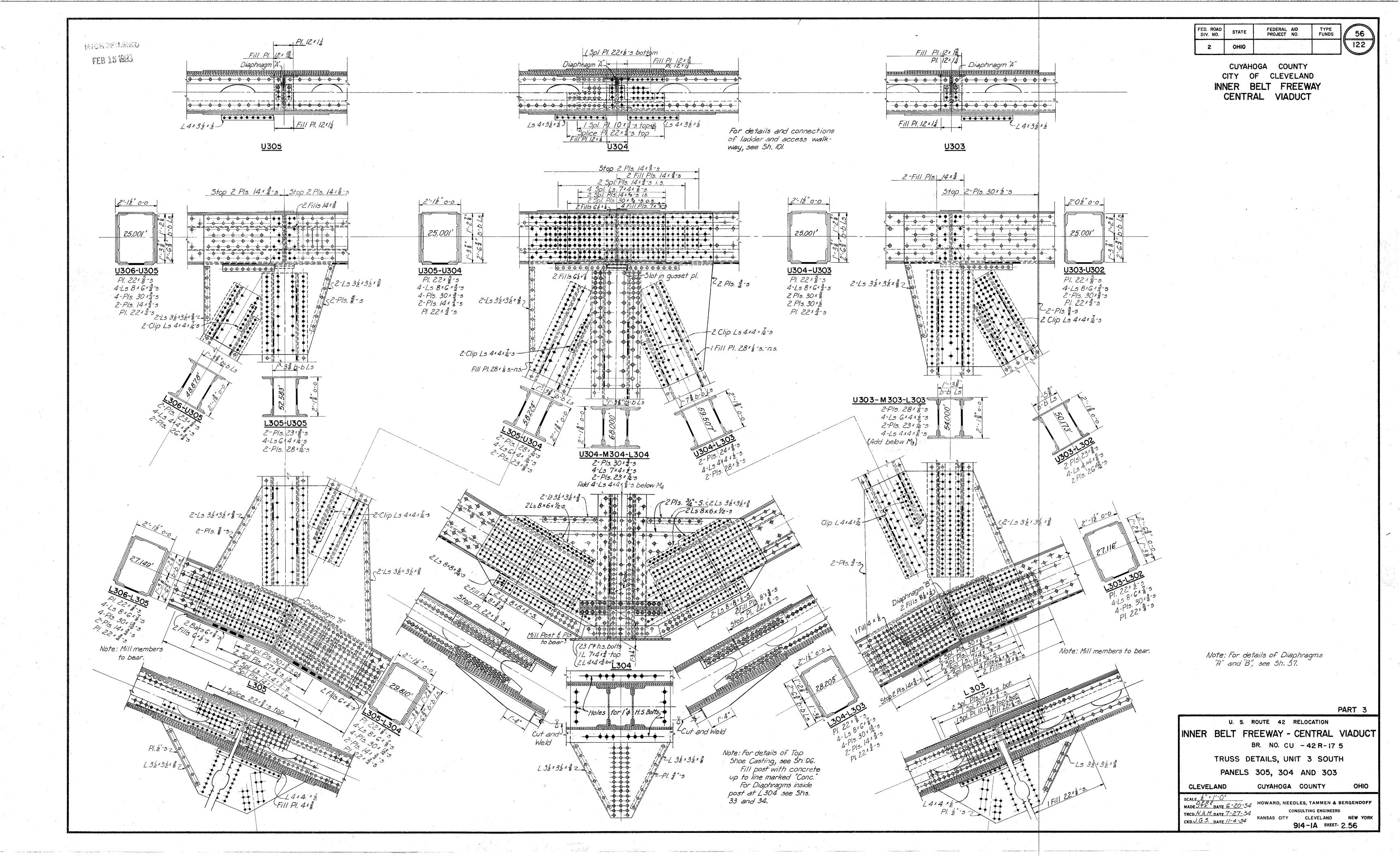
CKD. E.L. DATE 9-28-54

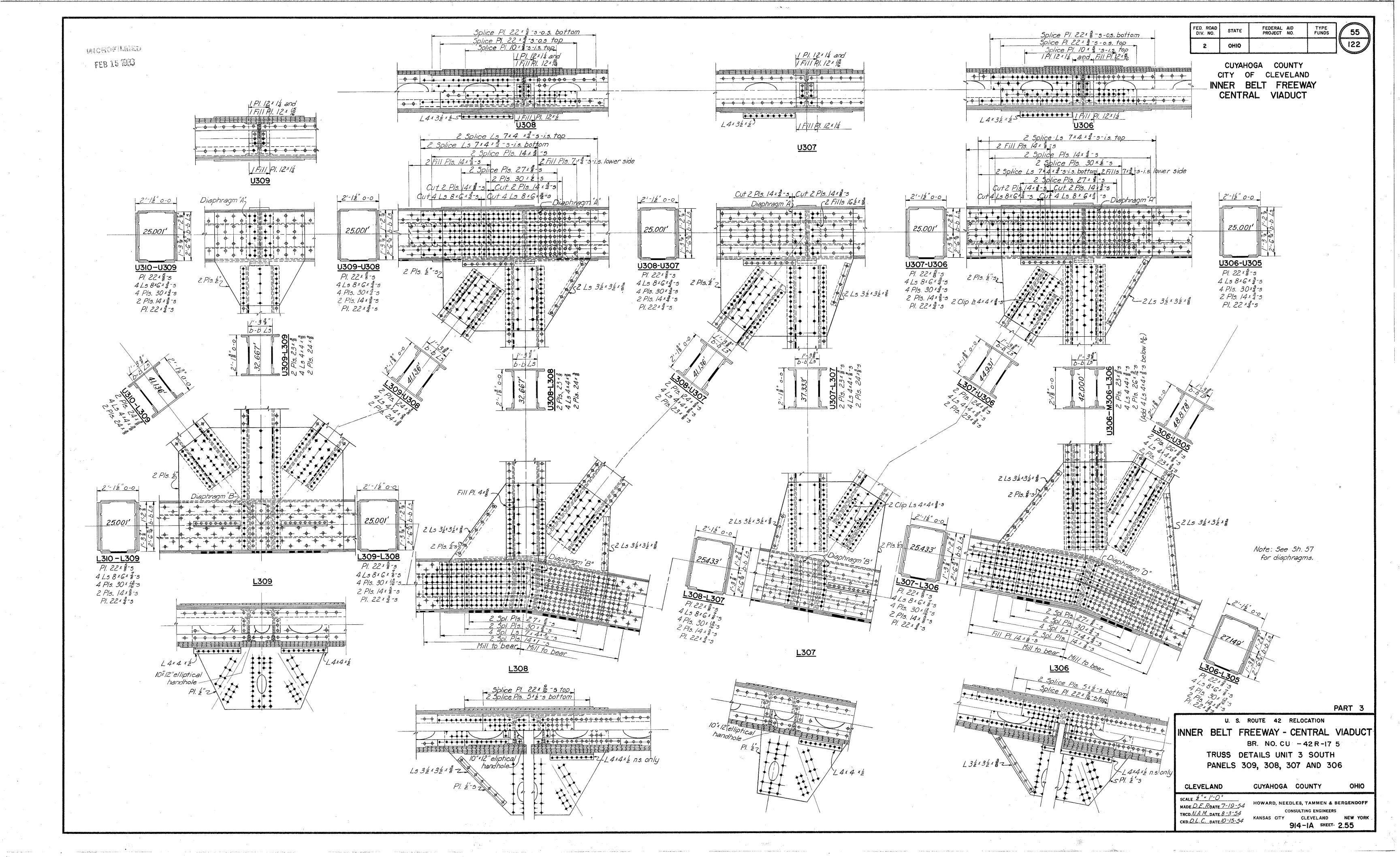
HOWARD, NEEDLES, TAMMEN & BERGENDOFF CONSULTING ENGINEERS

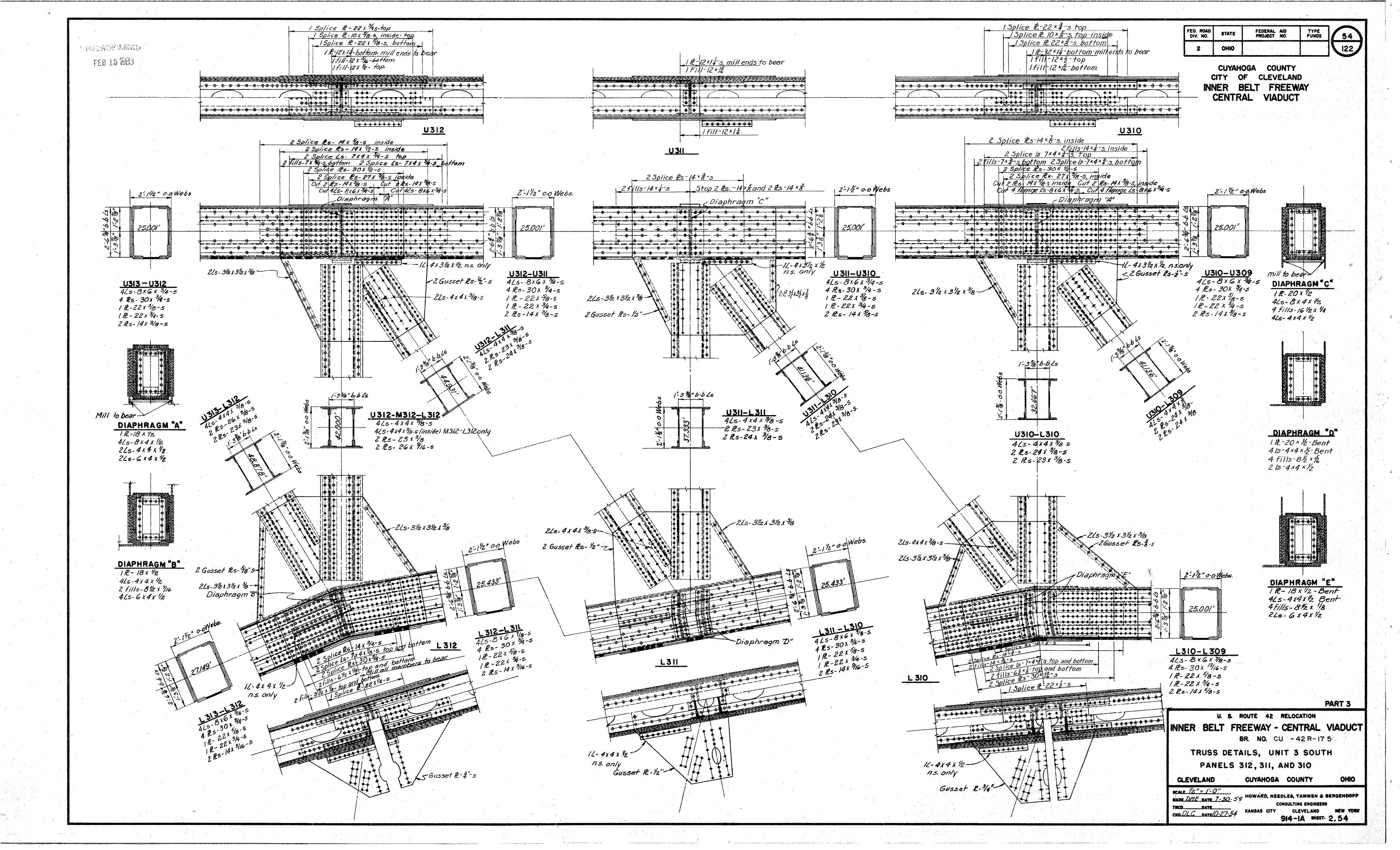
KANSAS CITY CLEVELAND NEW YORK 914-14 SHEET 2.58

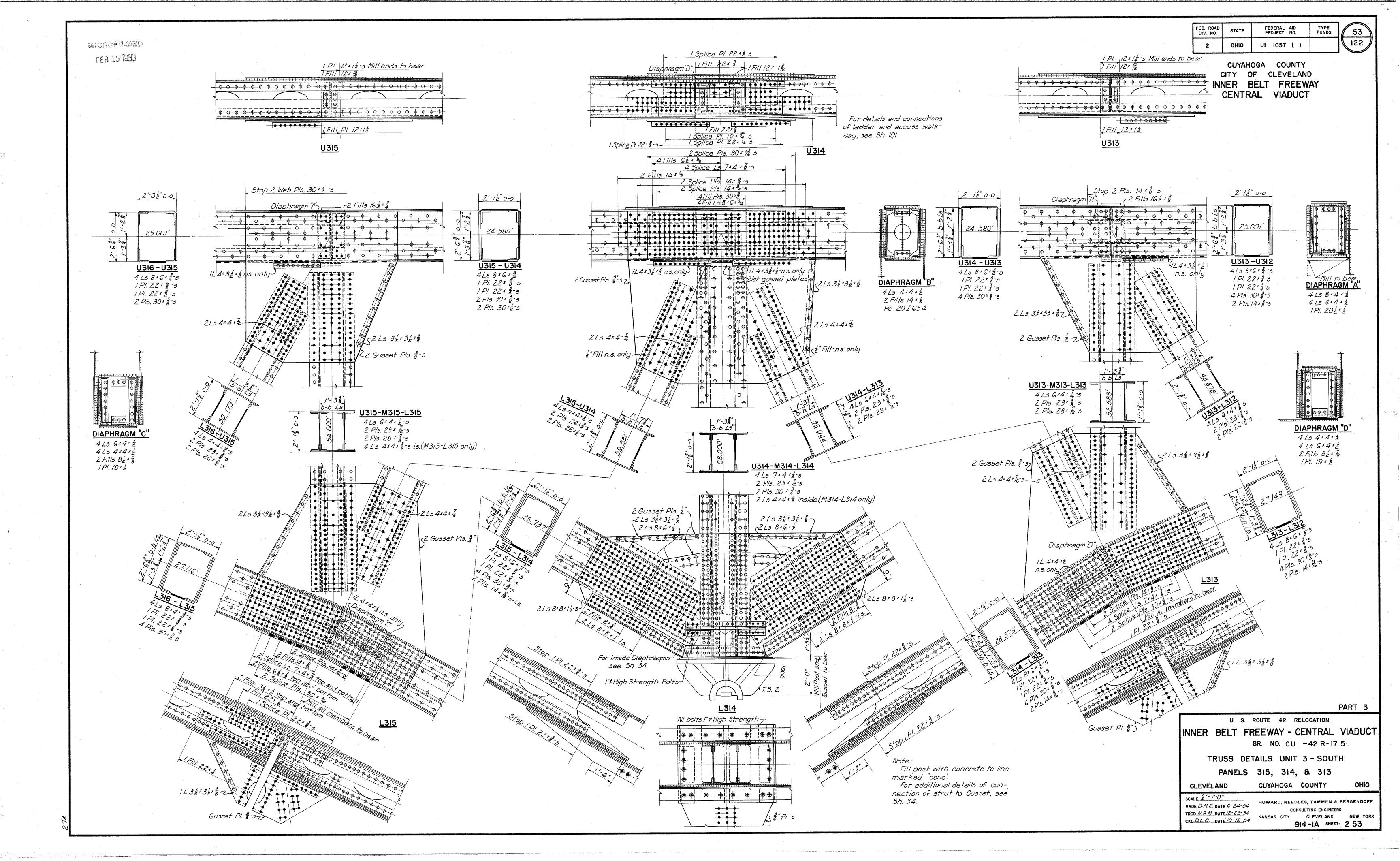
S = Special Steel C = Carbon Steel \*) = Handhole II"Wide \*\*)= Handhole IO"Wide

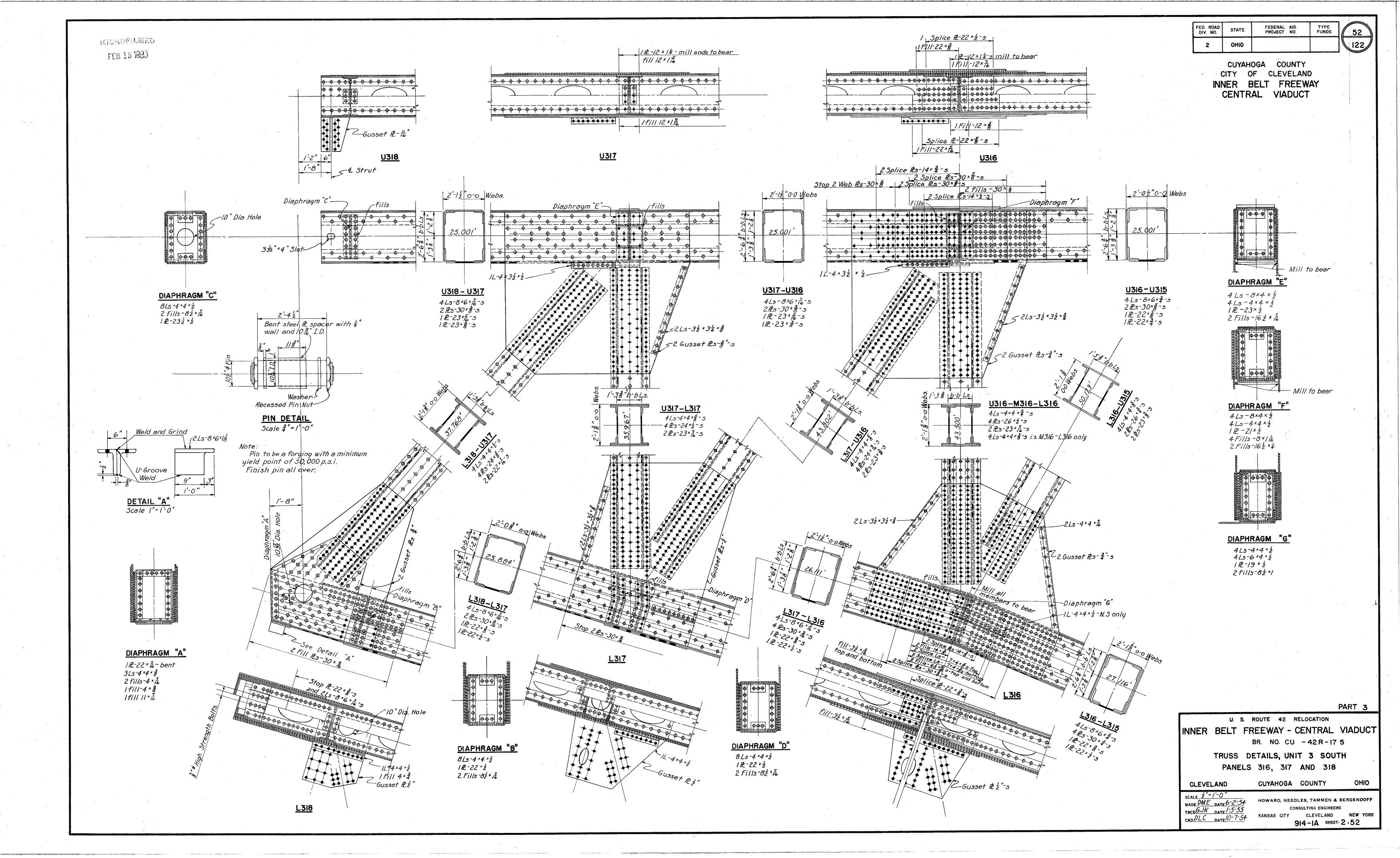


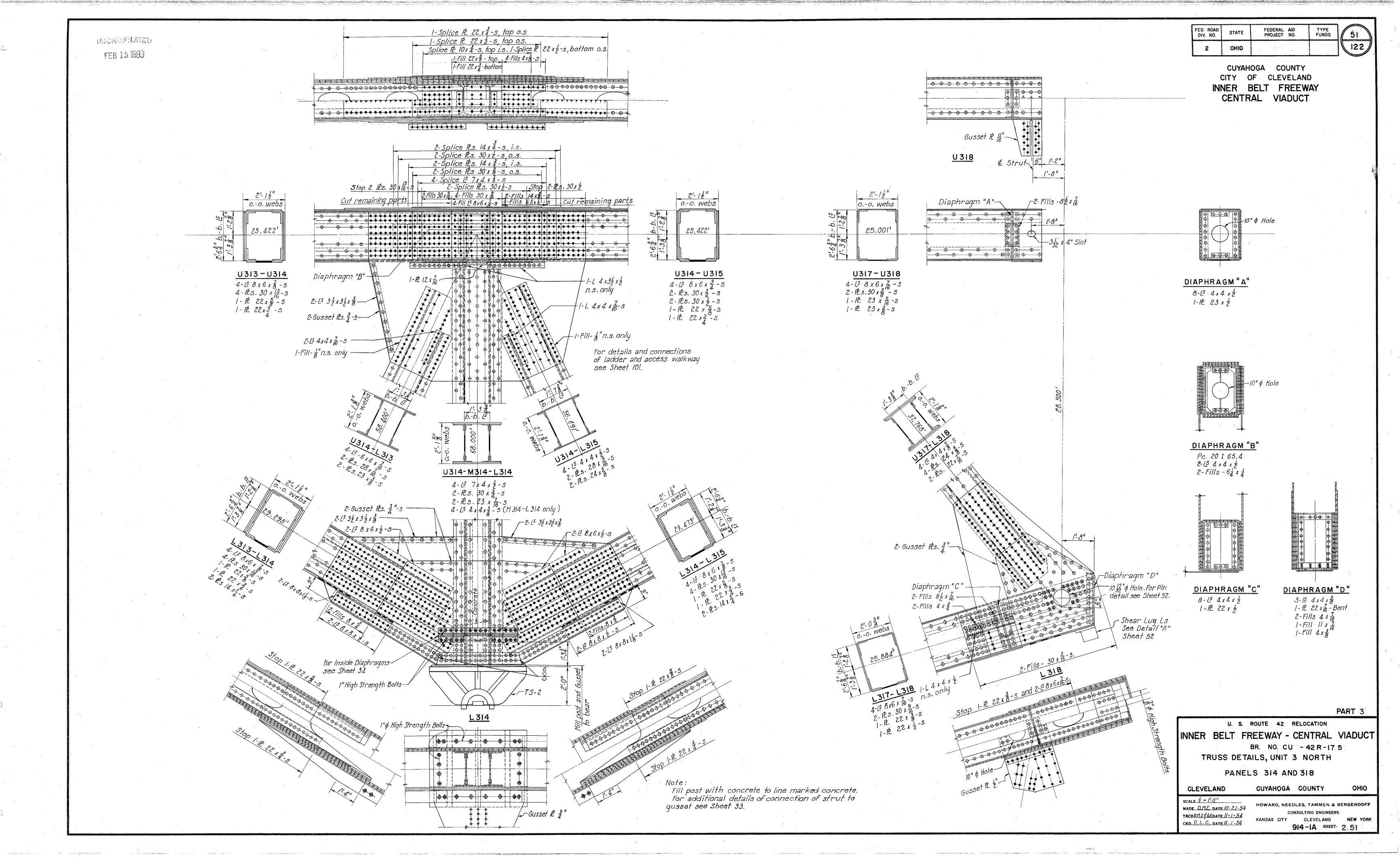


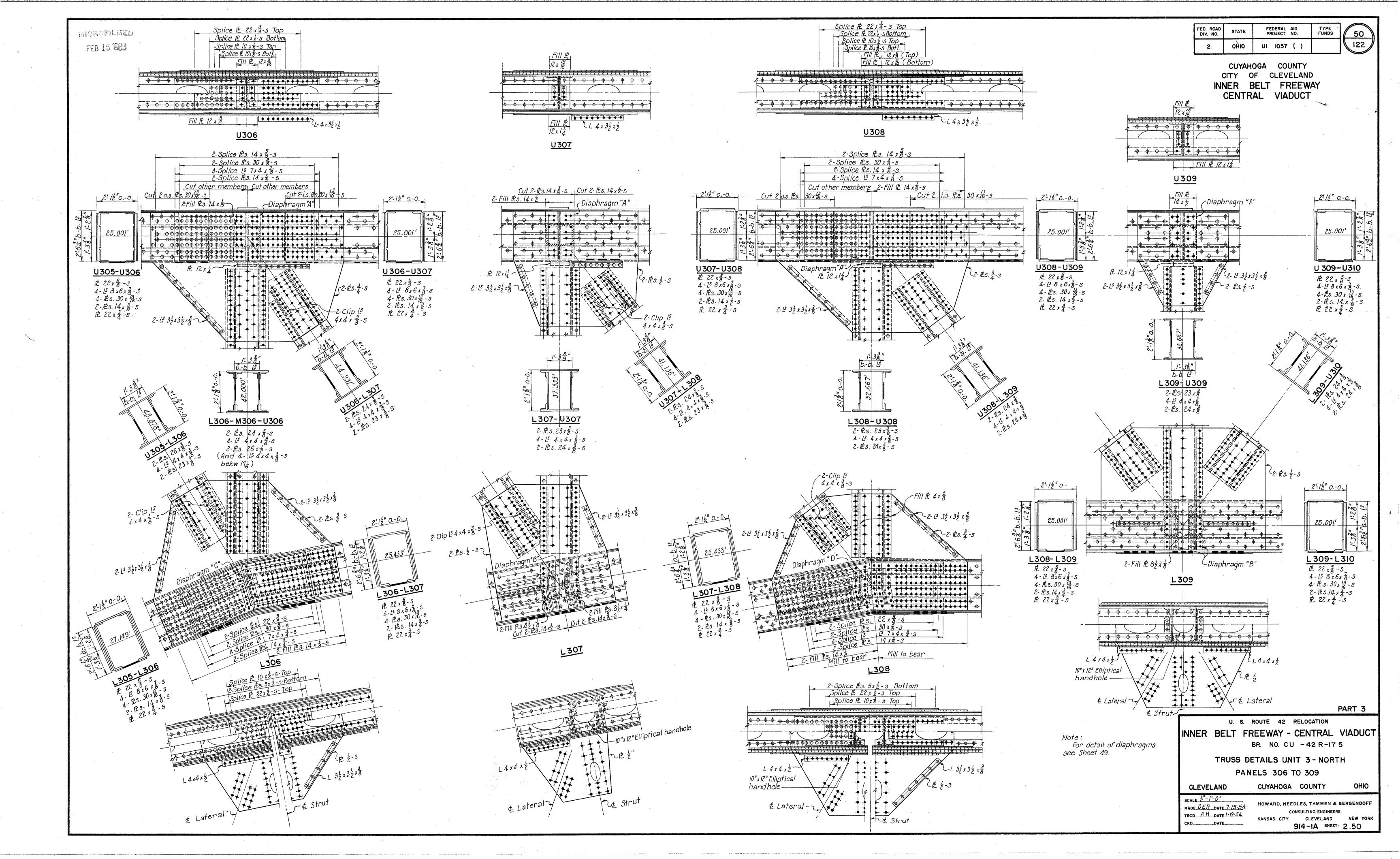


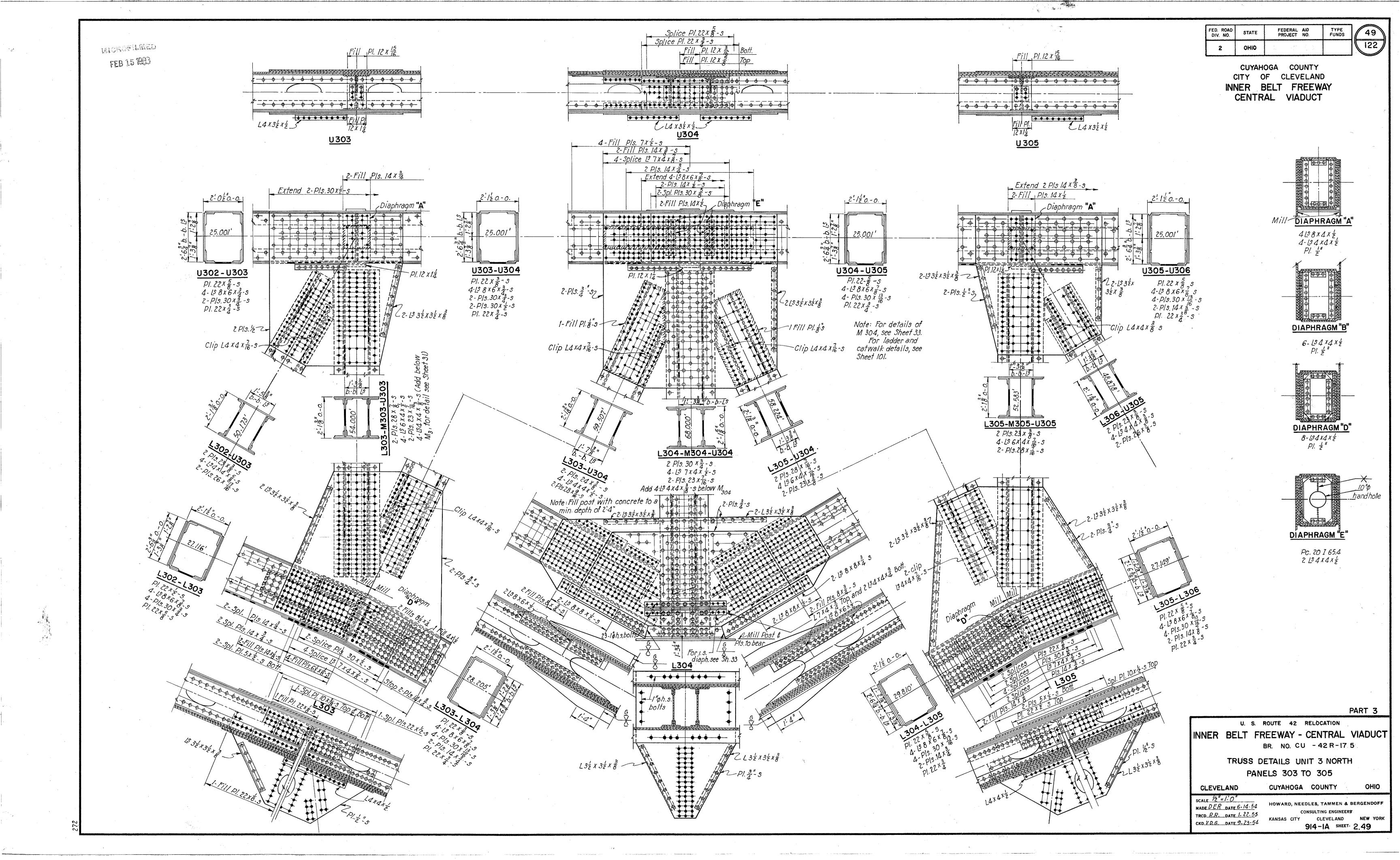












MICHOFINED

FEB 15 1933

FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. 122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

•															÷.																		CENIN	AL VIA	<u> </u>	
								CO	MPRESSI	ON CHO	ORD												· · · · · · · · · · · · · · · · · · ·			•	TENSION	CHOR	D							
MEMBE	<b>L</b> 300	L301 ·	L 302	L 303	L 304	L 305	4 306	L 307	L 308	L 309	L 310	L311	L312	L 313	L 314	L'315	L316	L 3/7	U 300	U301	U302   U303	U303	U304	U 305	U 306	U 307	U 308	U309	U310	U311	U 312	<i>U313</i>	U 314 U U 315	J315 U.	316 U317	<u>U 317</u>
MEMIDE	L30	L301 L302	1,303	L 304	L 30:	5 L 300	6 <u>L 30 7</u>	<u> </u>	L 30,9	L310	<u>L311</u>	L312	4313	1 <u>L314</u>	L315	4.3/0	L 31)	/\L3/8	<u> 4301</u>				VOC D	4506	0,507	J. V.200	4303	4510		40,2						
Dead Load	- 1016	- 1850	- 25 <b>5</b> 9	- 3088	- 3263	- 3097	- 2951	- 2770	<i>- 2741</i>	~ 2691	- 2680	- 2831	- 2959	- 2977	- 2994	- 2440	- 1757	- 947		+ 965	+ 1772		+ 2852			+ 2741					+ 2783		+ 2249			
0.8 Dead Load	- 813	- 1480	- 2047	- 2470	- 2610	- 2478	- 2361	- 2216	- 2193	- 2153	- 2144	- 2265	- 2367	- 2382	+ 2395	- 1952	- 1406	- 758	<u> </u>	+ 772	+ 1418	+ 1886	+ 2282	+ 2322	+ 2179	+ 2193	+ 2080	+ 2080	+ 2/53	+ 2108	+ 2226	+ 2180	+ 1799	+ 1346	<del>- /32</del>	
Live Load + Imp Tension																	-			1 4		<u>`</u>	<u> </u>	* 2.4	<u> </u>	1		+ 2						* 1		-
Reduced L L + Imp Tension						+ /58	+ 326	+ 478	+ 607	+ 607	+ 478	+ 326	+ 158	<u> </u>				<u> </u>		+ 219	+ 382	+ 485	+ 625	+ 695	+ 709	+ 781	+ 772	+ 772	+ 768	+ 692	+ 666	+ 599	+ 464	+ 365	+ 209	-
ive Load + impCompression														<u> </u>		1							<u>њ</u> /.	<u> </u>			4.4	~	24		<del>-</del>					1-
Reduced L L + ImpCompression	- 230	~ 399	+ 526	- 616	- 630	- 679	- 707	- 721	~ 781	- 769	- 7 <i>03</i>	<i>~ 678</i>	- 650	- 604	- 590	- 504	- 381	- 220					- /145				- /622				- /321				<u>.</u>	
Reduced L.L.+ ImpTension x D (CF) <sup>e</sup>						+ 262	+ 540	+ 792	+ 1006	+ 1006	+ 792	+ 540	+ 262							<b>→ 363</b>	+ 633	+ 804	+ 1036				+ 1280						+ 769	+ 605	<u>+ 346</u>	
Reduced L.L.+ ImpCompr. x D (CF)e	- 381	- 661	- 872	-/1021	+11044	- 1125	- 1172	- 1196	- 1294	- / <b>127</b> 5	- 1165	- 1123	a 1077	- 1001	- 978	- <i>83</i> 5	÷ 631	- 365					- 240	- 532	- 779	~ 1006	+ 1031	- 1031	- 1006	- 779	- 532	- 240				<del></del>
Line 4 Line 6 Ratio= Line I (Compr.) or Line I (Tensio						+ 0.05		- 0.17	+ 0.22	· · · · · · · · · · · · · · · · · · ·	- 0.18	- 0.12	- 0.05							1.1.	i l	4.	≈ 0.Q5	- 0.11	- 0.17	÷ 0.22	- 0.24	- 0.24	⇒ 0.23	+ 0.18	- 0.12	+ 0.05		<u> </u>	<u> </u>	1
L Sidewalk - Tension	,,					+ 8			+ 31	1		1	+ 8							+ 11	+ 19	+ 26	+ 38	+ 48	+ 54	+ 62	+ 62	+ 62	+ 62	+ 54	+ 48	+ 38	+ 26	+ 19	+ 14	1
L L Sidewalk - Compression	- 11	<u> </u>	28	- 3/	- 35	- 42		- 55	- 62		<b>-</b> 55	- E	- 42	- 35	- 34	- 28	<u> </u>	- 11		1. 11							+ 32					/7	1 2	1	<u> </u>	1
	- 1205	- 2161	- 2947	- 3525		- 3645				·	- 3364		1	- 3418		- 2815	- 2057	- 1134		+ 1146	+ 2070	+ 2716	+ 3356	+ 3522	+ 3408	+ 3549	+ 3422	+ 3422	+ 3488	+ 3309	+ 3378	+ 3211	+ 2594	+ 1970	+ 1089	1
Direct Design Stress	- 1205	+ 2101	- 2,941	<u> </u>	- 3089	- 3045	- J362	3-0/					1		- 19.																					1
Reverse Design Stress		_							<del> </del>				<u> </u>													;						<u> </u>				<u> </u>
																										· · · · · · · · · · · · · · · · · · ·						<u> </u>	1			
Lud o		<u> </u>																														<u> </u>				
SECTION Holes Of								1													***************************************								1			<u> </u>				
		8x6x 7/16	9.6. 7	9.6. 7	0.6.7	QUEN Z	8x6x 3	8x6x 7	8x6x 7	BYEY Z	8x6x 7	Bx6v Z	8x6x ₹	8x6x 7	8x6x 7	8x6x 3	8x6x 7/16	8x6x 7/16	8×6×7/16	8×6× 7/16	8x6y 3	8×6× 3	8x6x 3	8x6x 3	8x6x 3	8x6x 3	8x6x 3	8x6x 3	8x6x 3	8×6× 3	8×6× }	8x6x 3	8x6x 3	8×6× ₹ 8	3×6× 7/10	38x6
Angles 2										1						30. 3	30: 0/16	30. 0/16	200 3/	30× 3	30x 5	30x 5	30x 3	30x ₹	30× 3	30x 3	30x 3	30x 3	30× ₹	30x 3	30x ½	30x 3	30x ₹	30x ₹ 3	30x ₹	3
J. Web Plate 4	30x 9/16			1 ''			6 30x 13/16			30x 13/16		30x 3	30x 3	30x ₹	30x 3	30x 3	30x 9/10	30x 9/10	22 × 5/16	30x 3 23x 5/16	22 5	22v 2	22v 5	22x §	22x \$	22x \$	22x \$		22x \$	22x \$	22x 5		22x 5			
c Top Plate 3	22x 🖁	22x 3	22x ½					22x \$	22x \$	22x ₹	22x \$	22X 8	22x 5	22x \$	22X #	22.4 8	22 (+)	22 4	237 3710	234 341	22 3**1	224 8	224 3**!	222 3**1	224 3**1	22× 3**1	22× 3++1	22x 3**	) 22× 3**)	22x 3**)	1 22x 3**	) 22x 3**)	22x 3**)	22x 3**)	23x =*)	23
Bottom Plate 2	22x ½*)		22x 3**)	22x +**)	22x 3**)	22x 3**)	22x =**1	22x 3**)	22x 3**)	22x 3**1	22x 2**)	22x 344)	22x #**/	20x 344)	22x 2+*)	22x 3-4)	22X 3*1	26x 27)	23X 8" /	23x A 7	22.7	22X 3 1	14x 3	LAX 3	11/2 3	11x 3	14x }	14x 3	14x 5	14x 3	14x 3	1==-	1			
I. Inside Web Plate 2		14x 3		14x \$	14x 3	14x 3	14x §	14X \$	14x \$				30x 3/4	14x 9/16 30x 3			30x 9/16				·····	30x ⅓	30x 3		30x ⅓							30x 3	30x 4			
g 2. Outside Web Plate 4		30x 9/16	30x 2	30x 13/16	30x 13/16	30x 13/16	5 30x 13/16	30x 13/16	30x 13/16	30x 13/16	30x 4	30x 7	30x 4	30x 7	30x #	30A Z	300 3710					30X 2	30x 4	302 4	302		<del> </del>		30.2			1				
n 2. Inside Web Plate 2												<u> </u>			<del></del>									<u> </u>								1				
								<del></del>		<del> </del>								710.50		1				<u> </u>											1	$\Box$
Length //1.	3/5.8"					325.8"		305.2"	300"	300"	305.2"	305.2"	325.8"	343"	344.8"	325.4"	313.3"	310.6"						<del>-</del>							+	1				
Min, Radius of Gyration /n.	10,61	10.45	10.90	10,60	10.60	10.60		10.68	10.68	10.68	10.86	10.86		10.8	10.8	10,86	10.90	10.61		<b>+ -</b> . <b>- - -</b>		n4 aa-	24 605	24 000	34 000	24 000	34 000	24 000	24 000	24 000	24 000	24.000	24 000	24 000	24 000	,
Allowable Stress Lbs./5q./		19,590		19,530				19,620	19,640					19,540		19,590	19,620		24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	160 0	24,000	162 61	152.01	1E2 E1	24,000	100 01	57 01	
Actual Gross Area Sq. /	71.22	115.47				187.17		183.67		183.67		174.42	174.42	174.42	174.42	144.01	104.97		57.91	57.91	100.01	130.01	163.01	1/3.5/	163.01	1/3.51	163.01	163.01	170.01	163.01	103.01	134.14	130.01	85. <b>6</b> 4	10 72	1
Net Area 5q.1	7. 67.85	115.47	154.42	187,17	187.17	187.17	183.67	183.67		183.67		4		174.42					III .	49.72					140.14	149.14	140.14 V774	140.14	7 140 . 14	140.14	140.14	7 2%		32 000		1
Actual Unit Stress Lbs./5g./	7. 17,760	18,700	19,090	18,830	19,710	19,470	19,500	18,880	19,320	19,023	19,327	19,700	19,980 6	0. 19,600	19,530	19,550	19,590	16,720		23,040	24, 170 °	24,330 6.	23,940	23,610	24,310 0.	23,790	24,410 0	24,410 6	23.870	23,610	1 24, 100 0	24,480 o.	23,235	23,000 2	<u> </u>	+
Material	9	S	S	S	S	S	s	ls	S	s	s	s	S	S	S	S	S	S	5	S	S	5	S	5	5	<u> </u>	3	1 5	1 8		<u> </u>					

COMPRESSION WEB MEMBERS	TENSION WEB MEMBERS
U304 U305 U307 L310 L312 L313 U300 U301 U307 U308 U309 U310 U307 U308 U309 U309 U310 U307 U308 U309 U309 U309 U309 U309 U309 U309 U309	ER
L305 L306 L308 U311 U3/3 U3/4 L300 L301 L301 L301 L301 L301 L301 L301	+ 1468 + 1416 + 1173 + 903 + 318 + 232 + 149 + 264 + 886 + 1134 + 1351 + 1390
207 30 - 20 00 114 230 - 30 - 301 - 302 - 303 -	+ 1174 + 1133 + 938 + 722 + 254 + 186 + 119 + 211 + 709 + 907 + 1081 + 1112
3 Live Load + ImpT.	
+ 338 + 356 + 285 + 285 + 356 + 338	
5 Live Load + Imp.+C	
- 250 - 235 - 259 - 269 - 239 - 249 - 45 - 264 - 241 - 195 - 47 - 192 - 271 - 313 - 235 - 281 - 351 - 390 - 323 - 365 - 369 - 313 - 365 - 350 - 386 - 227 - 273 - 261 - 303 - 241 - 252 6 Reduced L L + Imp.	
+ 290 + 290 + 333 + 333 + 283 + 295 + 295 + 335 + 335 + 292 + 333   + 333   + 333   + 333   + 283   + 295   + 335   + 335   + 335   + 292     + 318   + 253   + 263	
14 + 389 - 429 - 446 - 396 - 413 - 75 - 437 - 399 - 323 - 78 - 318 - 449 - 519 - 389 - 466 - 582 - 646 - 535 - 605 - 580 - 605 - 580 - 605 - 580 - 605 - 580 - 605 - 580 - 605	
- 1.265 - 3.64 - 10.95 - 3.20 - 3.12 - 1.325   - 1.586 - 0.48   - 0.64   - 0.23 - 0.19 - 3.47 - 0.995 - 0.42 - 0.31 - 0.50 - 0.35 - 4.81 - 1.09 - 0.24   - 0.31 - 0.50 - 0.42 - 0.31 - 0.50 - 0.42   - 0.31 - 0.50 - 0.42   - 0.48   - 0.48   - 0.64   - 0.48   - 0.64   - 0.48   - 0.64   - 0.48   - 0.64   - 0.48	
20   19   16   16   19   20   1   13   12   13   14   16   16   17   18   14   16   17   18   18   19   19   19   19   19   19	
- 648 - 486 - 466 - 533 - 506 - 607 - 146 + 1434 + 508 - 589 - 181 - 531 - 1505 - 1631 - 1533 - 1533 - 1505 - 1631 - 1533	
+ 151 + 529 + 464 + 414 + 516 + 177 + 46 + 164 + 303 + 317 + 46 + 414 + 516 + 177	
SECTION	Holes Out for Tension
5x4x 7/16 4x4x 3	2 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½ 4x4x ½
6x4x 7/16 4x4x \$	⊕ 24x \(\frac{2}{8}\) 24x 9/16 26x 13/16 28x \(\frac{1}{8}\) 24x \(\frac{2}{8}\) 24x \(\frac{2}{8}\) 24x \(\frac{2}{8}\) 24x \(\frac{2}{8}\) 24x \(\frac{2}{8}\) 24x \(\frac{2}{8}\) 26x 13/16 24x 9/16 24x \(\frac{2}{8}\)
28x 7/16 = 20x 8   24x	2 22x 7/16**) 23x 3**) 23x 3**) 24x 3**) 24x 3**) 24x 3**) 24x 3**) 24x 3**) 24x 3**) 23x 3**) 23x 3**) 23x 3**) 23x 3**) 23x 3**)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 24.5
26x ½ 26x 26x 26x 26x 26x 26x 26x 26x 26x 26x	3 24x \( \frac{2}{8} \) 24x 9/16 \\ 24x \( \frac{2}{8} \) 3
698.7" 586.5" 493.6" 493.6" 586.5" 698.7" 342" 432.4" 448" 392" 392" 392" 522" 522" 648" 648" 631" 631" 504" 504" 504" 631" 816" 816" 816" 648" 522" 522" 448" 432.4" 48" 432.4" 25 Length	
8.61 /.93 /.70 /.70 /.70 /.93 8.61 /.70 /.70 /.93 8.61 /.70 /.70 /.93 8.61 /.70 /.70 /.93 8.61 /.70 /.70 /.93	10n 1/1.
16,970 17,480 18,110 18,110 17,480 16,970 14,510 18,490 18,440 18,810 17,910 17	
50.97 40.69 39.19 40.69 50.97 39.19 77.82 39.19	Sq. In.     85.50     82.19     70.44     53.50     39.19     39.94     39.94     39.19     53.50     70.44     82.19     85.50       Sq. In.     72.25     68.94     57.44     44.00     32.44     33.19     33.19     32.44     44.00     57.44     68.94     72.25
43 49 32 82 37 33 37 38 43 49 31 33 77 82 31 33 31 31 32 82 43 49 31 33 77 82 31 33 31 31	Lbs./Sq.In. 24,200 28 24,170 23,900 23,840 23,970 18,320 8 16,060 22,660 23,360 23,150 23,150 22,930
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2007 00 111 124.200 (0.124.17010, 125.200   CD,040 (0.1 105.200   CD,040 (0.1 105.200   CD,040 (0.1 105.200
43.49 32.82 31.33	S S S S S S S S S S S

\*) Handhole || I" Wide

\*\*) Handhole || IO" Wide

S= Special Steel

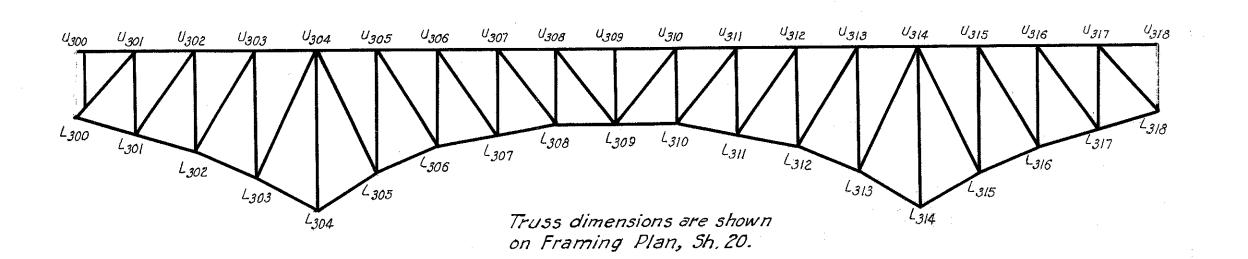
C= Carbon Steel

B 3 Holes Out of 24" Webs

4 Holes Out of 26"

And 28" Webs

All dead load and live load stresses are in kips.
Line 29,- Net area for tension or effective gross area for compression.



PART 3

OHIO

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42R-17 5

STRESS SHEET UNIT 3 SOUTH TRUSS

CUYAHOGA COUNTY CLEVELAND

HOWARD, NEEDLES, TAMMEN & BERGENDOFF CONSULTING ENGINEERS CLEVELAND NEW YORK
914-1A SHEET- 2.48

SCALE None

MADE H.W.L. DATE 5-3-54

TRCD 3.4 K DATE 8-31-54

CKD E.L. DATE 9-2-54

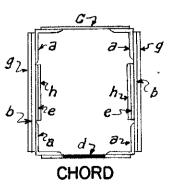
FEB 15 (44)

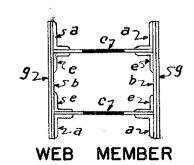
FEDERAL AID PROJECT NO. STATE 122 OHIO

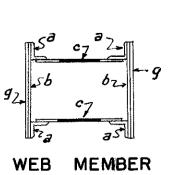
CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

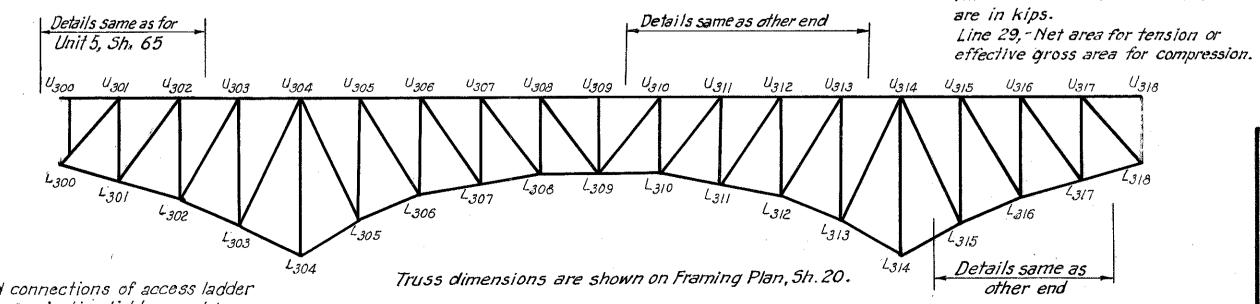
N													i														•							CENT	MAL VI	ADOCT	
Ш									COI	MPRESSI	ON CHO	RD																TENSION	CHOR	D		— · · · · · · · · · · · · · · · · · · ·					
	MEMBER	L 300 L'301	L301 1302	1302	1303	1304	L305 L306	L306 L307	1307	1308 1309	L309	L310	2311	L312	L3/3	L314	L315	L316 L317	L317	U300	U301	U302 U303	U303	U304 U305	U305 U30	U306 6 U307	U307 11308	U308 U309	U309	U310	U311	U312 U313	U313	U314 U315	U315	U316 U317	1317
I Dead Load		-1016	- 1851	-2560	-3086	-3260	-3//9	-3006	-2864	- 2884	-2912	-2912	-3070	-3/93	-3235	-3255	-26//	- 1888	-1021	2301	+ 965	+ 1773	+2359	+ 2 872	+2 956	5 + 2,817	+2884	+2.782	+ 2.782	+2.912	+ 2.864	+3.019	+2.941	+2.407	+1,808		
2 0.8 Dead Load		- 813	- 1481	-2048	- 2469	-2608	- 2495	-2405	- 2291	- 2,884 - 2,307	-2330	-2330	-2458	- 2554	- 2588	-2604	-2089	-1510	-817		+ 772	+1.418	+1 887	+2 298	+2 36	5 +2.254	+2.307	+2.226	+ 2.226	+2.330	+2.291	+2415	+2.353	+1.926	+1,446	+ 789	: .
3 Live Load + Imp Tens	sion				12,700			2,700		2,00,		<u> </u>	2,750	5.461 572 1.455 3 A.J	1,500	2,004	2,003	7,570	0.7			1.7	1.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	12,200	1 2,000		1,2,00.										
4 Reduced L.L. + Imp7	Tension						+ 158	+326	+478	+607	+607	+478	+326	+158							+ 219	+ 382	+ 485	+ 625	+ 695	5 + 721	+ 800	+ 803	+ 803	+ 812	+ 737	+723	+ 650	+ 505	+ 399	+229	
5 Live Load + ImpComp	pression																,									7											
6 Reduced L.L. + Imp Co		- 230	- 399	- 526	-6/6	- 630	-679	- 707	-733	- 800	- 8/3	-749	- 735	- 706	- 655	-640	-548	-416	-241					- 145	- 32	1 - 470	- 607	- 622	-622	- 607	-470	- 321	- 145				
7 Red. L.L. + Imp Tension	n× D(CF)e							+ 540	+ 792	+ 1.006	+1.006	+ 792	+540	+ 262		1 0,70	5.0	,,,,			+ 363	+633	+804	+1,036	+1,15	1 - 470 2 + 1,195 2 - 779	+1.326	- 622 +1,331 -1,031	+1.331	- 607 +1,346 -1,006 - 0.21	+1.221	+1,198	+1,077	+837	+661	+ 380	
8 Red.L.L.+ ImpCompr.	× D(CF)e	-381	-661	-871	-1,021	-1,044	-1,125	-1.172	-1,215	-1,326	-1,347	-1,242	+540 -1,218	-4170	-1.085	-1061	- 909	- 690	-399					- 240	- 53	2 - 779	-1,006	-1,031	-1,031	-1,006	- 779	- 532	- 240				,
8 Red.L.L.+ ImpCompr. 9 Ratio = Line 4 Ine I (Compr.) or 7 IO L.L.:Sidewalk - Tensi.	Line 6 Line I (Tens)						-0.05	-0.11	- 0.17	+ 1,006 - 1,326 - 0.21	-0.21	-0.16	-0.11	-0.05	<b>,</b>	7								- 0.05	- 0.1	1 - 0.17	- 0.21	- 0.22	- 0.22	- 0.21	- 0.16	- 0.11	- 0.05				
10 L.L.Sidewalk - Tensi	ion						+ 8	+ 16	+ 24	+ 31	+ 31	+24	+ 16	+8	****						+ //	+19	+ 26	+ 38	+48	+54	+62	+ 62	+62	+ 62	+54	+48	+38	+26	+ 19	+ //	
II L.L. Sidewalk - Comp.	oression	- 11	- 20		- 34		-42	- 49	-55	- <i>62</i> -3,695	- 62	- 55	- 49	-42	- 35	- 34	<i>– 28</i>	-20	-//					- 7	-16	- 24	-31	-32	+ 62 - 32	+ 62 -31	- 24	- 16	-7				
12 Direct Design Stress @+ @	)+ <i>@or</i> ②*3+@	-1,205	-2162	-2947	-3524	-3687	-3.662	-3,626	-356/	-3,695	-3,739	-3,627	-3,723	-3,766		-3699		-2,220			+ 1,146	+ 2,070	+2.717	+3,372	+3,565	5 +3.503	+3,695	+3,619	+3,619	+3,738	+3,566	+3,661	+3,468	+2,789	+2,126	+1,180	•
13 Reverse Design Stre	ess -														7										1								,				
14							3)																														
<i>15</i>																							At 1 Fr St. box bunk on St. From Add Will VVVI St Con CASS From				M PARE DAVID ABOUT THE ABO										
Section	Holes out for Tension		"																						:												
a Angles	2	8×6×7/16	8 x 6 x 7/16	8×6×7/8	8×6×7/8	8×6×7/8	8x6x78	8×6×7/8	8×6×7/8	8x6x7/9	8x6x7/8	8×6×7/8	8×6×7/8	8×6×7/8	8×6×7/8	8×6×7/8	8×6× 1/8	8×6×7/16	8x6x 7/16	8x6x7/16	8×6×1/16	6 8×6×3/4	8×6×3/4	8x6x1/8	8×6×7	8 8×6×7/8	8 x 6 x 7/2	8×6× 1/8	8×6×7/8	8×6×7/8	8×6× 1/2	8x6x 1/8	8x6x 7/8	8×6×3/4	8×6×3/4 30×3/4 22×5/8 22×3/4*	8×6×7/6 8	8×6× 7/1
b First Web Plate	4	30× 9/16	30×9/16	30×3/4	30x 13/16	30× 13/16	30× 13/16	30× 13/16	30x13/16	30x 13/16	30 × 13/16	30x 13/16	30×13/16	30 × 13/16	30× 13/16	30× 13/16	30× 3/4	30 × 9/16	30× 9/16	30 × 3/8	30×3/8	30x 3/a	30 x 3/4	30x 13/16	30×13/	6 30x 13/16	30x 13/16	30 x 13/16	30× 13/16	30x 13/16	30x 13/16	30x 13/16	30x 13/16	30 × 3/4	30×3/4	30 x 3/8	30× 3/8
c Top Plate	3	22×3/8	22 x 3/8	22×1/2	22×5/8	22 x 5/8	22×5/8	22× 5/8	22 x 5/8	22×5/8	22x 5/8	22×5/8	22x 5/8	22× 5/8	22 × 5/8	22× 7/8	22 x 1/2	22×3/8	22×3/8	23 × 5/16	23 x 5/16	22 x 5/8	22 x 5/8	22× 5/8	22×9/	22×5/8	22×5/8	22 x 5/8	22×5/8	22 x 5/8	22 x 5/8	22 x 5/8	22× 5/8	22×98	22×5/8	23 x 5/16	23 × 5/1
d Bottom Plate	2	22 * /2 * *	22×1/2**	22×5/8 *	22 × 3/4 *	22×3/4 *	22×3/4 *	22×3/4 *	22×34 *	22×3/4 *	22×3/4 *	22×3/4 *	22×3/4 *	22×3/4 *	22×3/4 ×	22×3/4 *	22×5/8 *	22×1/2**	22×1/2**	23×3/8* *	+ 23×3/8 + +	* 22×34 *	22×3/4 *	22×3/4 *	22×3/4	* 22×3/4 *	+ 22×34 ×	22×3/4 *	22×34 *	22×3/4 *	22×34 *	22×3/4 *	22×3/4 *	22×34 *	22×34*	23×3/8× × 2	.3×3/8*
e InsideWebPlate	2		14 x 3/8		14 x 3/4	14 ×3/4	14×7/8	14×3/4	14×5/8	14 x 3/4	14 x 3/4	14 x 5/8	14 × 3/4	14x 7/8	14 x 3/4	14 x 3/4		14 × 3/8							14 × 3/8	14 × 3/8	14 x 1/2	14 x 3/8	14 x 3/8	14×1/2	14 × 3/8	14 × 3/8					
f Inside Web Plate																			y.													, and					
g 2.Outside Web Plate	4		30 × 9/16	30×3/4	30 x 13/16	30×13/16	30 x 13/16	30x 13/16	30×13/16	30 × 13/16	30× 13/16	30×13/16	30×36	30×13/6	30×13/16	30x 13/16	30×3/4	30× 9/16					30×1/2	30 × 13/16	30x 13/	6 30× 13/16	30× 13/16	30 x 13/16	30× 13/16	30× 13/16	30× 13/16	30 x 13/16	30× 13/16	30×1/2			
h Inside Web Plate	2																										i.					,	/				
																																	12				
25 Length	In.	3/5.8"	3/3.3"	325.4"	353.7	357.7"	325.8"	305.2	305.2	300.0"	300.0"	305.2"	305.2"	325.8	357.7"	353.7"	325.4"	313.3"	315.8"								:							'n			
26 Min. Radius of Gyratic	ion In.	10.61	10.45	10.90	10.80	10.80	10.51	10.60	10.68	10.60	10.60	10.68	10.60	10.51	10.80	10.80	10.90	10.45	10.61																		
27 Allowable Stress	Lbs./Sq.In.	19,590	19,590	19,590	19,490	19,480	19,560	19,620	19,620	19,630	19,630	19,620	19,620	19,560	19,480	19,490	19,590	19,590	19,590	24,000	24,000	24,000 107.51	24,000	24,000	24,000	0 24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000 2	24,000
28 Actual Gross Area	Sq. In.	71.22	115.47	154.42	187.17	187.17	190.67	187.17	183.67	187.17	187.17	183.67	187.17	190.67	187-17	187-17	154.42	115.47	71.22	57.91	57.91	107.51	137.51	166:17	176.67	7 176.67	180.17	176.67	176.67	180.17	176.67	176.67	166.17	137.51	107.51	57.91	57.91
29 Net Area	5q. In.	67.85	115.47	154.42	187.17	187.17	190.67	187.17	183.67	187.17	187.17	183.67	187.17	190.67	3 187.17	187.17	154.42	115.47	67.85	49.72	49.72	92.14	118.14	142.80	151.80	151.80	154.80	151.80	151.80	154.80	\$ 151.80	151.80	142.80	3 118.14	92.14	49.72	49.72
25 Length 26 Min. Radius of Gyration 27 Allowable Stress 28 Actual Gross Area 29 Net Area 30 Actual Unit Stress-	Lbs./5q In.	17, 760	18,725	19,060	18,830	19,700	19,210	19,370	19,400	19,770	19,980	19,750	19,890	19,750	₹ <i>19,810</i>	19,760	19,590	19,230	18,080		23,100	22,470	23,000	23,610	23,48	0 23,080	23,870	23,840	23,840	24,150	23,500	24,120	3 24,290	23,610	24,000 107.51 92.14 23,070	23,730	
31 Material		5	5	5	5	5	5	5	5	5	5	5	5	5	5	S	5	5	.5	5	5	S	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5

						·							co	MPRES	SION	WEB	MEMBE	RS														m							TENSI	ON WE	B MEN				
U304 U305 U	U307	L310	L312 1	L313 L U314-	1300	U301	<i>U307</i>	U308	U309	U310	U302	M302 1/302	U303	M303 L303	U304-	M 304 L 304	U305 M305	M305 L305	U306	M306	U3/2 M3/2	M312	U313	M313	U314 M314	M314	U315 N	1315 L	1316 M M316 /	316 U3 1316 L	311 0	1317	MEMBER	L300 U30	D 430	71 L3C	203 4	1303 U3 11304 L	307 U3	08 L3C	09 L311	1 U314 12 L315	U315	11316 1317	317 L3/8
- 318 - 163		- 76	-154	- 306	- <i>8</i> 7 -	-1231		- 267	-128	-302	-1303	-1446		-1317		- 839	<del>- /</del>	-145	-346	-489	- 37/	-514	- //	-/55	- 742	-821	-1,198 -	1342 -	1327 - 1	469 -	83 -	1.260 1	Dead Load			1/7 +11	77 -	+895 + 2	248 +1	69 + 2	214 +27	18 +943	+1,201	+1,440 +	1,497
- 254 - <i>130</i>									-102	-242	-1.042	-1.157	- 938	-1.054	_		-/	-//6	-277	-39/	- 297	-411	- 9	-124	-594	-657	-958 -	1,074 -	1,062 -1	,175 - 1	56 -	1,008 2	0.8 Dead Load	+1,17	4 +1,1	134 + 9	142 +	+716 +1	198 +1	35 +1	71 +22	22 +754	+961	+1,152 +	1,198
																		,	, ,													3	Live Load + Imp Tension												
+ 338 + 356	+ 285	+ 285	+356	+338			+209	+165		+159					+184	+184	+212	+212	+ 185	+ 185	+/78	+178	+ 209	+209	+173	,ir				+1	99	4	Reduced L.L.+ImpTension	7 + 33	4 +3	13 +2	55 -	+192   +3	307 +:	245 +2	249 + 30	17 +196	+262	+323 -	349
																																5	Live Load + Imp Compr.												
<i>- 259  - 248  -</i>	- 279	- 270		- 260   -	- 45	- 264	- 241	-195	-47	-199	- 271	-313	-235	- 281	-351	-390	-323	-365	- 269	-313	-269	- 313	- 323	- 365	-352 +287 -583	-389	- 241  -	- 29/  -	- 280	325 -2	41 -	-275 6	Reduced L.L. + Imp Compr.					<u> </u>	223 - 7	<u> 230                                    </u>	24 -21	5			
+ 560 + 590 1			+ 590 -	+560			+346	+ 273		+263					+305	+305	+351	+351	+307	+307	+295	+ 295	+346	+346	+287		~			<b>+3</b>	30	7	Red. L.L. + Imp Tension × D(CF)	+55	53 + 5	119 +4	23 +	+ 318 + 3	509 + 4	106 + 4	$\frac{1}{3} + \frac{50}{3}$	19 + 325	+434	+ 535	5/8
- 429  - 411  -	-462	-447			-75 -	-437	<i>– 399</i>		- 78		-449	-519	- 389	- 466		-646	-535	- 605	- 446	- 519	- 446	- 519	- 535	-605	- 583	- 644	<i>– 399 -</i>	-482  -	-464  -	539 -3		456 8	Red.L.L.+ImpCompr. × D(CF)						370 -3	81   -3	371 - 35	6		*	<del></del>
- 1.06   -2.18   -			- 2.31 -					-0.618		-0.526		-			+ 0.265	-0.22	+212	<i>₹1.46</i>	- 0.535	- 0.38	-0.48	-0.35	-19.0	- /. 35	-0.24	.,.				-2	.40	9	Ratio = Line 4 Line 8	ton	<u> </u>		73		0.90 -1.	'. <i>3</i> 6 – /.	.05 - 0.7	7			
	+ 13			+ 17	,-	- /2	+ //		<del></del>	+10				-	+/3	+ /3	<del></del>	+ 16	+ 10	+10	+10	+10	+16	+16	+13					10 + 1	//	10	L.L. Sidewalk -Tension	+ 16	2 + 1	15 + 1	13 7	F 9 +	13 +	14 -	16 + 1.	5 + 9	+ /3	713	- 10
20 -19	- 10 E.C.E	-/6 F20		-20			-12		101	-/3	-14			-/4		-22	-/6	-18	-14	-/6	-14	_	-16		-20	-22	- 12	1.670		- 16 -		-13   //	L.L. Sidewalk - Compression  Direct Design Stress @D+@nD+®n	W - 171	12 -16	60 412	70 4	-1013 +5	122 4	14 - 1	14 - 1	= +1 000	+1100	+1702+	1702
- 703 - 560 - + 51 + 477 -	- 208 - 208	1 121	-548 -	_ 090   ·	-146		-456 +312	- 32 <i>@</i>	-781	T285	T1,505	71,692	-1339	7334	T/131	-1,338	- 352 +366	-739 + 153	-737	-926	-15/	- 946	1353	-747 +122	7,197	-1,323	-1,369 -	7,570	7,340 [7]	,730 -4 +2	75	1,477 12	B Parago Popios Strong	0,74	3 7,00	50 17,57	10 17	1,045	22 73	34 - 3	21 74	5 11,000	1,400	11,702 1	3176
+ 31   T477   1	T 330	+424	704	<del>+ /3</del>			T312							_		ļ	1 300	7733	<del></del>				7333	1,22		, , , ,				7 2	73	13	Reverse Design Stress							34	37		<del> </del>		
																	,				1									14 A		15	5								***************************************	. The second sec			
6×4×7/16 4×4×3/8	4×4×3/8	4×4×3/8	4x4 x 3/9 6	6x4×7/16 4	x4 x 3/0 4	1×4×3/1	4×4×3/8	4×4×3/a	4×4×3/a	4 x4 x 3/	4x4x30	4 4x4×3/	4 6x4x1/2	6x4x1/2	7x4x1/2	7x4x1/2	6×4×7/16	6x4×7/16	4x4x3/a	4×4×3/a	4×4×3/0	4x4x3/8	6x4x7/16	6x4x 7/16	7x4x1/2	7x4x1/2	6x4x1/2 6	5x4 x 1/2 4	1 x 4 x 3/4 4 x	4 x 3/4 4x4	×3/8 4	x4x3/4	a Outer Angles	2 4x4x	% 4x4	-x 5/8 4×4	x 5/a 4	4x4x1/2 4x4	4x3/9 4x	1×3/2 4×4	x3/8 4x4x	3/8 4×4×1/2	4×4×98	4x4x 5/8 4	x4 x 5/8
28 x 7/16 26 x 3/8 2	24 x 3/8	24 × 3/8	26 × 3/8 2	28×7/16 2	4 x 3/8	24×1/2	24 x 3/8	24×3/8	24 x 3/8	24 x 3/8	26 x 1/2	26 x 1/2	28 × 7/8	28× 1/8	30x3/4	30 × 3/4.	28 × 1/16	28x 7/16	26 x 1/2	26×1/2	26×1/2	26 x 1/2	28 × 7/16	28 × 7/16	30×3/4	30×3/4	28×1/8 2	28× 1/8 2	6×1/2 26	5x1/2 24x	3/8 2	24 x 1/2 >	b I. Web Plate	1 24x 5	8 24x	x 5/8 26x	x 13/16 2	28 × 9/16 24	1 x 3/8 24x	$x^{3/8}$ $24x$	$\sqrt{3/8}$ 24x 3/	% 28× %16	26x 3/16	24× 5/8 2	4× %
23×3/8 * 23×3/8 * 2	23×3/8 *	23×3/8 × × 2	23×3/8 * 2	23×%*** £	3×3/8 * 2	?3×7/6 ★	23x 3/8 *	23×36 ×	23×3/6+	* 23×¾ = 1	+ 23×1/16	* 23× 1/6	* 23×/16#)	+ 23×1/6° →	23×1/6 **	23×1/6 *	23×3/6 +	23×¾≈ <del>×</del>	24×% **	24×3/00 *	124×3/8 +	€ 24×¾ ×	23×3/8 *	+ 23×3/8 ×	* 23×1/6 *	23×716° *	23×416 * Z	23×1/6 + 2	3×1/16 * 23	×1/16 * * 23×	% × 23	3×1/6** C	a Outer Angles b I. Web Plate c Cover Plate	2 22x1/	6* 22x	$\frac{3}{8} * 23 \times 3$	1/8 * 2	$24x\frac{3}{8} * 23x$	·1/8 * 24;	3/8 * 24×	₹ 23× 3/2	3 * 24×3/8 *	23×3/8 *	22×3/8 * 2	2× 1/6*
															<u> </u>											1							·   d     S												
	·····											4×4×3/	8	4×4×36		4×4× 3/8				4×4×3/8		4x4x3/8	<u> </u>			4×4×3/8	4	1-x4×3/8	4,	x4 x 3/8		<u>;</u>	e Inner Angles	2								· .			
						24×1/2		1			76 x 1/2	26 x 1/2	,		<u> </u>		· · · · · · · · · · · · · · · · · · ·		<u> </u>	·									26×1/2 20	6x1/2		24 x 1/2 50	g 2. Web Plate	3 24×9	% 24x	5/0								24×5/8 2	4x5/8
	,,												-	***************************************	<u> </u>			<del> </del>															h E		,0  2 //	/8									
700.8" 586.5"	493.6"	493.6"	586.5*	700.8	342.	4324"	448.	392	392"	392	522.%	522"	648"	648"	816"	816"	631"	631"	504"	504"	504"	504"	631"	631"	816"	816	648"	648"	522" 5	522" 4	48" 4	432.4" 2.	5 Length //	7.											
8.61 7.93	7.70	7.70	7.93	8.6/	<i>7.70</i> L	7.63	7. <i>70</i>	1 7.70	7.70	7.70	7.92	7.75	8.47 0 /7,3/0 3 79.38	8.22	8.99	8.69	8.61	8.61	7.86	7.58	7.86	7.58 18,110 59.38 59.38 75,950	8.61	8.61 17,530	8.99	8.69	8.47	8.22	7.92	7.75 7 3.000 18.	70	7.63 26	Min. Radius of Gyration-	In.											
16,960 17,480	18,110	18,110	17,480	16,960	14,510	18,520	18,440	18,810	14,350 39.19	18,810		0 18,000	0 17,310	17,310	15,950	15,950	17,530	17,530	18,110	18,110	18,110	18,110	17,530	17,530	15,950	15,950 88.82	17,310	8.22 17,310 I			440 1.	8,520 2	7 Allowable Stress-Lbs./Sq./1	n. 24,00	00 24,0	000 24,0	000 2	:4,000 24,	,000 18,	000 18,0	000 24,00	00 24,000	24,000	24,000 2	1,000
50.97 40.69	39.19	39.19	40.69	50.97	39.19	81.14	39.19	39.19	39.19	39.19	85.14	96.58	79.38	90.82	77.38	88.82	50.97	50.97	47.94	59.38	47.94	59.38	50.97	50.97	77.38	88.82	79.38	90.82	85.14	96.58 3	9.19	81.14 28	8  <i>Actual Gross Area Sq.</i> //	ln. 88.9	94 87	7.44 70.	1.44	24,000 24,0 57.00 39 47.00 32	<i>9.19 39</i>	1.94 39	.94   39.1	9 57.00	70.44		38.94
43.49 32.82	31.33	31.33		43.49	31.33	81.14	31.33	31.33	31.33	31.33	85.14	96.58	3 79.38	90.82	77.38	88.82	43.49	43.49	41.27	59.38	41.27	59.38	43.49	43.49	77.38	88.82	79.38	90.82	85.14 9	96.58 31	1.33	81.14 29	9 Net Area Sq.1	n. 74.6	69 73	.44 57.	,44 (	47.00 32 22,190 22,	2.44 3:	5.19 33	3.19   32.4	14 47.00	57.44	73.44	4.69
	18,030	16,730		16,020	4,570	17,680	14,550	17,600	5,670	0 18,66	0 17,680	17,520	16,850	16,930	14,870	15,070	12,680	16,990	17,860	15,590	18,340	15,950	12,870	17,170	15,470	14,900	17,250	17,290	18,080 3 1	7,920 16,	,220 1	18,200 30	O Actual Unit Stress-Lbs./Sq.	In. 23,36	<i>50 22,</i>	110 64,0	200 2	72,190 22,	,260 /6,	780 18,0	080 23,00	23,150	24,500	23,150 2	<i>3,990</i>
5 5	5	5	5	S	C	5	5	5	C	5	5	5	5	<u> </u>	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	$\mathcal{S}$ .	5	5 3	Material	5	ع ا	5 5	<u>;                                    </u>	_5   5	<u>5</u>	<u> </u>	c 5	5	5	5	5









For details and connections of access ladder and walkways to navigation lights panel L300, see Sheet 102.

All dead and live load stresses

- LEGEND

  S Special Steel
  C Carbon Steel
  9 3Holes out of 24" Webs

\* 4 Holes out of 26" and 28" Webs
\* 10" Holes
\*\* /!" Holes

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R-17.5

STRESS SHEET UNIT 3

NORTH TRUSS

CUYAHOGA COUNTY CLEVELAND

SCALE NONE

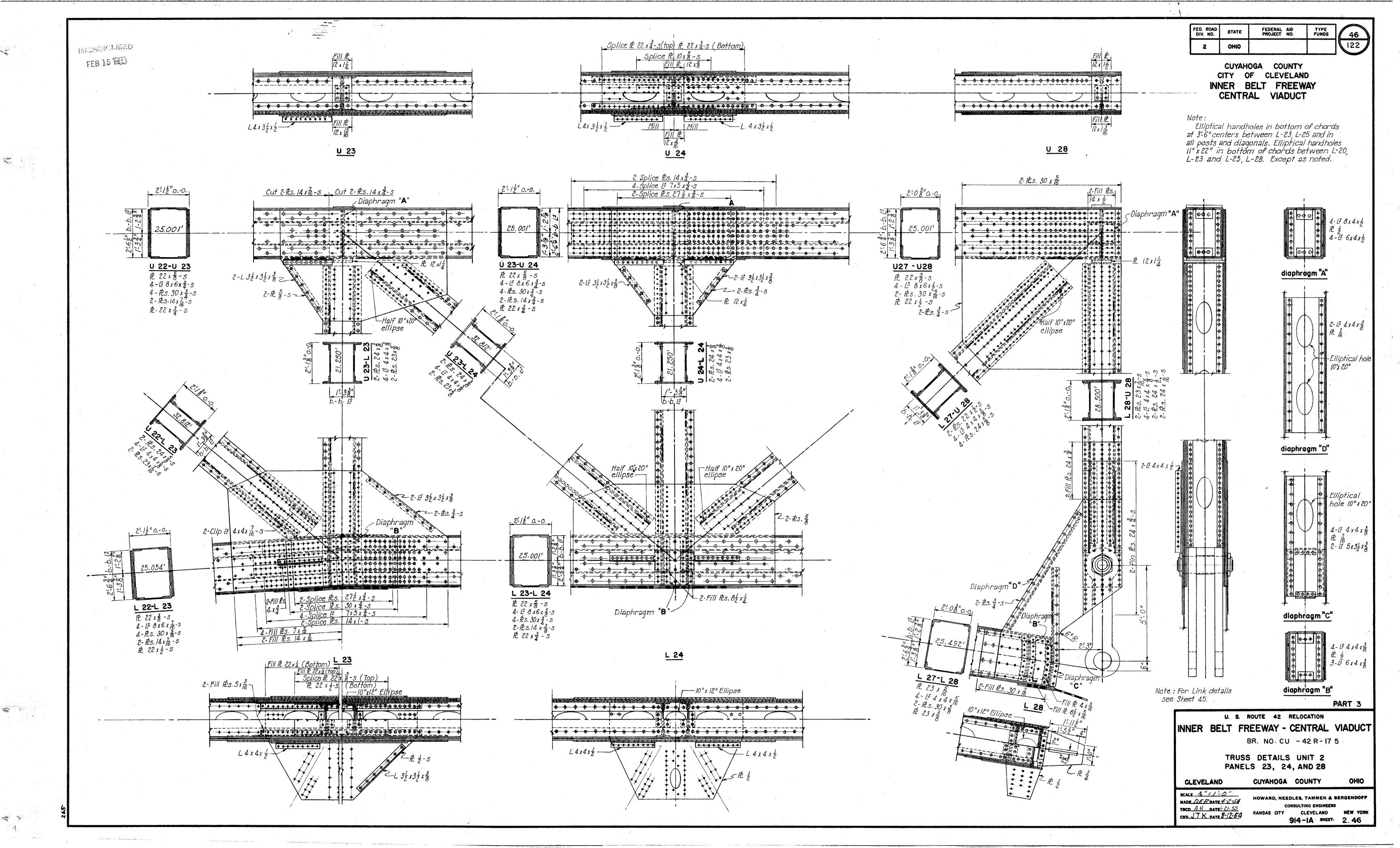
MADE H.W.L. DATE 4-30-54

G.J.K.

TRCD H.7.S. DATE 9-15-54 CKD EL DATE 8-17-54

HOWARD, NEEDLES, TAMMEN & BERGENDOFF CLEVELAND NEW YORK 914-1A SHEET 2.47

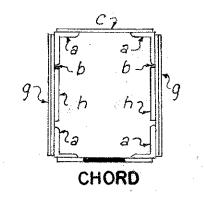
PART 3



MICROFILMED FEB 15 Wi

FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO. 5	TYPE FUNDS	44
2	оню			122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT



	K2	CZ	<u> </u>	Ţ .
92	ςb	cz	bζ	59
	Ita	1	23	J

WEB MEMBER

•				·				
						-		
					·	-		
								,
						·		
	i							
4x4x	4x4x \$	4x4x ½	4x4x 3	4x4x 3	4x4x 3	4x4x ½	4x4x }	4x4x }
24x ±	24x 11/16	24x 3/16	24x 3	24x 3	24x }	24× 9/16	24x 11/16	,
× 7/16**		23x 3**	23x 3**	23x ∄**	23x 3**	23x ₹**	23x 7/16**	23× 7/16**
x 7/16								24x 7/16
		:						
342"	294"	274.5"	255"	<i>2</i> 55"	<i>25</i> 5"	274.5"	294"	342"
7.57	7.70	7.68	7.70	7.70	7.70	7.68	7,70	7,57
19,060	19,330	19,410	14,720	14,720	14,720	19,410	19,330	19,060
74.82	62.82	51. <b>75</b>	39,19	39,19	39.19	51.75	62.82	74.82
74.82	61.27	46.35	31.88	31.88	31.88	46.35	61.27	74,82
19,120	18,900	19,160	13,000	5,950	13,000	19,160	18,900	18,220
	<del>  </del>			<del> </del>			<del></del>	

COMPRESSION CHORD

-2789

8x6x3

30x 3

22x \$

22x4\*\* 30x4

300" 300" 300"

122.25 164.76 173.51 173.51 164.76 122.25 74.50

÷135

*≥108* 

-280

-224

+ 37

-187

- 4

-0.132

- 49 -113

-190 -415

122,25 164.76 172,76 172,76 164,76 122,25 18,350 19,550 19,400 19,480 19,480 19,400 19,550 18,350

COMPRESSION WEB MEMBERS

*~280* 

+113

~187

-0.132

- 4

-415

-562 -224

+ 9 + 37

14x3 14x3 14x 7/16 14x1

10.82 10.59 10.59 10.82 10.42 10.61

+2609

- 651 - 493

8x6x<sup>2</sup> 8x6x<sup>2</sup>

22×4\*\* 22×2\*

30x <sup>3</sup>/<sub>4</sub> 30x 9/16

30x<sup>2</sup>/<sub>4</sub> 30x 9/16 30x 9/16 22x<sup>2</sup>/<sub>8</sub> 22x<sup>2</sup>/<sub>8</sub> 22x <sup>3</sup>/<sub>8</sub>

-702

-192

-318

+1888

-0.013

-937

*-239 -277* 

-1157 <u>∻1362</u>

÷396

- 8 - 11 - 13

-562 -750 - 890

22×2\*

*-1937* 

-1550

-2789

-2087 -2231 -2231

- 651 - 675 - 675

-1119

- 30 | - 32 | - 32 |

-3196 -3382 -3382

22x 🖥

22x3\*\*

30×3

-2609

30x∄

22×8

22x<sup>3</sup>\*\* 30x<sup>3</sup>

14x 7/16

300"

-702

-192

-0.013

*-888* 

19,630 19,620 19,640 19,630 19,630 19,640

-1937

- 22

22x ∄

22x ½\*

14x ½

30x 9/16

10.42

-750

-239

-1157

- 951

-282

- 13\_

-1431

*-2389* 

- 842 - 1550

- 272 | + 493 |

- 451

+1305

30x 9/16 22x 3

22× ½\*

PART 3

S = Special Steel
C = Carbon Steel
\* = !!" Hand Hole Out
\*\* = 10" Hand Hole Out

MEMBER

I Dead Load

2 08 Dead Load

3 Live Load + Imp.-Tension 4 Reduced L.L.+ Imp. Tension

5 Live Load + Imp. -Comp.

10 L L Sidewalk-Tension

11 LL Sidewalk-Comp.

12 Direct Design Stress

113 Reverse Design Stress

a. Flange Angles

b. Ist. Web Plate

c. Top Cover Plate

g. 2 nd. Web Plate

26 Min. Radius of Gyration

Lbs./Sq In.

Lbs/Sq.In.

MEMBER

Sq. In.

Sq./n.

27 Allowable Stress

28 Actual Gross Area

30 Actual Unit Stress

25 Length

29 Net Area

31 Material

I Dead Load

2 0.8 Dead Load

3 Live Load + Imp. +Tension

5 Live Load + Imp.-Comp. 6 Reduced L L + Imp.-Comp.

10 L L Sidewalk-Tension

II L.L. Sidewalk-Comp.

12 Direct Design Stress

13 Reverse Design Stress

a: Flange Angles

b. 1 St. Web. Plate c. Cover Plates

g. 2 nd. Web Plate

25 Length \*\*

26 Min. Radius of Gyration

27 Allowable Stress

28 Actual Gross Area

30 Actual Unit Stress

29 Net Area

31 Material

4 Reduced L L + Imp. +Tension

7 Reduced L L + IMP.-Ten. xD (CF)

8 Reduced L L + IMP.-Comp. xD (CF) e

9 Ratio = Line 4 Line 6 Line (Ten.)

h. Inside Web Plate

d. Bottom Cover Plate

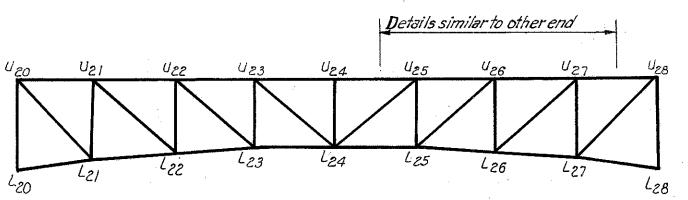
6 Reduced L L + Imp. +Comp.

7 Reduced L L + Imp. "Ten. XD (CF) e

8 Reduced L L + Imp. -Comp. xD (CF) e

Line 4 or Line 6

Ratio Line i (Comp.) or Line 6
Line I (Ten.)



TENSION CHORD

+2609

+2087

+ 30

8x6x 8

30x ⅔

22x ¾\*\*

30x 3

71.22 1117.22 1156.69 1156.69 1117.22

134.82

21,450 23,740 23,720 23,720 23,740 21,450

TENSION WEB MEMBERS

+ 235

-172

0.443

24,000 24,000

22x \$

+1941

+1553

+ 843

4x4x 5/16 8x6x 7/16 8x6x 7/16

3 23x 5/16 22x 3 22x 3

118,000

+1178

+ 633

+ 17

+1828

24,000

90.44

75.94

In.

5q. /n.

Sq.In.

Lbs. | Sq. In.

Lbs./Sq. In.

2 23x 3 \* 22x 1 \* 22x 1 \*

30x 9/16 30x 9/16

61,10 100.85

+ 960 + 707

+ 382 + 332 + 276

-1111

-18

0.009

+1524

24,000

76.94

64.19

24,070 23,720

30x 9/16

14x 7/16

+ 883

- 30

+1176

24,000

59,82 49,32

23,850

4x4x \( \frac{5}{8} \) 4x4x \( \frac{5}{8} \) 4x4x \( \frac{5}{8} \) 4x4x \( \frac{5}{8} \) 4x4x \( \frac{5}{8} \) 4x4x \( \frac{5}{8} \)

24x \$ 24x \$

18,000

39.19

32.44

14,550

0

0

+2609

+2087

+ 30 + 22

 $30x_{\frac{3}{4}}^{\frac{3}{4}}$  30x 9/16

30x3/ 30x 9/16

24,000 24,000

134.82 100.85

+ 188 + 188 + 707 + 1960

+ 104 - 104 - 30 - 11

+ 168 + 168 + 276 + 332 + 382

0.034

+ 11

+1176

24,000

59.82

49.32

23,850

*+*" 50 - 18

0.009

+ 14

+1524

24x ½

76.94

64.19

23,720

 $14x^{\frac{3}{8}}$   $14x^{\frac{3}{8}}$  14x 7/16

+ *23*5

+550 + 458 + 278 + 278 + 458 + 550 + 633

-172

0,443

18,000 -

32,44

14,550

39.19

+ 3 - 3

+ 472 + 472

+ 275 + 494 + 651 + 651 + 494 + **27**5 0

+ 456 + 819 + 1079 + 1079 + 819 + 456 0

+2394 +3196 +3196 +2394

+1941

÷1054

+1553 + 843 0

8x6x 8 8x6x 7/16 8x6x 7/16 4x4x 5/16

22x \$ 22x \$ 22x \$ 23x 5/16

22x3\*\* 22x ½\* 22x ½\* 23x 3\*

30x 9/16 30x 3

71.22

61.10

43.79

+1473

+1828

22x ½\*\*

24x \$

75, 94

Truss dimensions are shown on Framing Plan, Sh. 19. North and south trusses are alike.

All dead load and live load stresses are in kips. Line 29,- Net area for tension or effective gross area for compression.

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT

STRESS SHEET UNIT 2

NORTH AND SOUTH TRUSSES

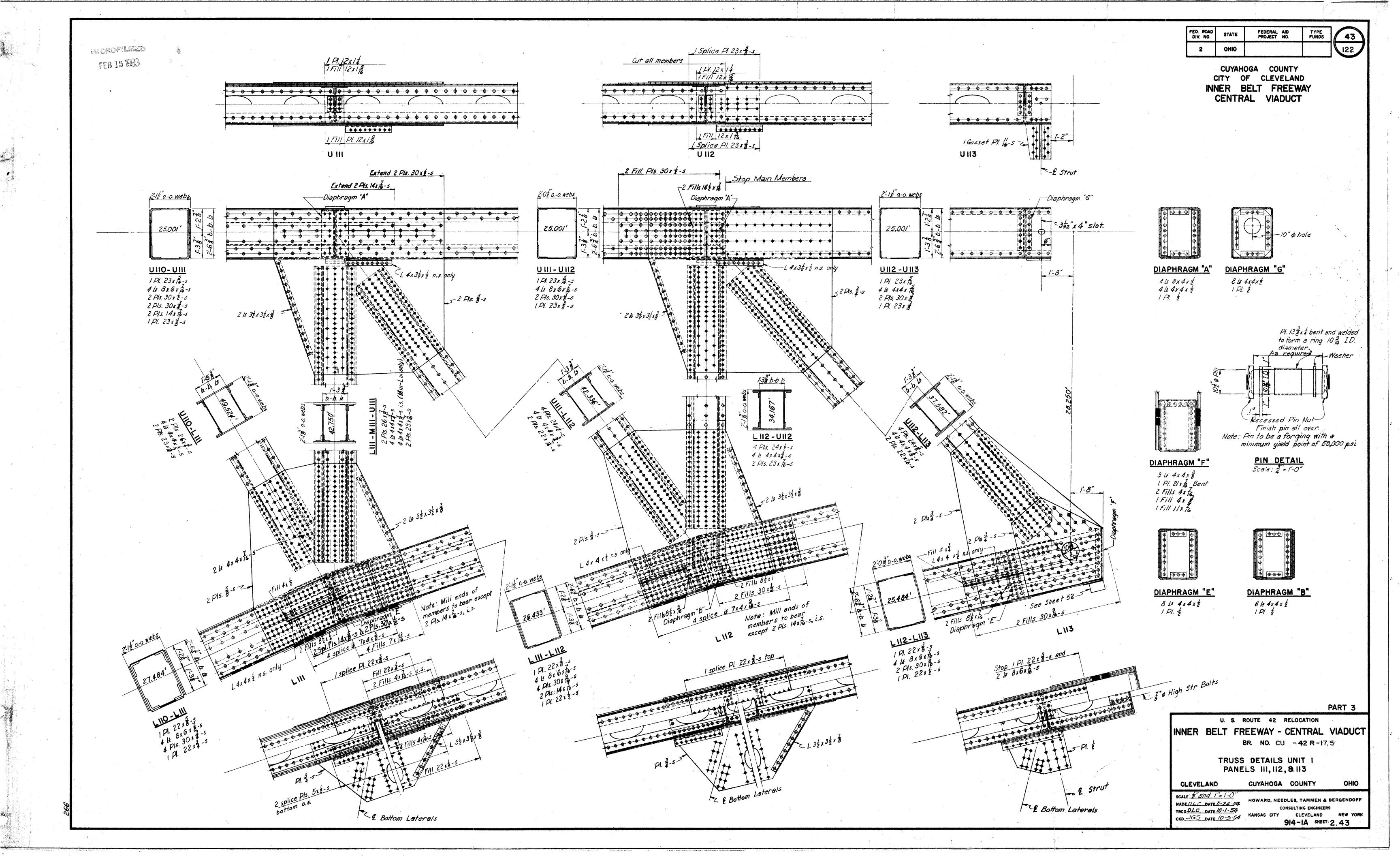
CUYAHOGA COUNTY CLEVELAND

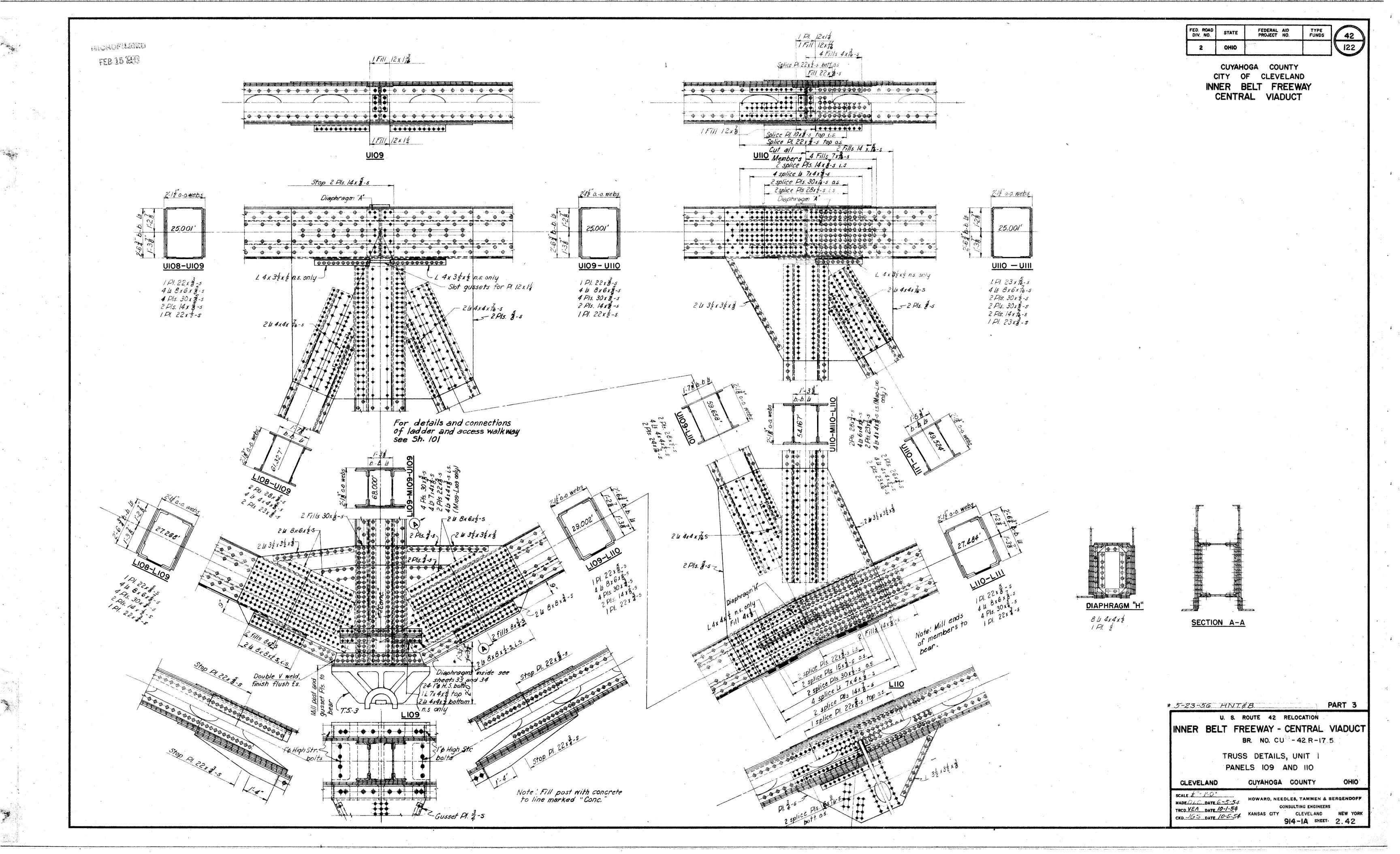
SCALE None 

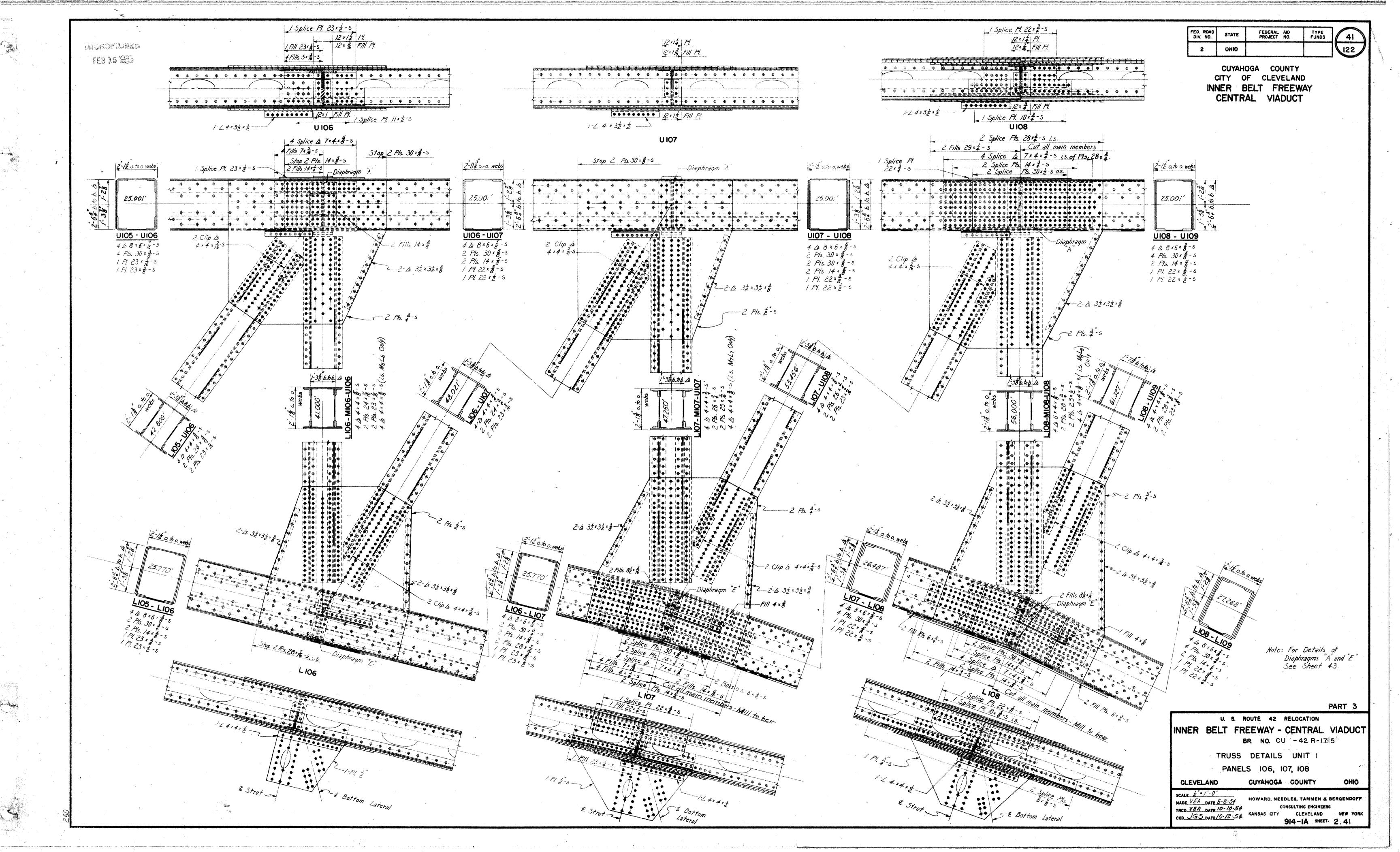
HOWARD, NEEDLES, TAMMEN & BERGENDOF CONSULTING ENGINEERS CLEVELAND NEW YORK

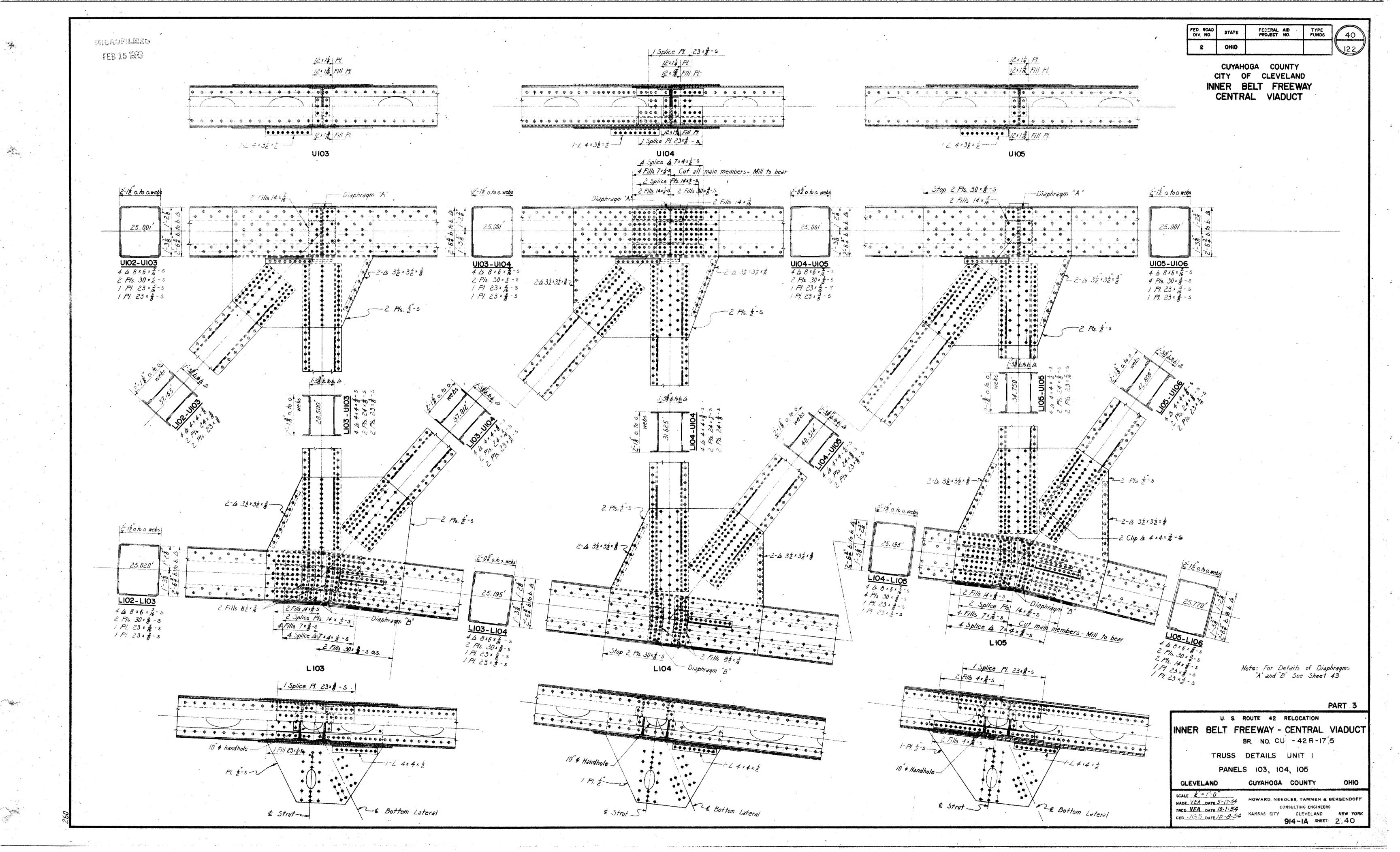
BR. NO. CU - 42 R-17 5

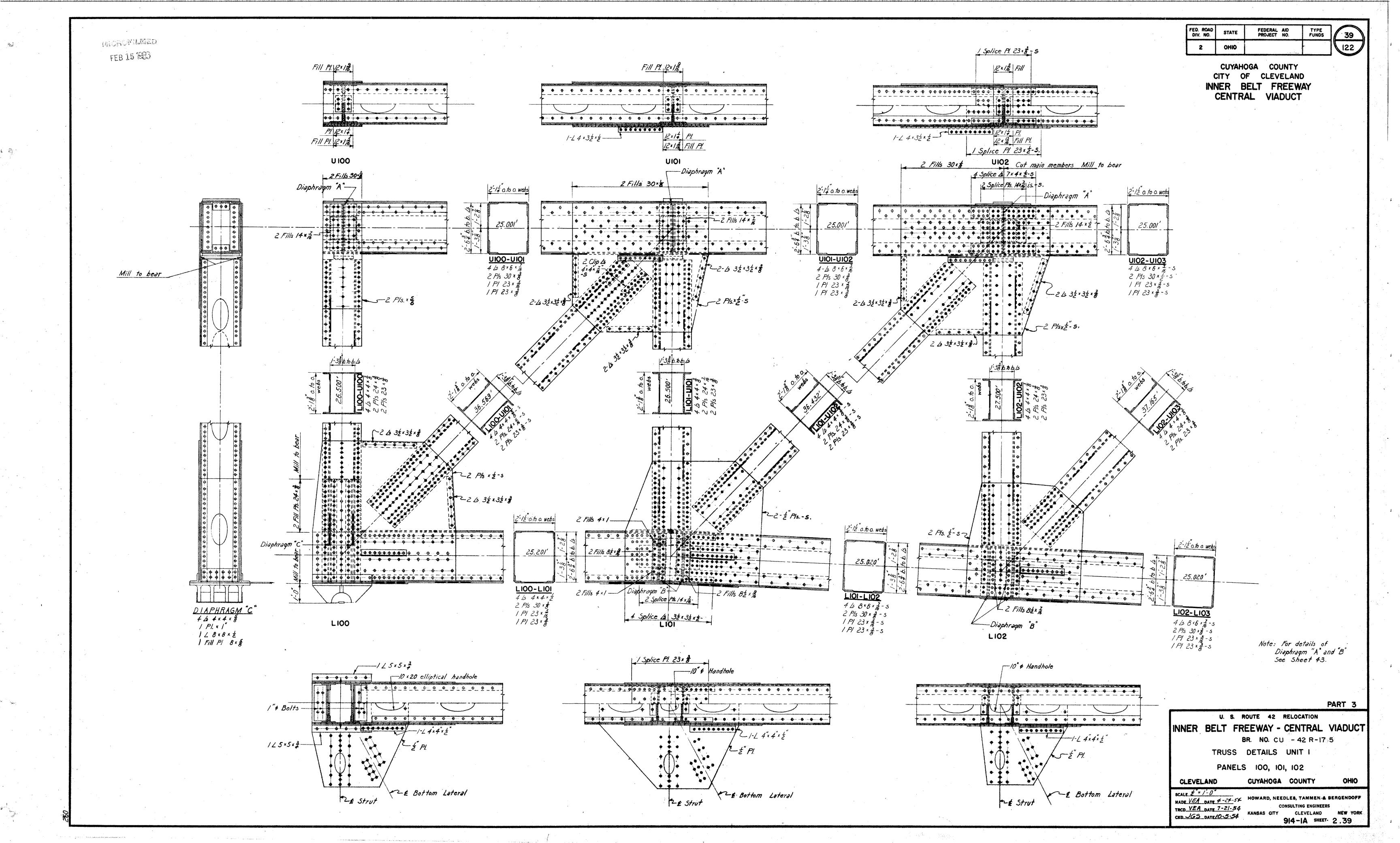
914-1A SHEET- 2:44











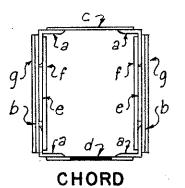
FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	38
2	оню		,	122

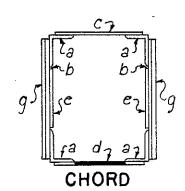
CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT

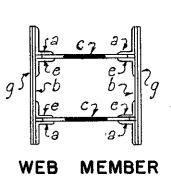
						TENSION	CHOR	D.					·		34	<del>,</del>		,	COM	IDRESSI	ION CH	OBD		,		<u>, , , , , , , , , , , , , , , , , , , </u>	······································
		17.107	1.100	TUDA	Luas	· · · · · · · · · · · · · · · · · · ·			111100	14446	1		11100	11101	1000	11100	17.702	1101	CON	IFRE 331	IUN CH	UNU	1 ( 10.0	1,	1	1, ,,,	
MEMBER	L 100 L 101	L 101 L 102	L 102 L 103	U 104 U 105	U 105 U 106	U 106 U 107	U 107 U 108	U 108 U 109	U109 U110	<i>U110</i> <i>U111</i>	UIII	11113	U 100 U 101	U 101 U 102	U 103	U 103 U 104	L 103 L 104	L 10.4 L 10.5	L 105 L 106	L 100 L 107	L 10.7 L 108	1 108	L 109 L 110	1 111	1.112	1112	·
Dead Load	+334	+384	+186		+769	+1310	+1874	+2351	+23/1	+1771	+998	0	0	-334	-384	-185	-224	-775	-1351	-/931	-2492	-2939		-2541	-1873	-1018	
0.8 Dead Load	+267	+307	+149	+178	+616	+1048	+1500	+1881	+1849	+1417	+799	0	0	-267	-307	-148	-/79	-620	-1081	-1545	-1994	-2351	-2503	-2033		-815	
Live Load + Imp Tension													,										·				
Reduced L.L. + ImpTension	+271	+453	+556	+513	+585	+595	1603	+581	+484	+391	+230	0	0	+153	+295	+428	+550	+501	+392	+272	+145	0	0	0	0	.0	
Live Load + Imp Comp.																					Ï						
Reduced LL+ImpComp.	-/5 <sup>:</sup> 3	-295	-428	-545 +850	-497	-385	-266	-129	0	0	0	0	0.	-271	-453	-556	-519	-587	-613	-620	-617	-597	-623	-532	-412	-236	
Reduced LL+Imp-Ten.xD(CF)e	+449	+751	+922	1850	+970	+986	+1000	+963	+802	+648	+381	0		+254	+489	+709	+912	+830	+650	+451	+240	0	0	0	0	0	
Reduced LL+ Imp-Comp.xD(CF)e	-254	-489	-709	-903	-824	-638	-441	-214	0	0	0	0		-449	-751	-922	-860	-973	-1016	-1028	-/023	-990	-1033	-882	-683	-391	
Ratio = Line (Comp.) or Line (Ten.)	0.458	0.768	2.300	2.455	0.647	0.294	0.142	0.055	0	0	0	0	0	0.458	0.768	2.310	2.455	0.647	0.290	0.141	0.058	0.	0	0	0	0	
LL Sidewalk - Tension	+13	+22	+27	+29	+33	+33	+34	+32	+26	+20	#//	0	0	+9	+16	+24	+27	+25	+/9	+/3	+6	0	0	0	0	0	
LL Sidewalk-Comp.	-9	-16	-24	-27	-25	-/9	-/3	-6	0	0	0	0	0	-/3	-22	-27	-29	-33	-34	-35	-34	-33	<i>-35</i>	-28	-21	-12	
Direct Design Stress	+729	+1080	+1098	+1057 -	+1619	+2067	+2534	+2876	+2677	+2085	+//9/	0	0	-729	-1080	-1097	-1068	-1626	-2/3/	-2608	-3051	-3374	-357/	-2943	-2203	-1218	
Reverse Design Stress			-584	-752												+585	+760										
							ļ			,																	
<u> </u>																					,						
SECTION Holes out for Tension				·																		<u>.</u>					
a Flange Angles 2	4x4x1/2	8x6x7/6 30x3/8	8x6x1/6	8x6x1/16	8x6x7/6	8x6x5/8	8x6x58	8x6x58	8x6x58	8x6x1/6	8x6x1/6	4x4x5/16	8x6x1/16	8x6x7/6	8x6x7/6	8x6x1/6	8x6x7/6	8x6x 1/16	8x6x5/8	8x6x5/8	8x6x78	8x6x1/8	8x6x78	8x6x1/8	8x6x7/16	8x6x 1/6	
b 1st Outside Web Plate 4	30x3/8	30 x 3/8	30x 3/8	30 x 3/8	30 x 3/8	30 x 5/8	30 x 5/8	30 x 5/8	30 x 5/8	30 x 3/8	30 x 3/8	30 x 3/8	30x 3/8	30x3/8	30x1/2	30x1/2	30x3/8	30x3/A	30 x 3/4	30 x 3/4	30 x 3/4	30x 3/2	30x3/4	30x3/a	30x %	30 x %	
c lop cover Plate   3	23x 1/6	123x716	23x 7/16	23x 1/16	123x716	1 22 x 3/8	1 ZZX 7/8	122x 3/8	122x1/8	238716	123x716	23x 2/16	1 23x 3/1c	1 23x %/6	123 x 2/16	123x %6	$123x^{3/8}$	$23x^{3/8}$	$123x^{3/8}$	$123x^{3/8}$	$122x^{2/8}$	122x 3/8	122x <sup>2</sup> /8	122 x 3/8	$122x\frac{3}{8}$	$+22x^{3/8}+$	
d Bottom Cover Plate 2	23x3/g(11"Hole	23x3/g(II"Hole)	23x3/8 (11"Hole)	23x3g(11"Hole)	23x3/g(11"Hole	) 22x1/2 (11" Hole	22x1/2(11" Hole	) 22x 1/2 (11" Hole,	22x1/2 (11"Hole)	23 x 3/6 (11" Hole)	23x3/g(11"Hole)	23 x 3/8 (II" Hole)	23x3/6(11" Hole)	23x3/8(11" Hole	23x 3/8(11" Hole)	23x3/g(11"Hole)	) 23x1/2(11"Hole)	23 x 1/2 (11"Hole)	23x/2(11"Hole)	23×1/2(11"Hole,	) 22x 3/6(10"Hole	) 22x3/4(10"Hole	22x 3/00" Hole	22x3/ (10" Hole	22x1/2(11"Hole	) 22x1/2(11"Hole)	
e   st   Inside Web Plate   2						14 x 5/8	14 x 5/8	14 x 5/8	14 x 3/8	14 x 1/16									14 x 5/8				14x1/8		14 x 1/6	12.	
f 2nd Inside Web Plate 4																	· ·			28 x 1/16							
g 2 <sup>nd</sup> Outside Web Plate 4		1			30 x 3/8		30 x 3/8	30 x 5/8	30 x 5/8	30 x 1/2								30 x 3/8		,6	30 x 3/n	30 x 3/2	30x3/4	30x 34	30 x %		
g 2" Ourside Web Plate   4		<del></del>			1				1										<b></b>		1	1	1	1 11 17	1 - 1.716		
q  2 · · · · · · · · · · · · · · · · · ·				i				+	<del>                                     </del>				300	300	300	300	3024	3024	3093	3093	317.8	3272	327.2	3298	317.2	305.8	
									1							200	JUL. 7	1000.	1000.0	1000	1 277.0	V2.1.2	1 0 ~ / . 2				
Length In.									<del> </del>		<u> </u>				11.20	11.20	1 1063	//./9	1 <i>10.82</i> -	1 70.38	1 10 80	1 10.87	1058	10.80	10.40	1 70.62 1	l l
Length In. Min. Radius of Gyration In.		24.000	24.000	24,000	24.000	24.000	24,000	24,000	24.000	24.000	24.000	18.000	10.98	10.98	11.20 19.670	11.20 19.670	19.630	11.19 19.660	19.620	19.590	19.600	10.81 19.580	10.58	10.80	10.40	10.62	-
Length In. Min. Radius of Gyration In. Allowable Stress Lbs/Sq.In. Actual Gross Area Sa.In.	18,000 49,19	24,000 57.91	24,000 57.91	24,000 57.91	24,000 80.41	24,000	24,000 124.69	24,000 139.69	24,000 132.69	24,000 100.16	24,000 57.91	18,000 43.79	10.98 14,810 57.91	10.98 14,810 57.91	19,670 6541	19,670 65.41	19,630	19,660 83.35	19,620	19,590	19,600 158.67	19,580	19,560	19,570	19,570	19,620 70.22	
Length In. Min. Radius of Gyration In. Allowable Stress Lbs/Sq.In. Actual Gross Area Sq.In. Net Area Sa.In.	18,000 49.19 40.50	49.72	49.72	49.72	69.22	87.57	1 <i>107.07</i>	120.07	114.07	86.22	<i>49.72</i>	36.60	10.98 14,810 57.91	10.98 14,810 57.91	19,670 6541	19,670 65.41	19,630	19,660 83.35	19,620	19,590	19,600 158.67	19,580	19,560	19,570	19,570	19,620 70.22	
Length In. Min. Radius of Gyration In. Allowable Stress Lbs/Sq.In. Actual Gross Area Sa.In.	18,000 49.19 40.50	49.72	49.72	49.72	69.22	87.57	1 <i>107.07</i>	120.07	114.07	86.22	<i>49.72</i>	36.60	10.98 14,810 57.91	10.98 14,810 57.91 51.51	19,670 65.41 59.49	19,670 65.41 59.49	19,630 60.85 54.28	19,660 83.35 82.97	19,620 110.57 110.19	19,590 135.07 135.07	19,600 158.67 158.67	19,580 172.67 172.67	19,560 183.17 183.17	19,570 158.67 158.67	19,570 117.22 117.22	19,620 70.22	

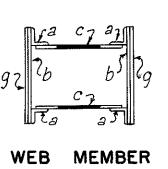
		TENSION WEB MEMBERS												COMPRESSION WEB MEMBERS																				
	MEMBER	L 102 U103	L 103 U 104	L 104 U 103	L105 U106	L 106 U 10	1 L 107 7 U 108	L 108 U 109	U109 L110	1 4110 LIII	UIII LII2	U112	3 U101 3 L10	U 102 1 L 10	2	U100 L100	L 100 U101	L 101 U 102	LI 103 L 103	U104 L104	U 105 L 105	U 106 M 106	M 106 L 106	U 107 M 107	M 107 L 107	U 108 M 108	M 108 L 108	U109 M109	M 109 L 109	U 110 M 110	M/10 L/10	UIII MIII	M///	U112
Dead Load		+295 +236	+618	+881	+928	+1082	+1022	+842	+914	+1070	+1306	+1501	+230	+.67		-102	-488	-73	-339	-595	-816	-889	-1032	-1075	-1218	-1051	-//95	-1761	-/910	-1078	-1222	-//93	-/336	-/250
0.8 Dead Load		+236	+618 +495	+881 +705	+743	+866	+818	+674	+731	+856	+1045	+1201	+184	+54		-82	-488 -391	-73 -59	-27/	-476	-653	-7//	-826		-975	-841	-956	-1409		-863	-978	-954	-1069	-100
Live Load + Imp Tension																																		
Reduced LL+Imp. Tens		+207	+196	+211	+252	+277	+308	+315	+201	+238	+298	+347	+254	+183		0	+225	+208	+/32	+58	+33	+2	+2	+2	+2	+40	+40	+23	+23	0	0	0	0	0
Live Load + Imp Comp.																														, in the second				
Reduced LL+ImpCon	ηρ.	-219	-//2	-69	-7	-3	-47	-105	. 0	0	0	0	-/63	-/52	*4	-47	-397	-296	-154	-154	-/75	-220	-271	-249	-296	-288	-333	-347	-386	-220	-267	-255	-296	-274
Reduced LL +ImpTen.	xD(C.F)e	+343	+325	+349	+418	+459	+511	+522	+333	+395	+494	+575	+421	+303		0	+373	+345	+219	+96	+55	+4	+4	+4	+4	+66	+66	+38	+38	0	0	0		0
Reduced LL+ImpComp		-363	-186	-115	-/2	-5	-78	-/74	0	10	0	0	-270	-252		-78	-658	-49/	-255	-255	-290	-365	-449	-413	-491	-477	-552	-575	-640	-365	-443	-423	-491	-454
Ratio = Line 4 or -	Line G	0.742		0.078	0.007	0.003	0.046	0.125	0	10	0	0	0.709	2.265		0	0.461	2.850	0.407	0.098	0.041	0.002	0.002	0.002	0.002	0.038	0.033	0.013	0.012	0	0	0	0	0
LL Sidewalk-Tension		+/2	+//	+/3	+//	+/3	+14	+/5	+10	+/2	+/5	+17	+/2	+8		0	+/3	+12	+6	+2	+/	0	0	0.00	0	+2	+2	+/	+/	0	0	0	0	0
LL Sidewalk - Comp.		-9	-4	-2	0	0	-3	-6	0	0	0	10	-9	-8		-/	-/9	-/3	-9	-9	-//	-/0	-12	-/2	-14	-/4	-16	-20	-22	-/2	-/4	/3	-15	-14
Direct Design Stress		+5.91	+831	+1067	+//72	+/338	+1343	+1211	+1074	+1263	+1554	+1793	+617	+365		-161	-1068	-563	-535	-740	-954	-1086	-1287			-/332	-/524	-2004		-/240		-1390		
Reverse Design Stres					<del>  '''                                 </del>				1.0	1,200	+	1		-206		1 /01	1000	+298		140	1 2 3 7	1000	1201	7205	7400	1552	1027	2007	2750	1240	1733	1,555	1 , 3 , 3	1,,,,
	,						V 1	·						1 200		<b>-</b>		1.200	·		<u> </u>						-							· · · · · · · · · · · · · · · · · · ·
						<u> </u>								<u> </u>					<del> </del>	_				-										
SECTION	Holes out for Tension										· ·																							
a Outer Flange Angles	2	4 x 4 x 3/8	4x4x3/8	4 x 4 x 1/2	4x4x5/8	4x4x 3/4	4x4x 5/8	4x4x 5/8	4x4x1/2	4x4x1/2	4 x 4 x 3/4	4x4x 5/8	4 x 4 x 3/8	4 x 4 x 3/	3	4 x 4 x 3/8	4x4x5/8	4x4 x 3/8	4 x 4 x 3/8	4 x 4 x 3/8	4x4x1/2	4 x 4 x 5/8	4 x 4 x 5/8	4 x 4 x 3/a	4x4x3/4	Gx4x5/8	6x4x5/8	7x4x 1/8	7x4x7/8	6x4x1/2	6x4x1/2	4 x 4 x 3/a	4 x 4 x 3/a	4 x 4 x 3
b 1.5t Web Plates	3	24 x 3/8	24 x 7/16	24 x 5/8	24 x 5/8	24 x 3/4	26 x 3/4	28 x 5/8	28 x ½	26 x 3/4	24 x 1/2	24 x 5/8	24 x 1/16	24 x 3/8									24 x 11/16											
c Cover Plates	2	23×3/6(10" Hole)	23x3/e(10"Hole	) 23x3/0(10"Hol	le) 23x7/2 (10" Hol	le) 23×7/6 (10" Hole	2) 23× 1/1 (10" Hol	(e) 23x 3/6 (10"Ho/e	) 24× 7/4 (10" Hal	10) 23 x % (10"Ho	(c) 22 x 1/4 (10"Ho)	(a) 22x % (10" Ho	(e) 22 x 3/2 (10 4/2)	(a) 23 x 3/0 (10" Hc	(e)	23 × 3/0(10" Ho.14	1 23 3/0 (10"40 10	1 23× 3/0/10"Ha	(a) 22 × 3/2 (10" U2 10	1 21 3/2 (10"11-12	1 22 × 7/ (10" 4-1	122 1/ /10"4-10	) 23×7/6(10"Hole)	23 7/ (10"4-101	28, 7, (10/11/2)	23 x ½ (10"40 /0)	23x 1/4 (10"Hole)	) 22 x 5/0 (10" 40 /p)	22 × 50 (10"Hale	23× 7 (10"Ha/a)	23 × 3/ (10"Halo	1 23 × 3 (10"40 10)	23 7. (10"4 10	(a) 23x 7. (10"H
e Inner Flange Angles	s 2				76.	76			7,6 (10)	76(	7/6	7,00	- 25 4 78 (10 110)	27227786	· · · · · · · · · · · · · · · · · · ·	257.5610.000	7 23. 18(10 11010	23.78 (0 1101	27 Z3X /BUO HOLE	7 L4x 78 (10 Haie,	1 23 × 7/6 00 71016	IL IN ME (10 HOIE	4 x 4 x 3/8	1 2 2 1/600 11016)	4 x 4 x 3/8	23/200110101	4 x 4 x 3/8	, 18 60 110107	4 x 4 x 3/8	2327600 110107	4 x 4 x 3/8		4x4x3/8	
e Inner Flange Angles g 2 <sup>nd</sup> Web Plates	3							<del>-  </del>			24 v 1/2	24 x 5/8					<del> </del>					<del></del>	7 3 7 3 7 5	<del>                                     </del>	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	<del> </del>	7777 70	30 x 5/8			7 7 7 7 0		77770	24 x ½
, , , , , , , , , , , , , , , , , , , ,											24172	21770																30 x 4/8	JU X 9/8					2411
Length	10															210	438.8	1372	3/12	270 5	4/7	102	7402	507	FC7	274	C22	916	010	CFO	CEO	F12	F12	410
Min. Radius of Gyrat.	$\frac{111}{100}$					<del>- </del>	-				·				<del>- </del>	7.70	770.0	771.6		379.5		492	# 7C	0.07	770	0.16 0.EC	672	8/6	816	650	650	513		410
Allowable Stress	160/00/10	18 000	21 000	21.000	21.000	24.000	24 000	21 000	24.000	24 000	24 000	21 000	10000	1/0 000		14.570	10.70	10.500	7.70	7.60	7.63	10.000	7.50	8.00	7. 78	8.56	8.28	9.08	8.87	8.50	8.23	7.96	7.75	1.63
Actual Gross Area	Lbs/Sq.ln. Sq.ln.	20 10	12 10	24,000	124,000	24,000	24,000	24,000	24,000	24,000	24,000	24,000	10,000	18,000	<u> </u>	14,570	18,510	10,020	13,090	18,850	10,630	10,020	7.30 18,020 74.26 74.26 17,300	11,060	11,560	11,040	11,040	16,//0	16, 110	11,130	11,130	17,980	17,980	10,6/
N. L A	3q. [F].	33.13	25.13	34,15	10.02	69.14	68.82	65.19	35.25	65.38	80.26	88.94	42.19	39.19		<b>39./9</b>	61.19	39.19	39.79	45.94	56.38	62.82	14.26	12.14	83.58	18.44	89.88	125.44	136.88	12.38	83.82	18.64	90.08	81.14
Net Area	Sq.ln. Lbs/5q.ln.	32.44	33.07	45.50	47.56	36.09	56.01	31.69	45.50	53.63	66.5/	14.69	35.07	32.44		31.88	59.64	31.33	31.33	39.28	52.78	61.27	14.26	12.14	83.58	78.44	89.88	125.44	136.88	12.38	83.82	18.64	90.08	81.14
Actual Unit Stress	LOS/ 59./n.	18,220	23,100	23,450	23, 160	23,500	23,950	23,430	23,600	23,550	23,370	24,000	17,600	11,250		5,050	17, 910	17,970	17,070	18,820	18,080	17,700	17,300	17,800	17,700	17,000	16,950	15,980	16,000	17,130	17,130	17,670	17,500	18,150
Material		C	5	5	5	S	1 5	1 5	<i>S</i>	1 5	5	1 5	1 C	1 C			15	1 S	15	1 S	1 5	15	1 S	1 5	15	1'5	15	1 S	IS	1 5	1 5	1 <i>S</i>	S	1 <i>S</i>

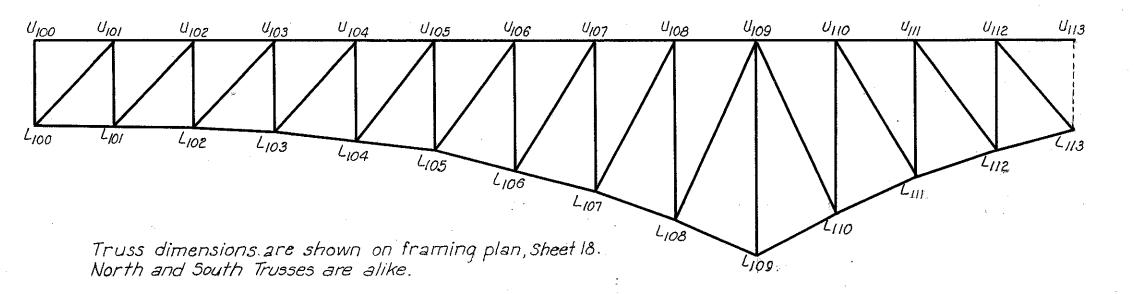
S = Special Steel C = Carbon Steel











PART 3

u. s. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42 R-17.5

STRESS SHEET UNIT I NORTH AND SOUTH TRUSSES

CLEVELAND CUYAHOGA COUNTY

SCALE Nome

MADE D.M.E. DATE 5-7-54

TRCD L.B.R. DATE 9-16-54

CKD G.J. K. DATE 9-16-54

KAI

HOWARD, NEEDLES, TAMMEN & BERGENDOFF

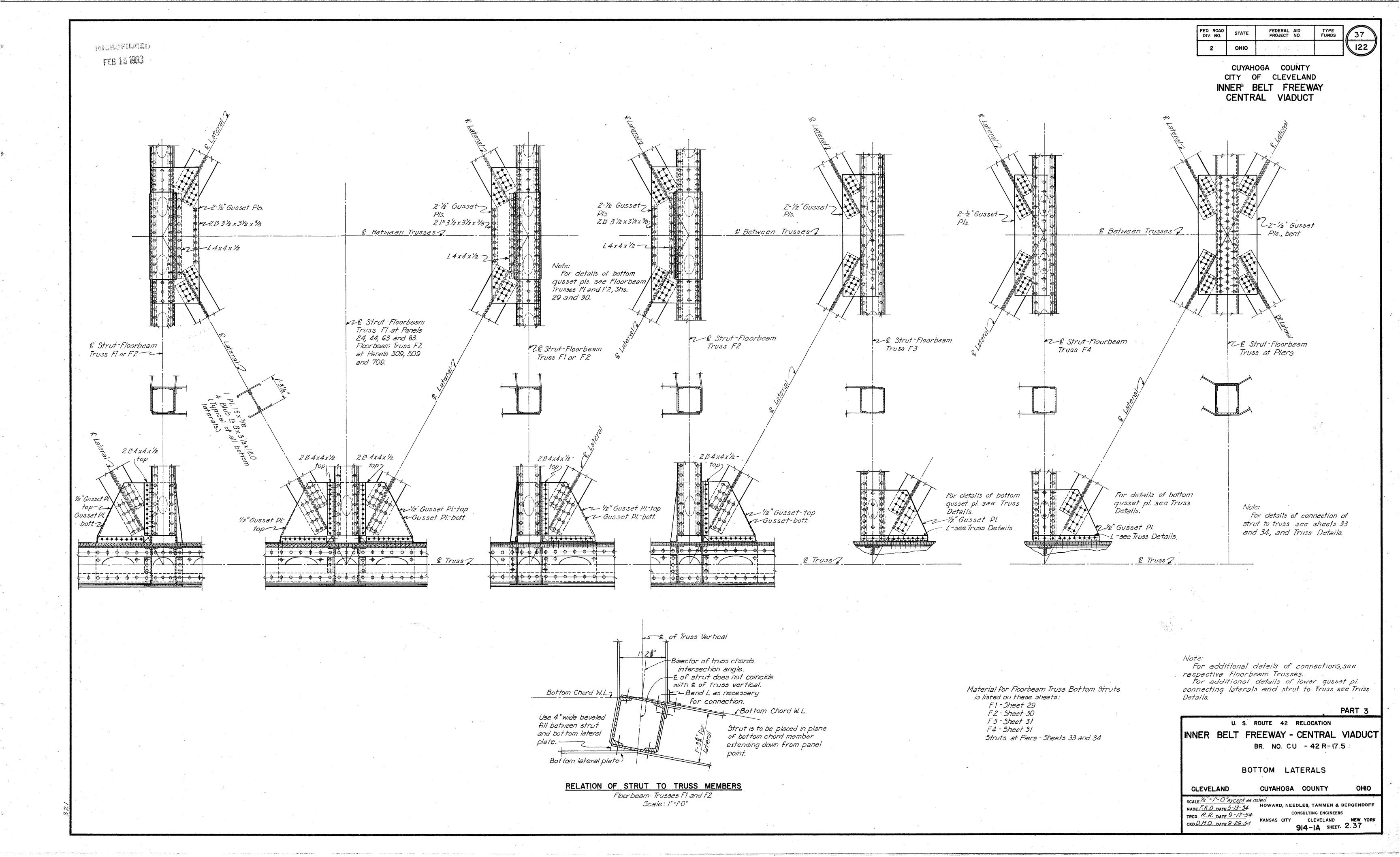
CONSULTING ENGINEERS

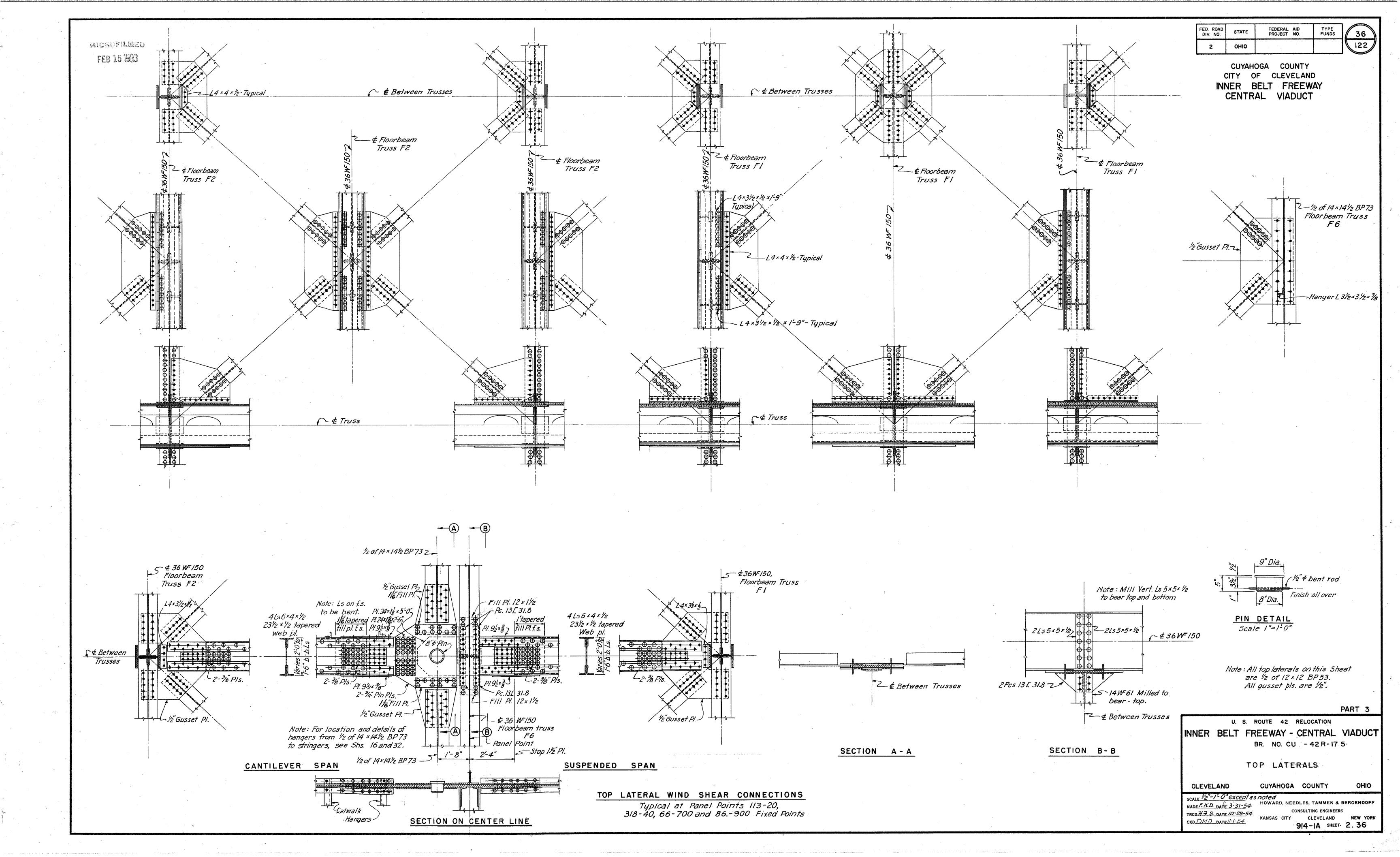
KANSAS CITY CLEVELAND NEW YORK

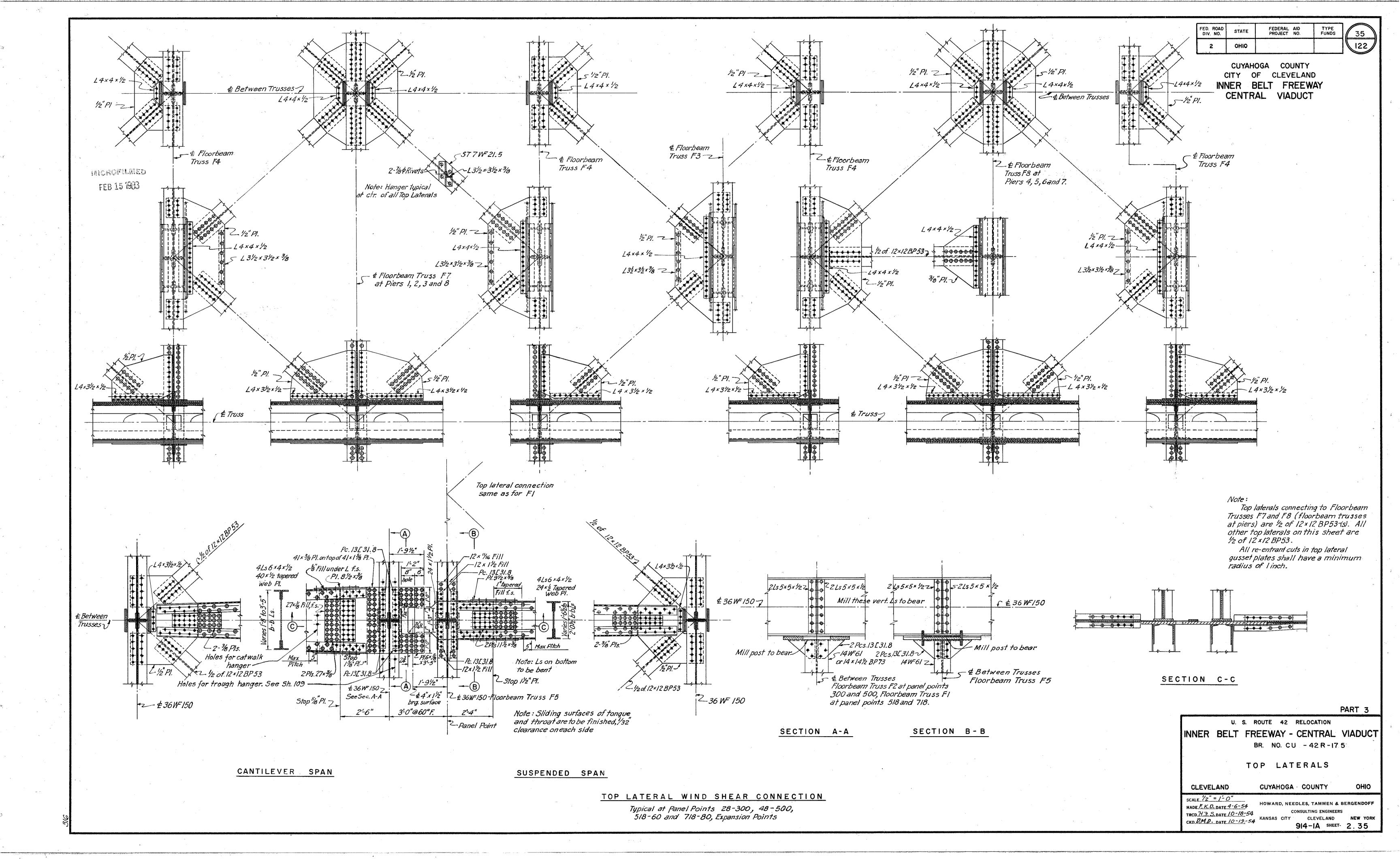
914-14 SHEET- 2.38

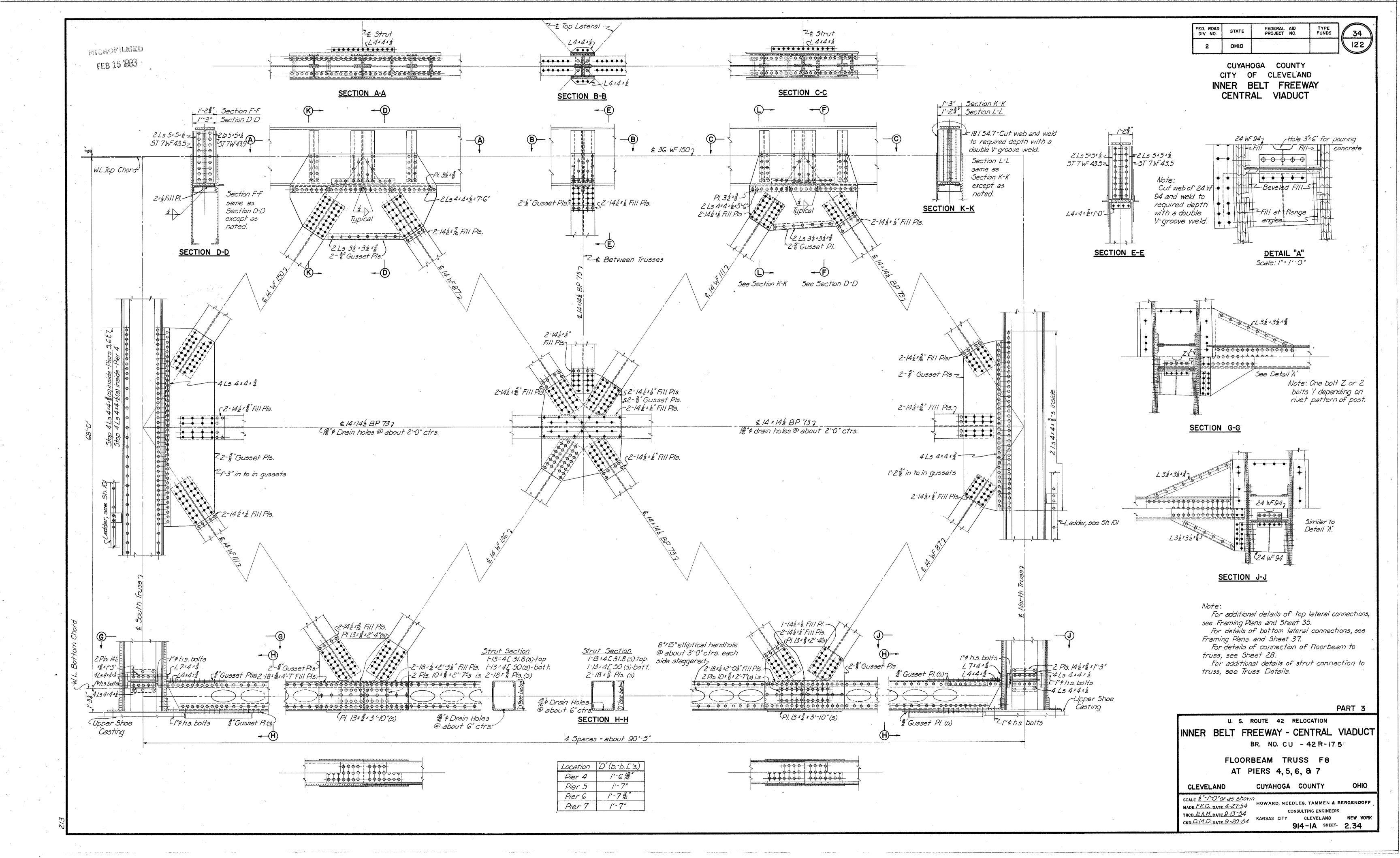
/ All dead and live load stresses are in kips.

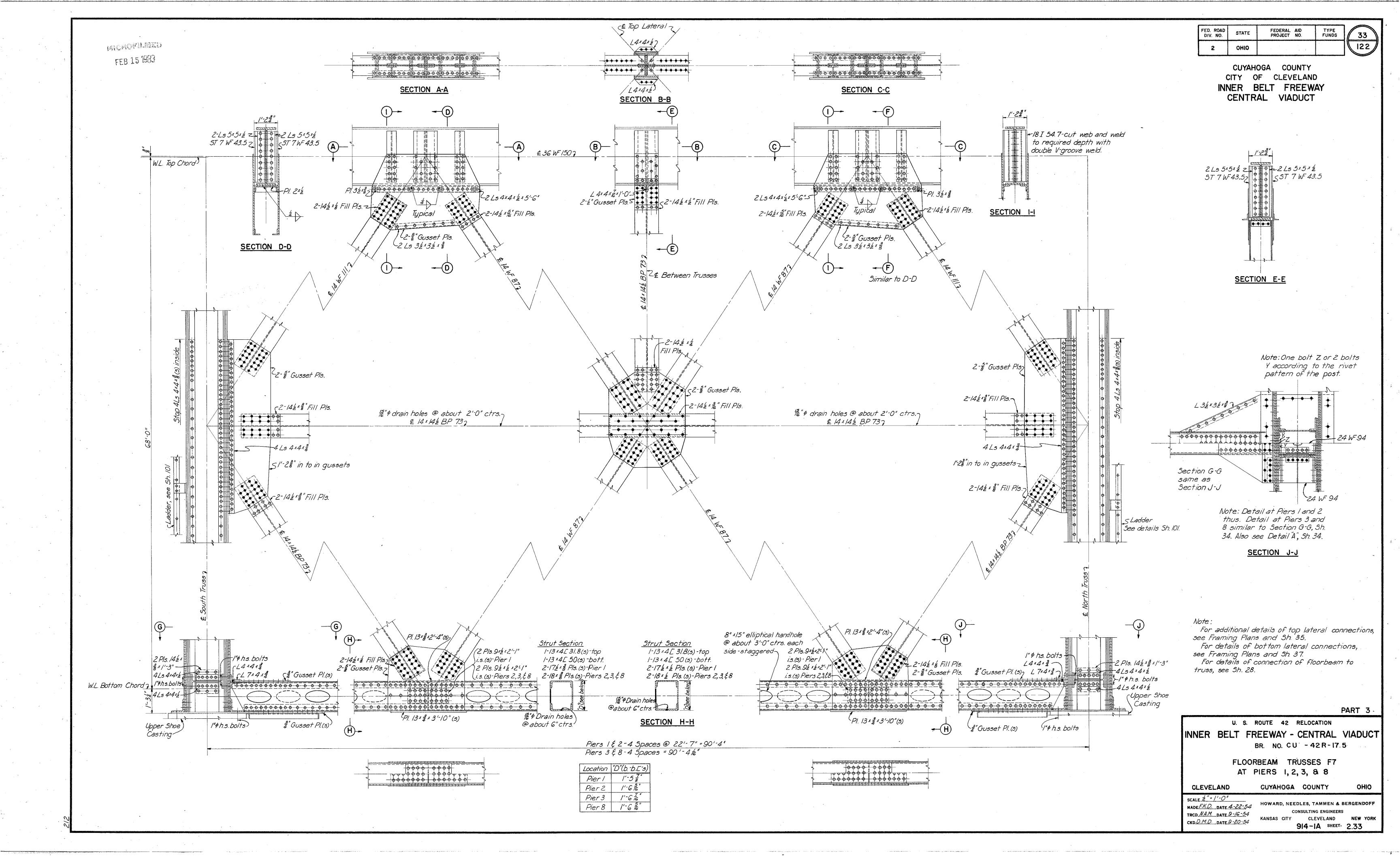
Line 29, net area for tension or effective gross area for compression.

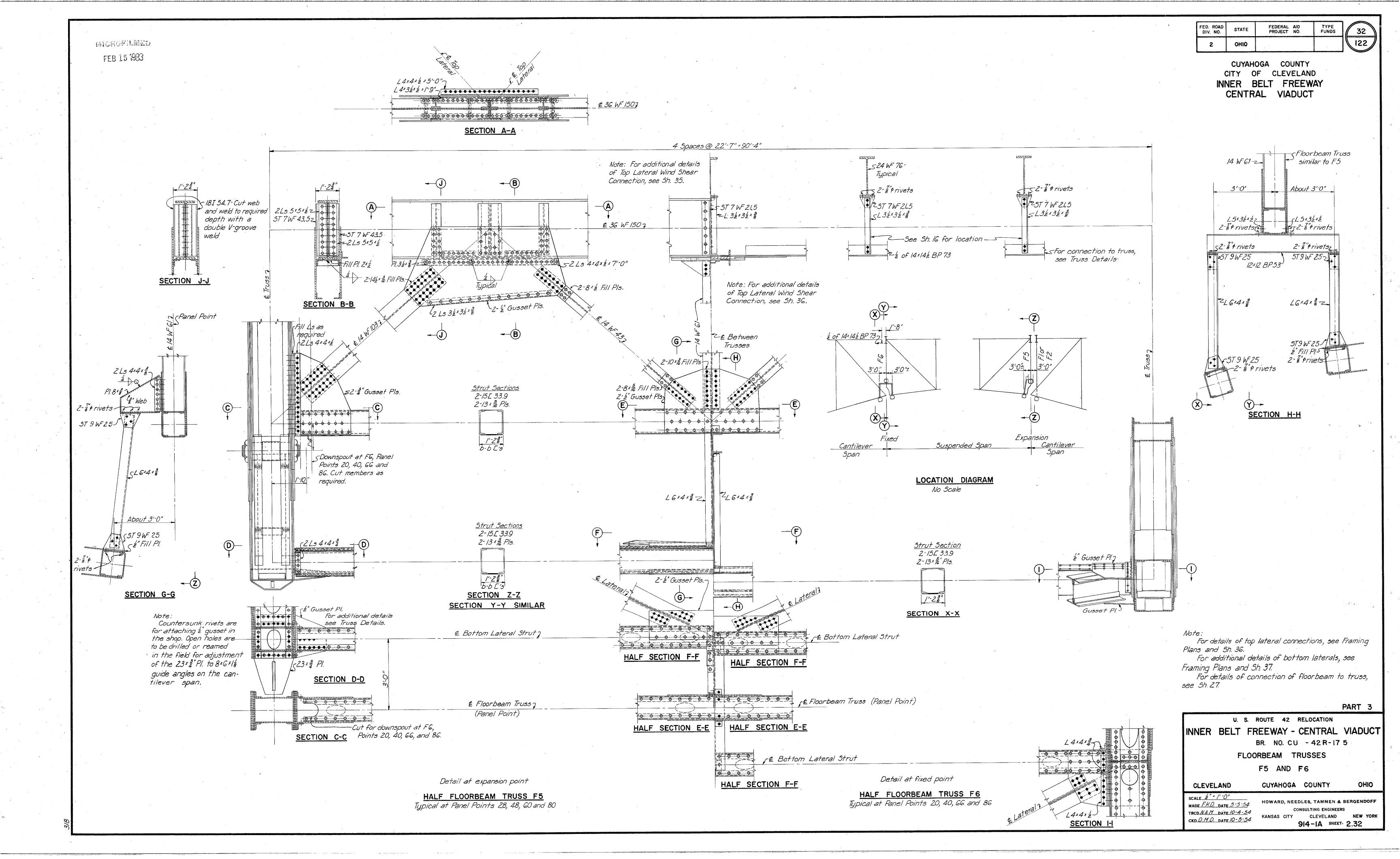


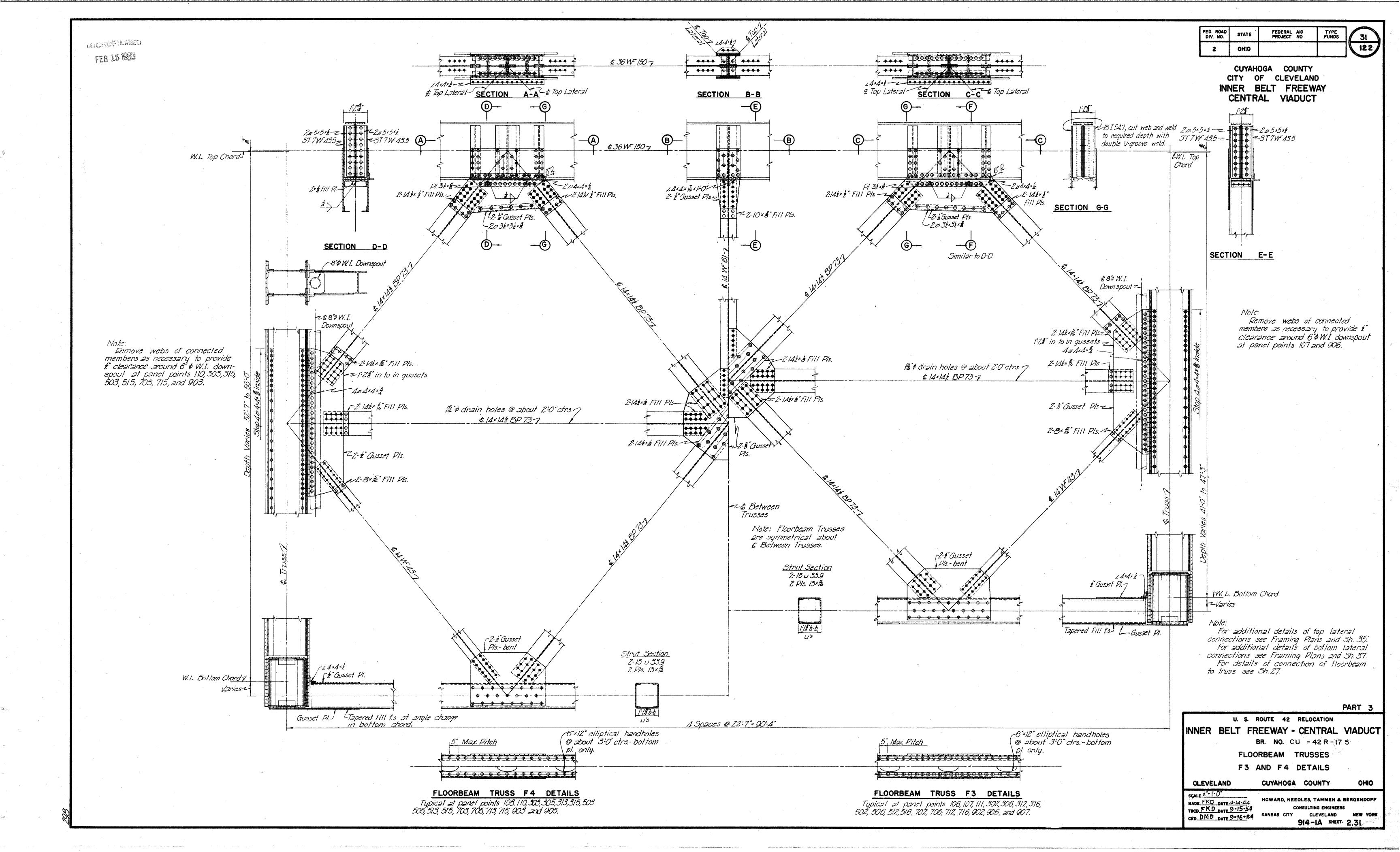


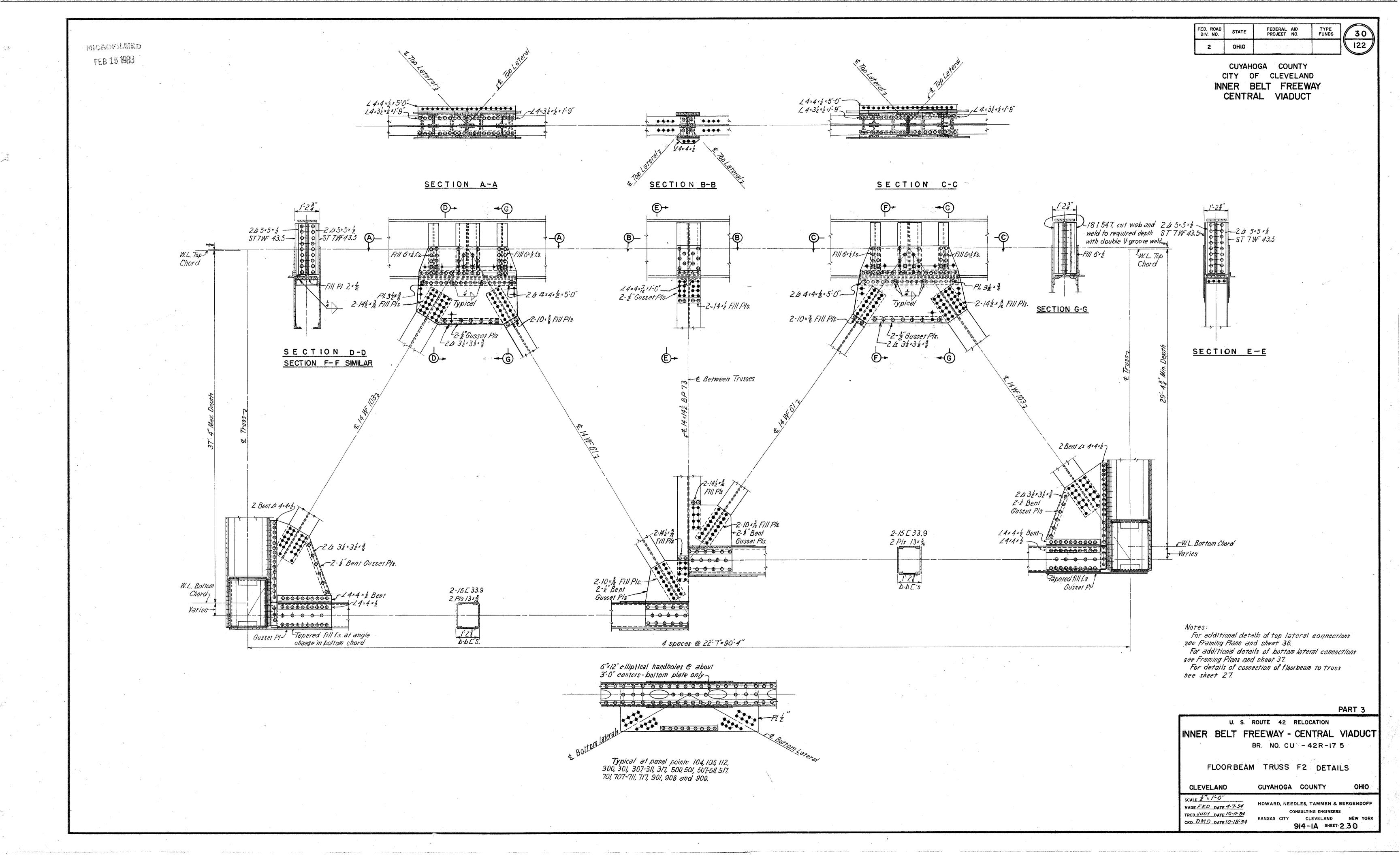


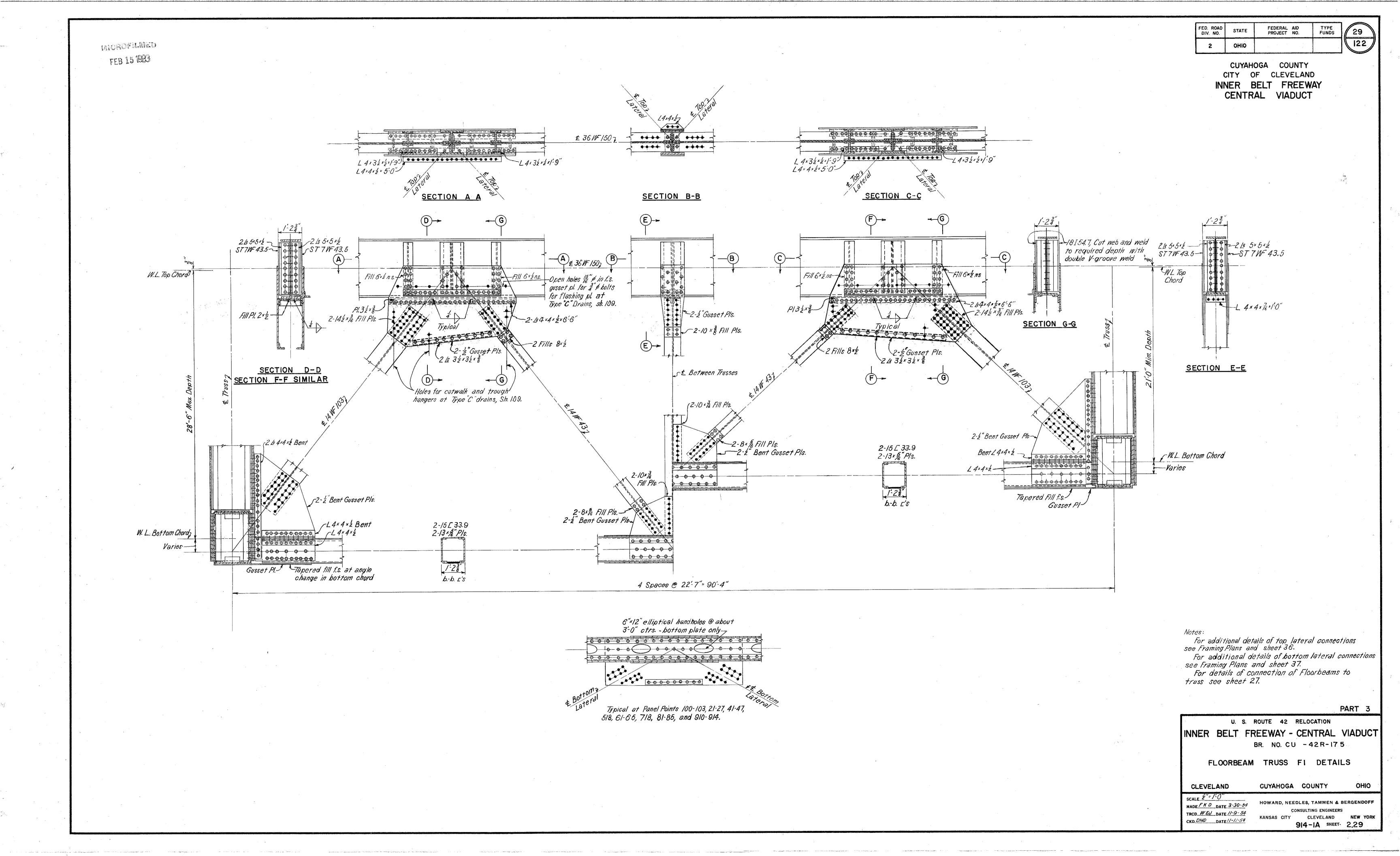


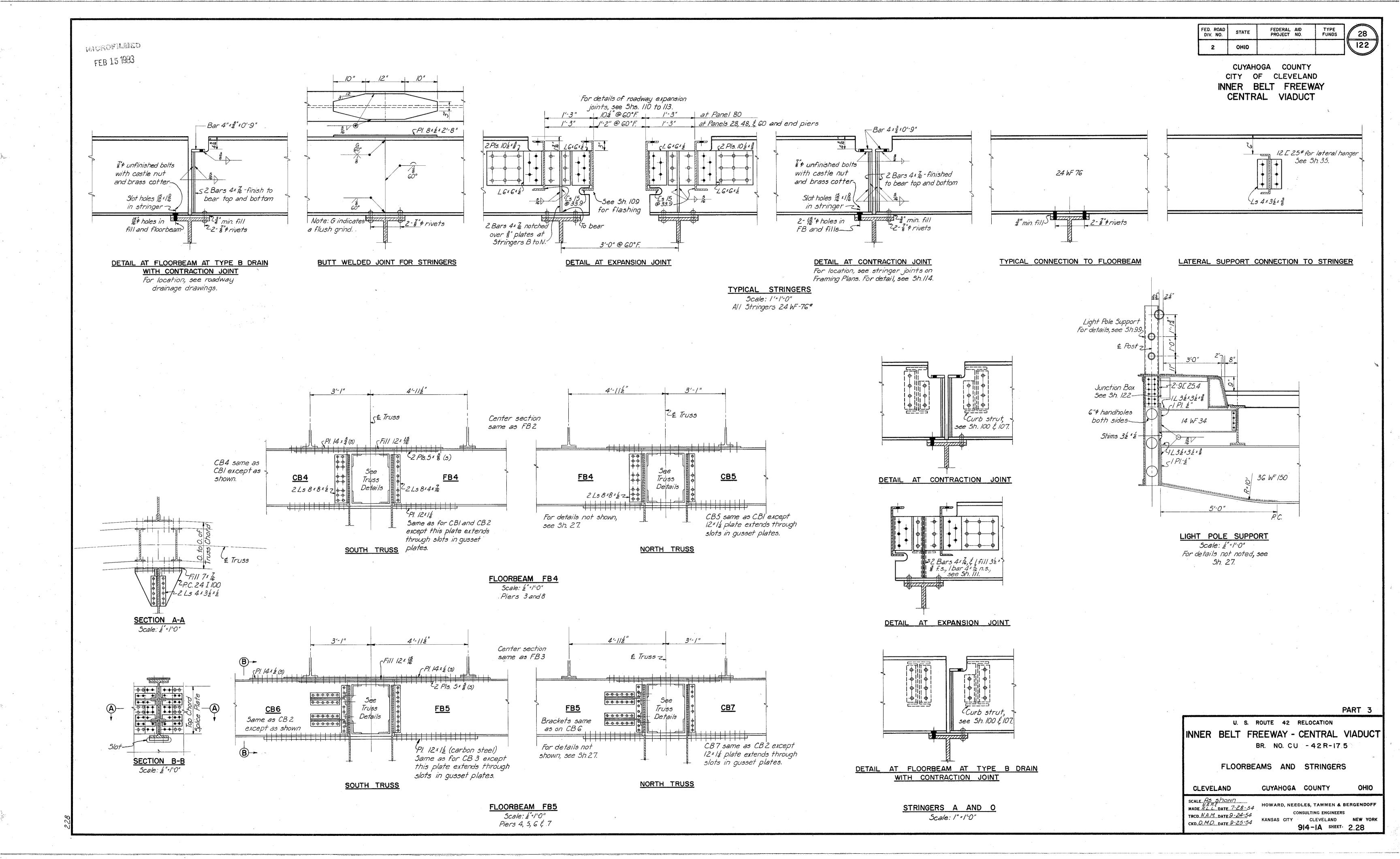


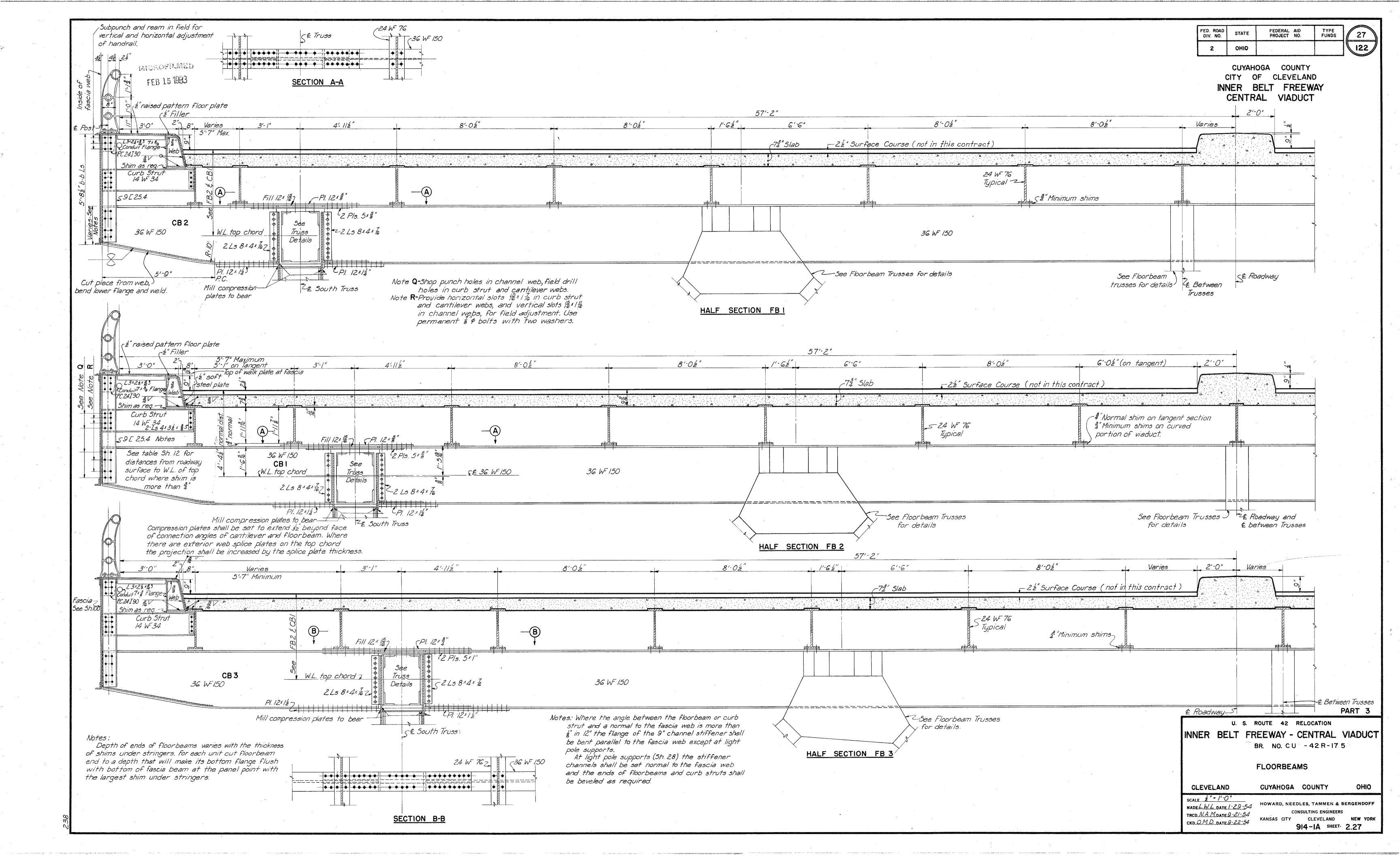


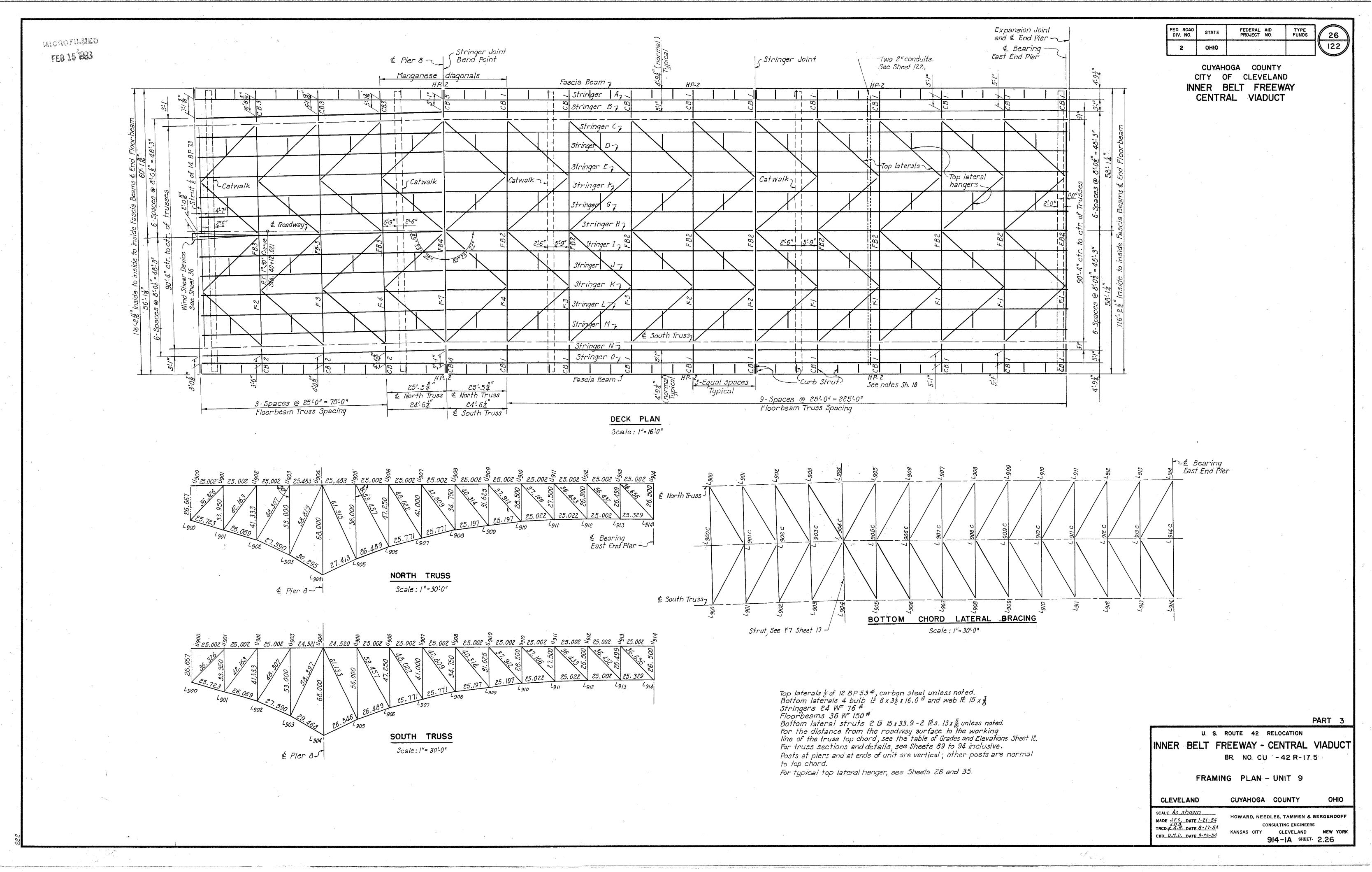












£ Expansion Joint -3 25.002 \$ 25.002 \$ 25.002 \$ 25.002 \$ 25.002 \$

MICEOFILMED

FEB 15 (43)

FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. OHIO CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

STATE

Stringer Joint

Stringer Az

Stringer By

Stringer E-

Stringer J-

Fascia Beam

Le North Truss

É South Truss

6-Spaces @ 25'-0"= 150'-0" Floorbeam Truss spacing

Scale : l'= 16!-0"

Stringer F

Stringer

(Top lateral hangers

Top laterals -

Fascia Beam

¢ Roadway →

TRUSSES

Scale: |"=30

BOTTOM CHORD LATERAL BRACING

Scale: |"= 3010"

TYPE FUNDS

122

Top laterals tof 12 BP 53 #
Bottom laterals 4 bulb 1 8 x 3 to x 16.0 # - Web 12 15 x 3 to Stringers 24 WF 76 #
Floorbeambs 36 WF 150 # Bottom lateral struts 2 [ 15 x 33.9 # - 2 Rs. 13 x \frac{5}{16}

For details of north truss, see Sheet 18 for Unit 6.

For details of south truss, see Sheet 19 for Unit 6.

Sections are identical to trusses of Unit 6, and details

will be similar except as modified by lengths of members

in end panels, and vertical bend points in trusses of Unit 6 at U62 and U64.

For the distance from the roadway surface to the working line of the truss top chord, see the table of Grades and Elevations, Sheet 12.

For truss sections and stresses, see the Stress sheet

for Unit 8, Sheet 88.
Posts at ends of units are vertical; other posts are

normal to the top chord.

For typical top lateral hanger, see Sheets 28 and 35.

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R-17.5

FRAMING PLAN - UNIT 8

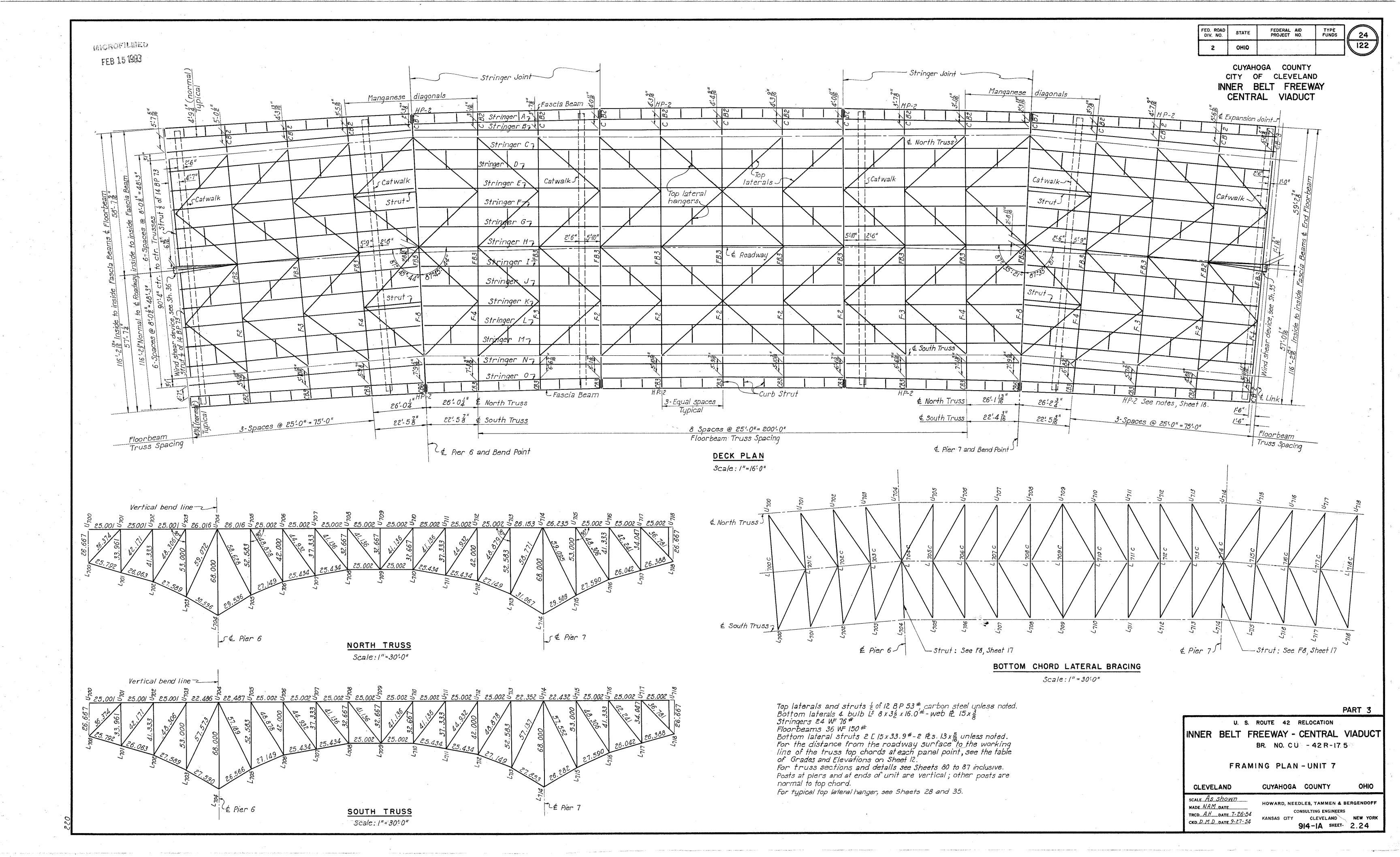
CUYAHOGA COUNTY CLEVELAND

SCALE As shown MADE J.G.S. DATE 1-14-54 TRCDG.K. FA.H.DATE 8-17-54

CKD D.M.D. DATE 9-29-54

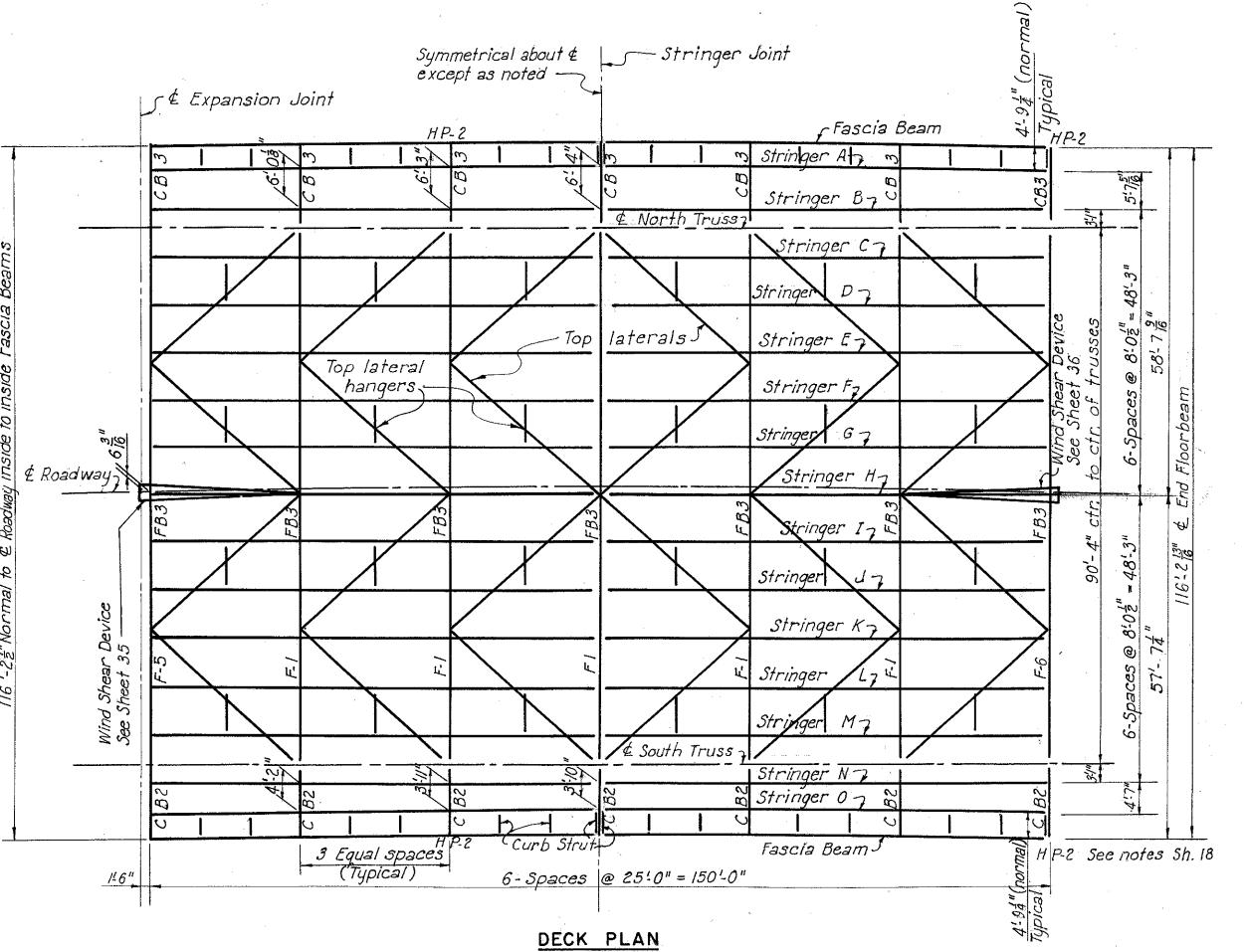
HOWARD, NEEDLES, TAMMEN & BERGENDOFF CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK 914-IA SHEET- 2.25



iaicadfilmed Feb 15 (483 FED. ROAD DIV. NO. STATE FEDERAL AID TYPE FUNDS
2 OHIO

CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT



+0.0536 % -0.2390 % -0.5316 %

\$25.000 \( \frac{1}{2} \) 25.000 \( \frac{1}{2} \) 25.022 \( \frac{1}{2} \) 25.008 \( \frac{1}{2} \) 25.008 \( \frac{1}{2} \) 25.022 \( \frac{1}{2} \) 25.022 \( \frac{1}{2} \) 25.008 \( \frac{1}{2} \) 25.008 \( \frac{1}{2} \) 25.022 \( \frac{1}{2} \) 26.008 \( \frac{1}{2} \) 25.008 \( \frac{1}{2} \) 25.022 \( \frac{1}{2} \) 25.008 \( \fra

Top laterals \{ of 12 BP 53 \pm\$

Bottom laterals 4 bulb \( \text{L} \text{ 8x3\frac{1}{2} x 16.0 \pm\$-1 web \( \text{L} \text{ 15 x \frac{3}{8}} \)

Stringers 24 WF 76 \pm\$

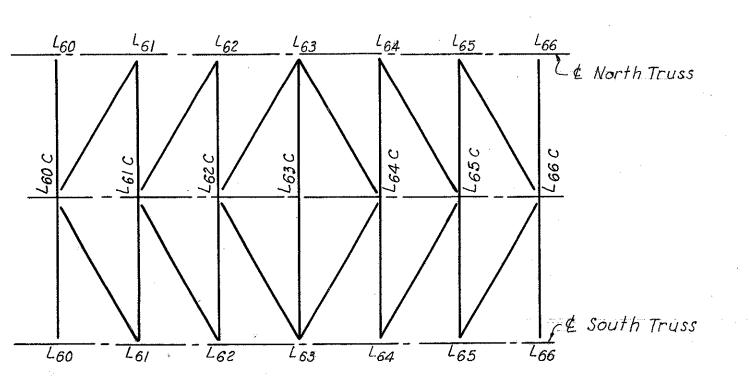
Floorbeams 36 WF 150 \pm\$

Bottom lateral struts 2 \( \text{L} \text{ 15 x 33.9} - 2 \cdot \text{Rs. 13 x \frac{5}{16}} \)

For the distance from the roadway surface to the working line of the truss top chords at each panel point, see the table of Grades and Elevations, Sheet 12.

For truss sections and details see Sheets 77 to 79 inclusive. Posts at ends of unit are vertical; other posts are normal to top chord as shown.

For typical top lateral hanger, see Sheets 28 and 35.



BOTTOM CHORD LATERAL BRACING

Scale: \( \lambda'' = 30\forall \textit{O''} \)

PART 3

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42 R-17 5

FRAMING PLAN - UNIT 6

CUYAHOGA COUNTY

SCALE *AS Shown*MADE *R. K.* DATE 7-12-54

TRCD*GK &A.H.* DATE 8-13-54

CKD *D. M. D.* DATE 9-30-54

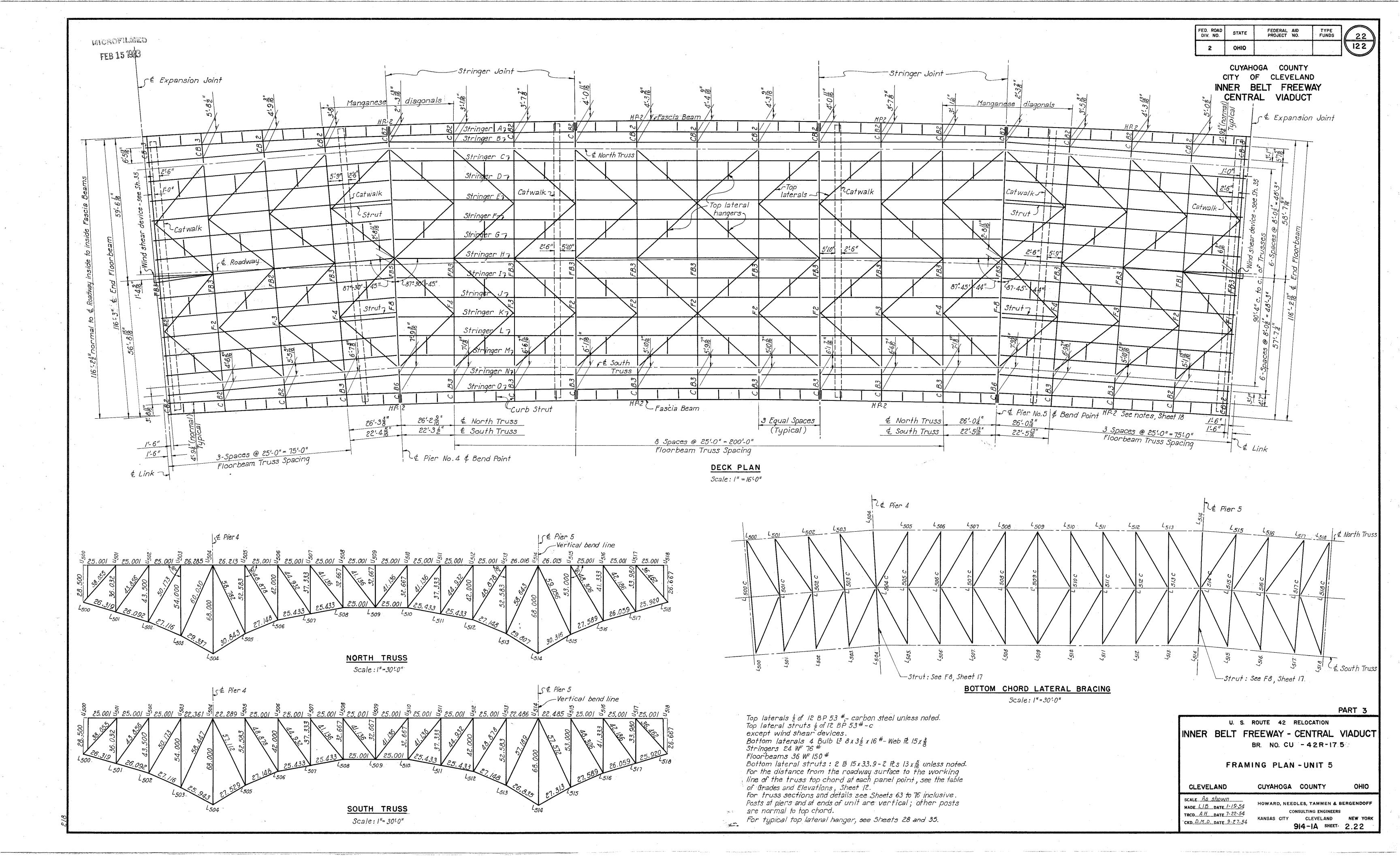
CLEVELAND

HOWARD, NEEDLES, TAMMEN & BERGENDOFF

CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK

914-14 SHEET 2.23



оню CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT Stringer Joint & Expansion Joint Stringer"A" E North Truss |laterals Top lateral hangers Stringer "F" A Roadway Stringer"H" Stringer "K"-Stringer"L"-Stringer W" Stringer "O" Curb Struts Fascia Beam\_ HP 2 See notes Sheet 18 3 equal spaces typical 8 Spaces @ 25'-0" = 200'-0" Floor Beam Truss Spacing DECK PLAN
Scale: |"=|6'-0" TRUSSES Scale: [ 30'-0" All top laterals tof I2BP53#
Bottom laterals 4bulb & 8x3t x 16.0#-Web Pl. 15x &
Stringers 24WF76#
Floorbeams 36WF150# £ North Truss L42 L43 L44 Bottom lateral struts: 2 8 15 x 33. 9-2 Pls. 13 x 16 For the distance from the roadway surface to the working line of the truss top chord at each panel point, see the table of Grades and Elevations, Sh. 12. For truss sections and details see Sheets 58 to 62 inclusive.

Posts at ends of unit are vertical; other posts are normal to top chord. U. S. ROUTE 42 RELOCATION For typical top lateral hanger, see Sheets 28 and 35. INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R-17.5 £ South Truss FRAMING PLAN-UNIT 4

BOTTOM CHORD LATERAL BRACING

Scale: | "=30"-0"

47

MICHOFILMED

FEB 15 (483)

FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. TYPE FUNDS

PART 3

CUYAHOGA COUNTY

HOWARD, NEEDLES, TAMMEN & BERGENDOFF CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK

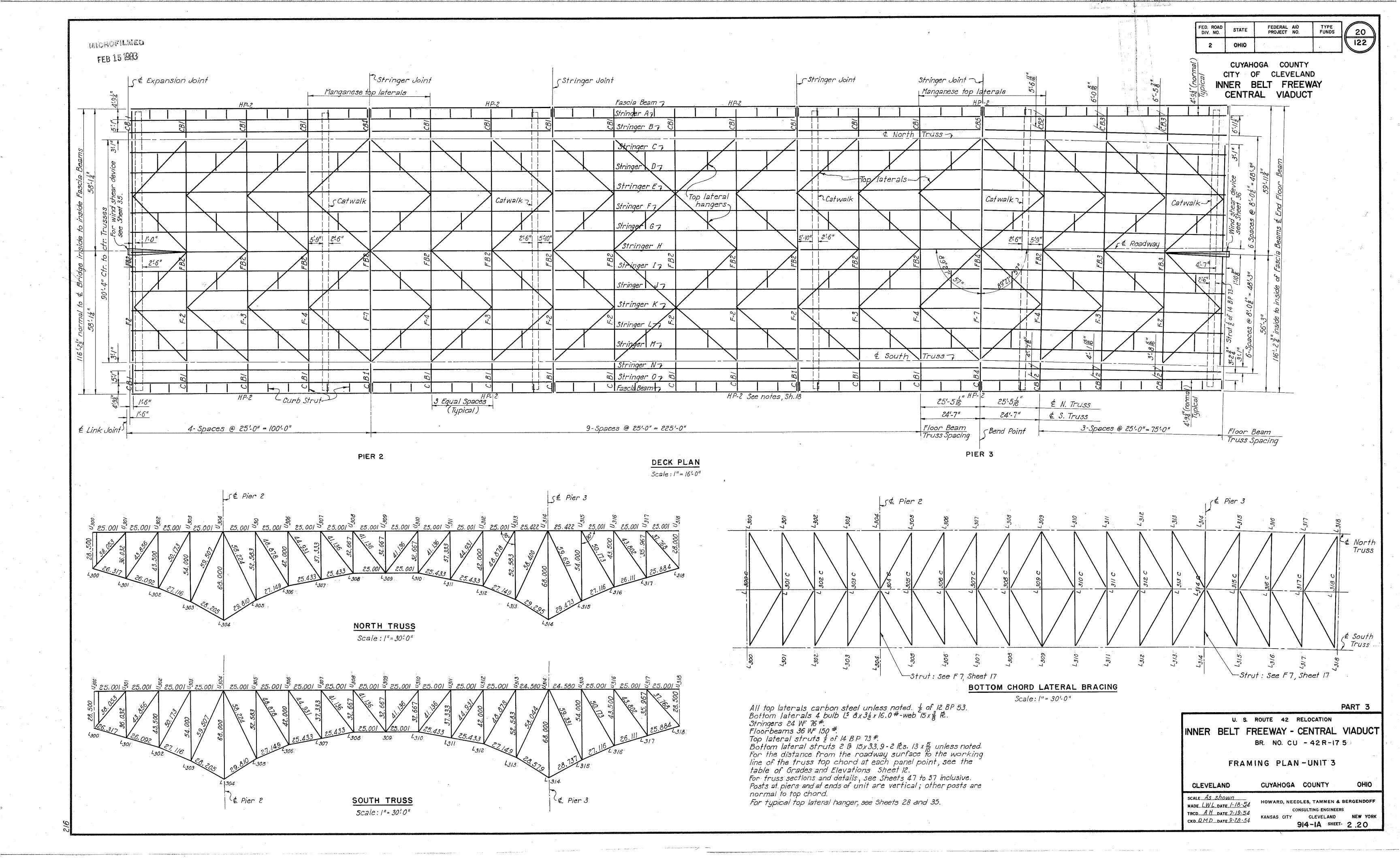
914-1A SHEET 2.21

CLEVELAND

SCALE 35 Shown MADE LLD DATE

TRCD BJ.R. DATE 6-8-54

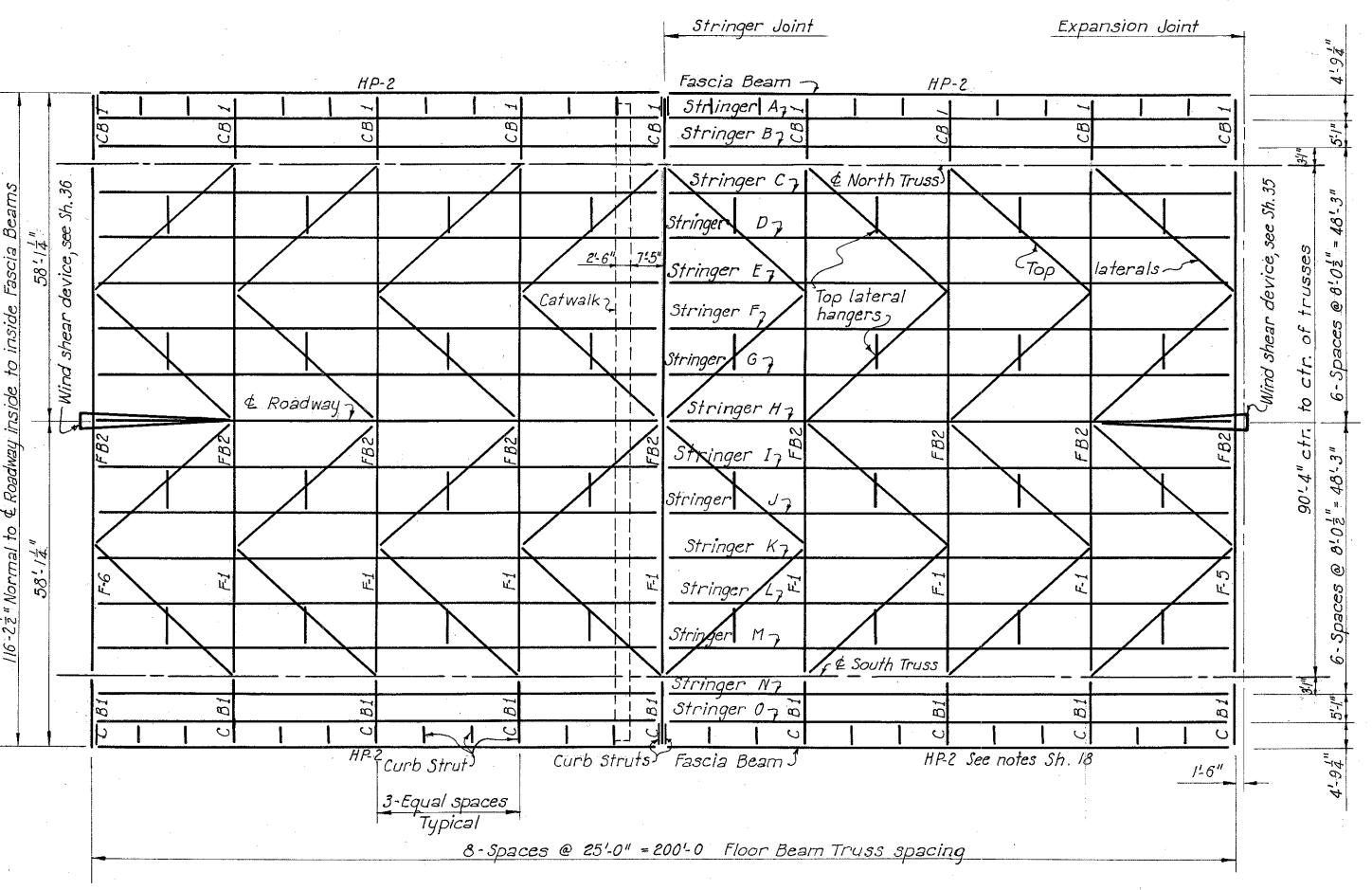
CKD D.M.D. DATE 9-30-54



MICROPILMED
FEB 15 MG

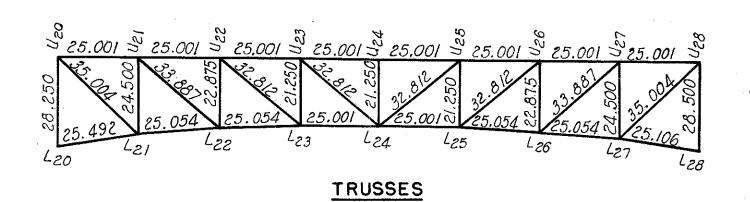
FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	19
2	оню			122

CUYAHOGA COUNTY
CITY OF CLEVELAND
INNER BELT FREEWAY
CENTRAL VIADUCT



DECK PLAN

Scale: \( \frac{1}{16} \) = \( \frac{1}{1} - 0 \) "



Scale: |"= 30'0"

Top laterals \$\frac{1}{2}\$ of 12 BP 53 #

Bottom laterals 4 bulb \$\frac{15}{2} \text{ 8} x 3\frac{1}{2} x 16.0 # - web \$\mathbb{R}\$. \$15 x \frac{3}{8}\$.

Stringers 24 WF 76 #

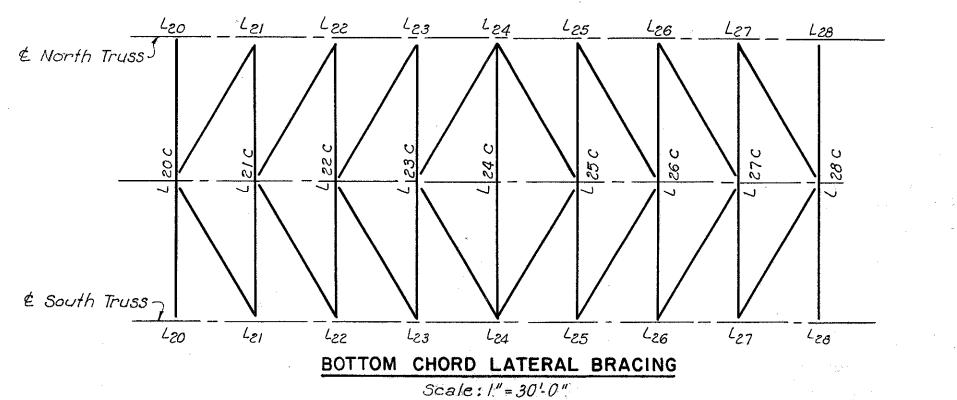
Floorbeams 36 WF 150 #

Bottom lateral struts 2 \$\mathbb{E}\$ | 5 x 33.9 - 2 \$\mathbb{R}\$. \$13 x \frac{5}{16}\$.

Working line of truss top chord is 4'-4\frac{1}{2}" below roadway surface. See the table of grades and Elevations, Sheet 12.

For truss sections and details, see Sheets 44 to 46 Posts at ends of unit are vertical; other posts are normal to top chord.

normal to top chord. For typical top lateral hanger, see Sheets 28 and 35.



U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU : - 42 R-17.5

FRAMING PLAN - UNIT 2

CLEVELAND CUYAHOGA COUNTY

scale As shown

MADE FG DATE 1-14-54

TRCD GK AH DATE 7-27-54

CKD D.M.D. DATE 9-30-54

KANSAS CI

CONSULTING ENGINEERS

KANSAS CITY CLEVELAND NEW YORK

914-1A SHEET- 2.19

MICAGFILMED FEB 15 (SQ) \_Stringer Joint Stringer Joint Stringer Joint Two 2" conduits. See Sheet 122. Manganese top laterals Fascia Beam - Strlinger Az -S strlinger B7 S Stringer C7 & North Truss 5'9" 2'6" Stringer D7 Stringer E -Top laterals Catwalk s Cat walk Catwalk -(Top lateral hangers Stringer Gy 1 Stringer H-/ £ Roadway -Stirilnger Stringer K-1 Stringer ! & South Truss Stryinger 070 10 Fascia Beam -Curb Strut) 3-Equal spaces (Typical) ⊈ Expansion Joint rt Bearing and & Pier \_\_ West End Pier ¢ Pier 1 9-Spaces @ 25'-0" = 225'-00" Floorbeam Truss Spacing 4- Spaces @ 25'-0" = 100'-0" DECK PLAN Scale: 1 = 1.0" . € Bearing West End. Pier € North Truss  $\frac{1}{2}$  25.001   South Truss

→ t Pier 1

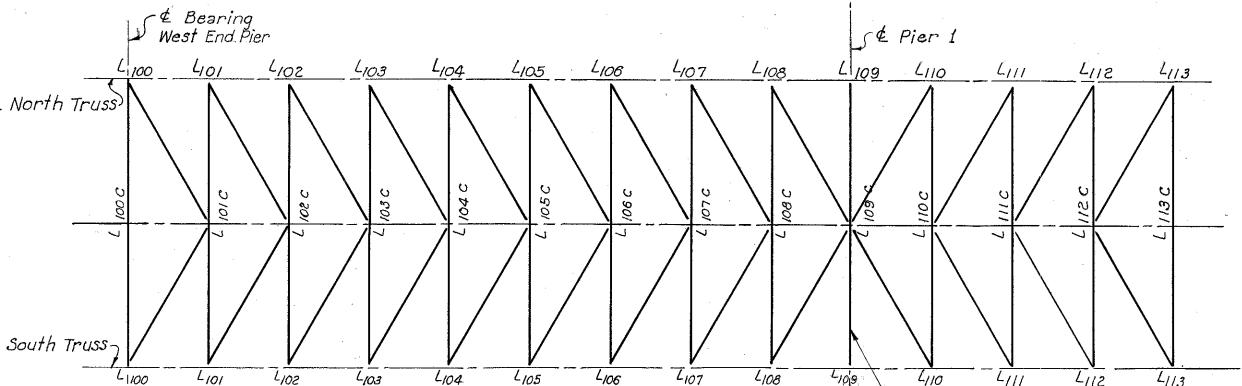
For 15" channel framing at expansion joints see Roadway Expansion Joints.
For 13" channel framing at contraction joints see Roadway Drains Type B and Slab Plans.

TRUSSES

Scale: 1" = 30'-0"

FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. TYPE FUNDS STATE 122 OHIO

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT



BOTTOM CHORD LATERAL BRACING Scale: |" = 30'-0"

Top laterals \$ of 12 BP 53 #, carbon steel unless noted.

Bottom laterals 4 bulb LS 8x3 \( \frac{1}{2} \) x 16.0 # - Web R. 15 x \( \frac{3}{8} \)

Stringers 24 WF 76 #

Floorbeams 36 WF 150 #

Bottom lateral struts 2 \( \bar{1} \) 15 x 33.9 - 2 Rs. 13 x \( \frac{5}{16} \) unless noted.

The working line of the truss top chord is 4'-4\( \frac{1}{2} \) below the

roadway surface. See the table of Grades and Elevations ,

Sheet 12. For truss sections and details, see Sheets 38 to 43 inclusive. Posts at piers and at ends of unit are vertical; other posts are

normal to top chord. Handrail posts to be located at floorbeams and at third points between floorbeams. Posts not marked HP-2 (light pole support) will be HP-1. See Sheet 99.

For typical top lateral hanger, see Sheets 28 and 35.

PART 3 U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. QUY - 42 R-17.50

FRAMING PLAN - UNIT I

CLEVELAND

SCALE As shown

MADE W E G DATE /-/9-54

TRCD. # AH DATE 7-28-54

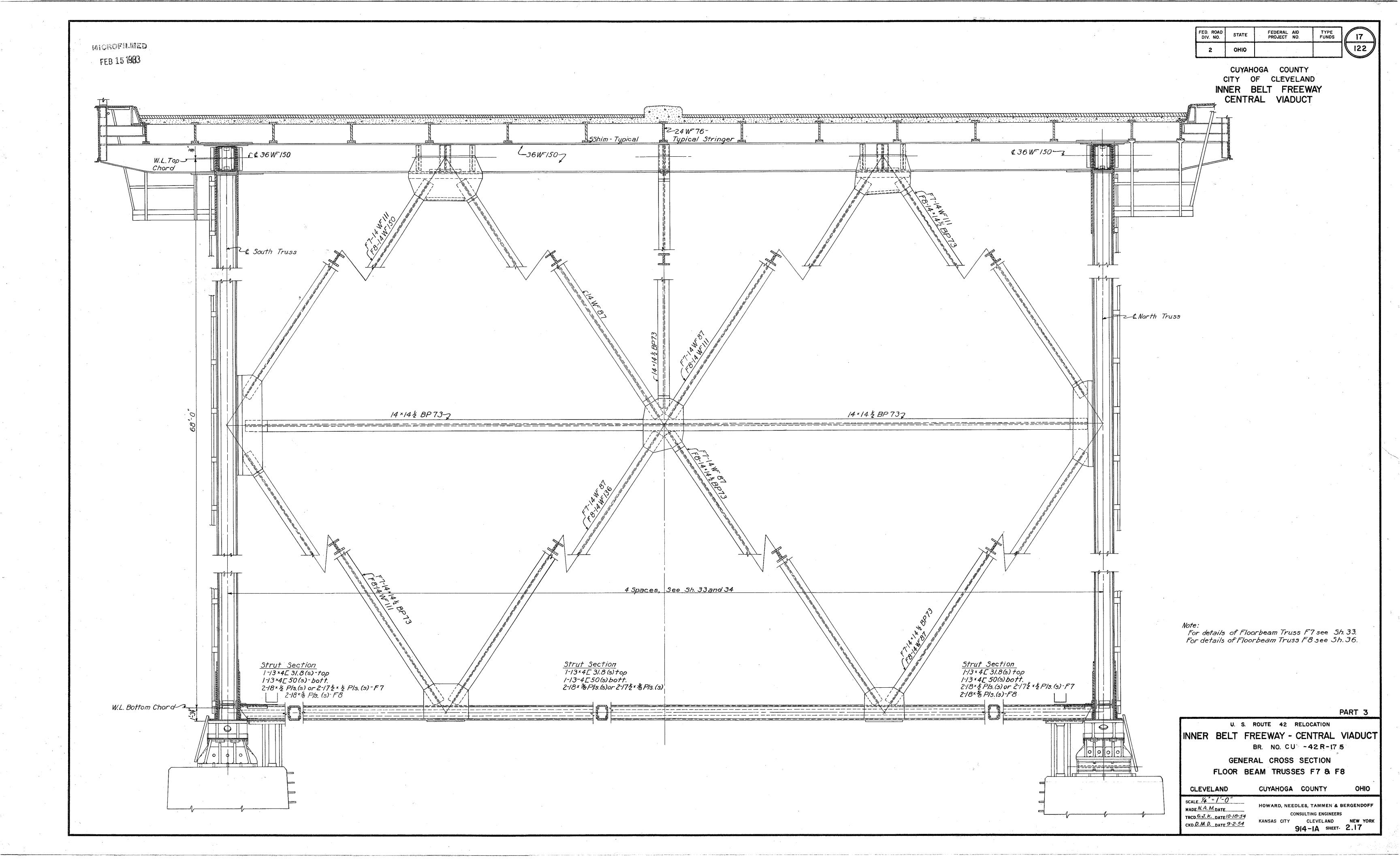
CKD D.M.D. DATE 9-24-54

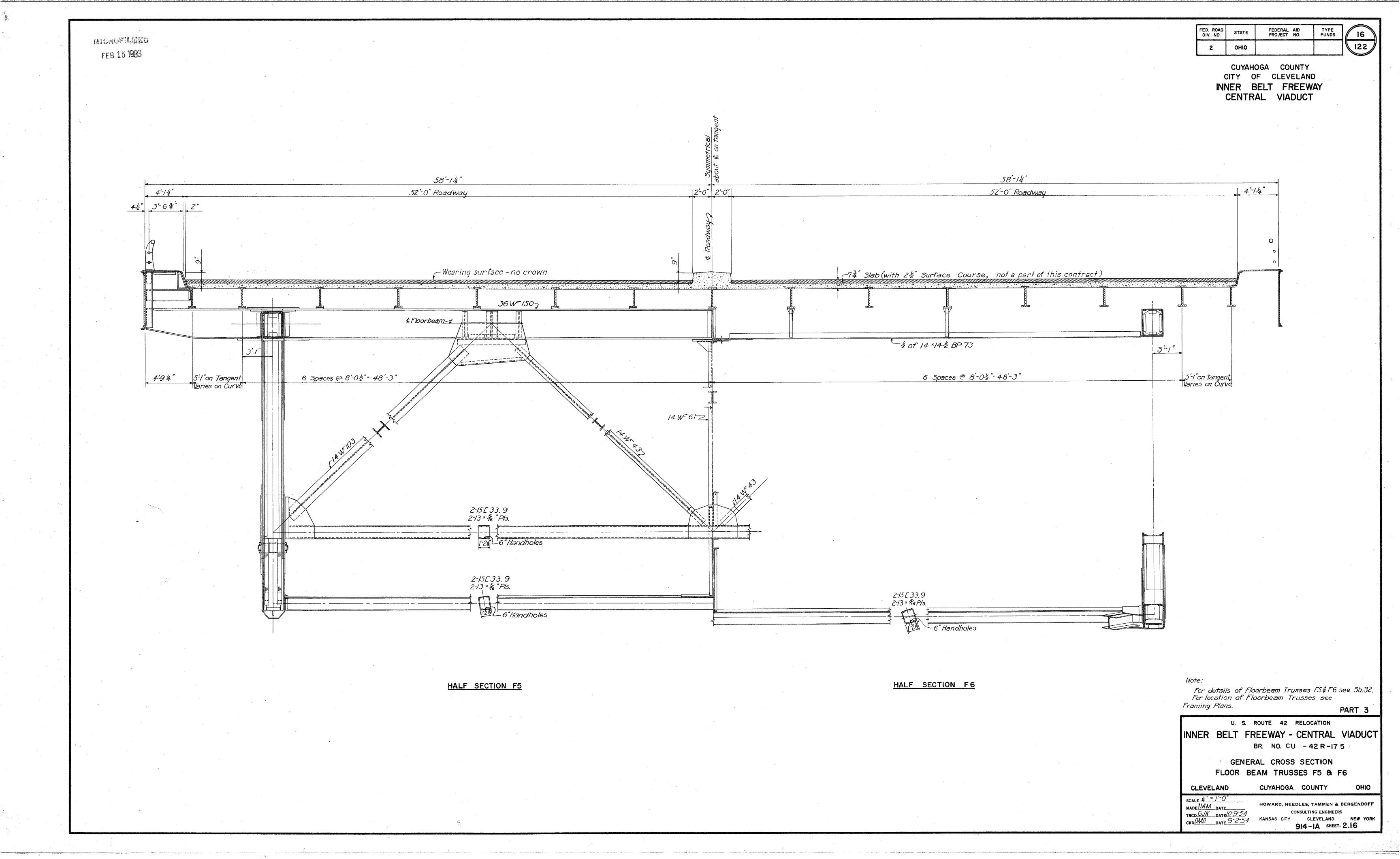
Strut: See F7, Sheet 17

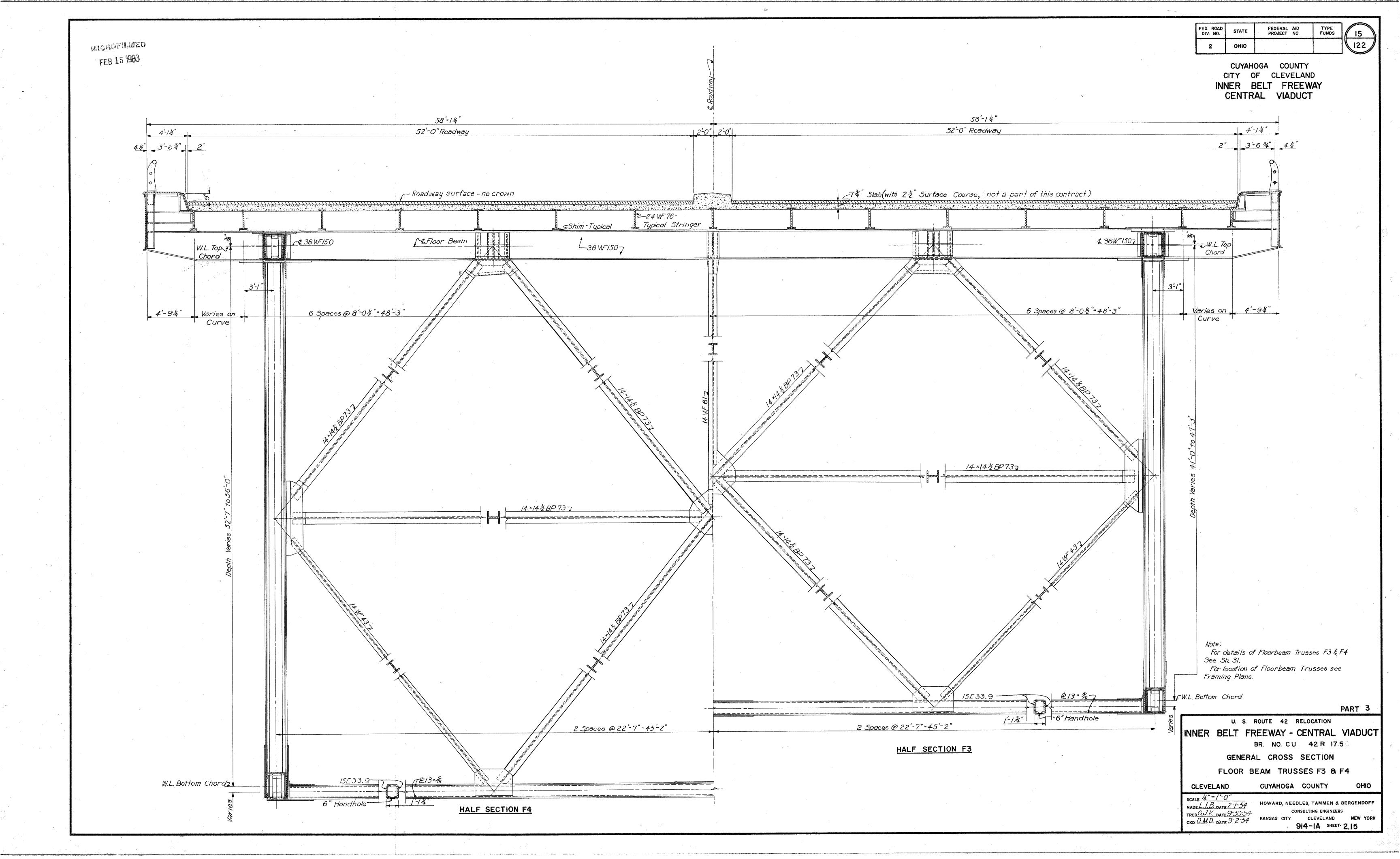
CUYAHOGA COUNTY

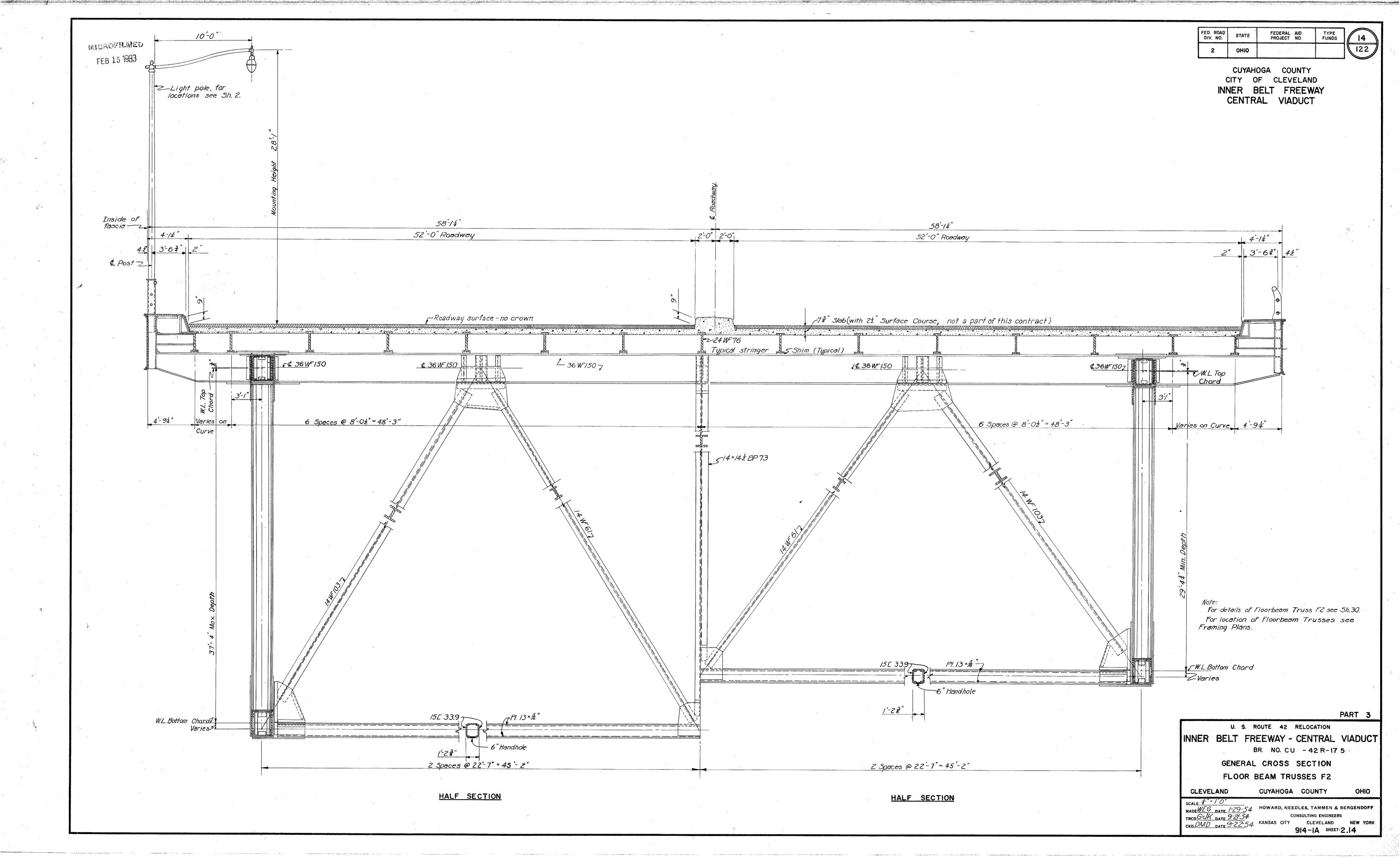
HOWARD, NEEDLES, TAMMEN & BERGENDOFF

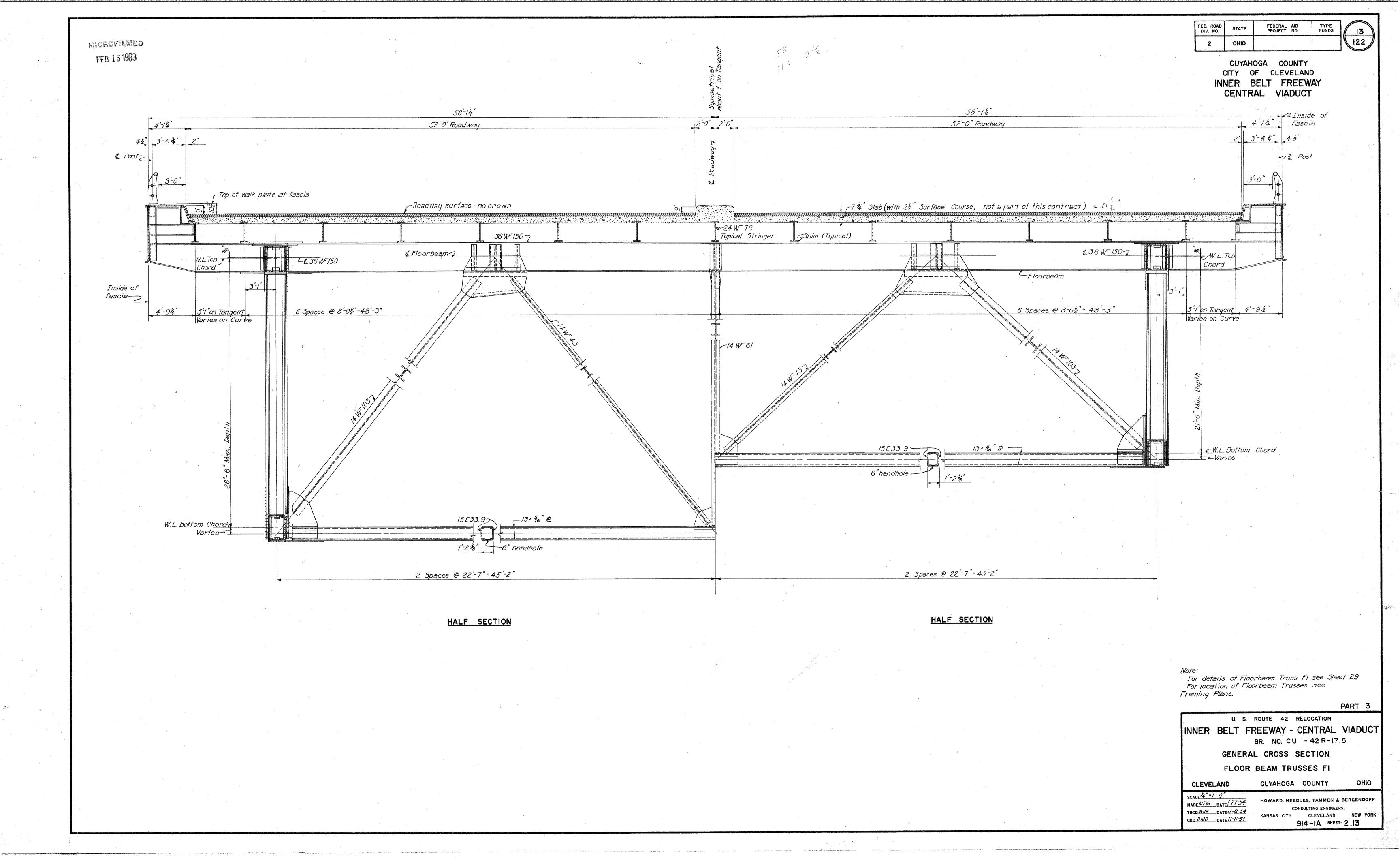
CONSULTING ENGINEERS CLEVELAND NEW YORK 914-1A SHEET 2.18

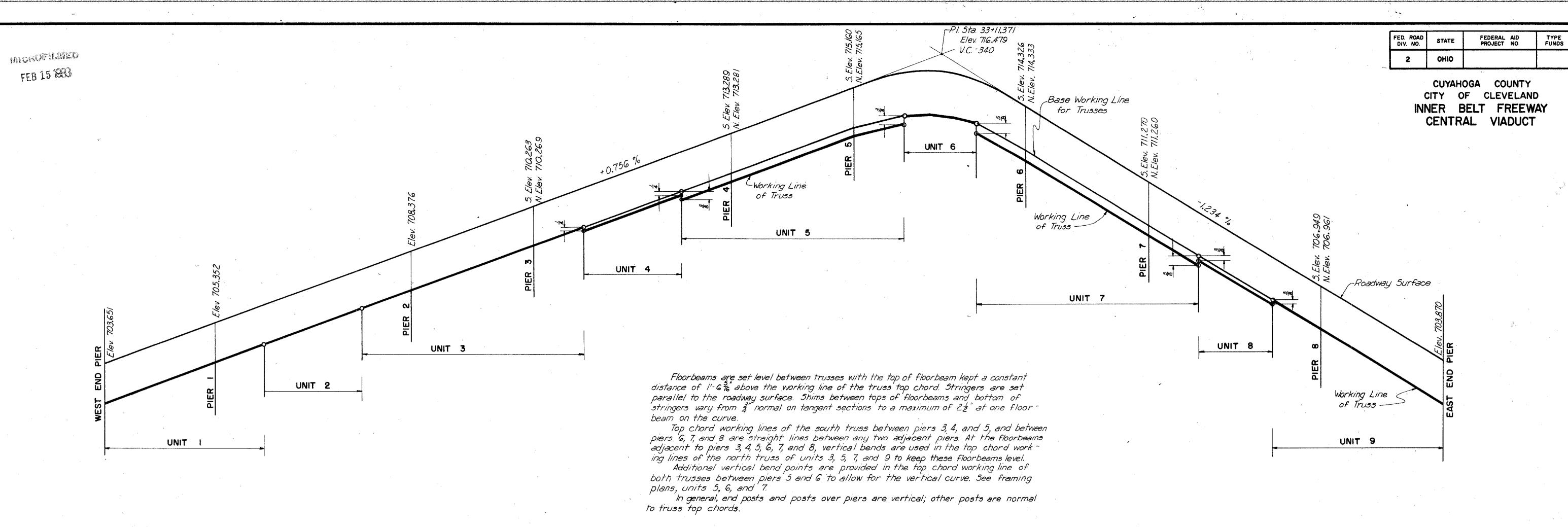












PIER	PANEL POINT	ELEVATION W.L. OF TRUSS	ELEVATION ROADWAY SURFACE NORTH TRUSS	DISTANCE R.S. TO W.L. OF NORTH TRUSS	ELEVATION ROADWAY SURFACE SOUTH TRUSS	DISTANCE R. S. TO W.L. OF SOUTH TRUSS
W. End Pier	100	699.274	703.651	4.377	703.651	4.377
	101	699.463	703.840	4.377	703.840	4.377
	102	699.652	704.029	4.377	704.029	4.377
	103	699.841	704.218	4.377	704.218	4.377
	104	700.030	704.407	4.377	704.407	4.377
	105	700.219	704.596	4.377	704.596	4.377
	106	700.408	704.785	4.377	704.785	4.377
	107	700.597	704.974	4.377	704.974	4.377
Ī	108	700.786	705.163	4.377	705.163	4.377
Pier I	109	700.975	705.352	4.377	705.352	4.377
	110	701.164	705.541	4.377	705.541	4.377
	111	701.353	705.730	4.377	705.730	4.377
· ·	112	701.542	705.919	4.377	705.919	4.377
	20	701.731	706.108	4.377	706.108	4.377
	21	701.920	706.297	4.377	706.297	4.377
	22	702.109	706.486	4.377	706.486	4.377
	23	702.298	706.675	4.377	706.675	4.377
	24 }	702.487	706.864	4.377	706.864	4.377
	25	702.676	707.053	4.377	707.053	4.377
	26	702.865	707.242	4.377	707.242	4.377
	27	703.054	707.431	4.377	707.431	4.377
F	28	703.243	707.620	4.377	707.620	4.377
					ŕ	
	300	703.266	707.643	4.377	707.643	4.377
	301	703.432	707.809	4.377	707.809	4.377
	302	703.621	707.998	4.377	707.998	4.377
Ì	303	703.810	708.187	4.377	708.187	4.377
Pier 2	304	703.999	708.376	4.377	708.376	4.377
Ţ	305	704.188	708.565	4.377	708.565	4.377
. [	306	704.377	708.754	4.377	708.754	4.377
	307	704.566	708.943	4.377	708.943	4.377
	308	704.755	709.132	4.377	709.132	4.377
	309	704.944	709.321	4.377	709.321	4.377
,	310	705.133	709.510	4.377	709.510	4.377

	<u> </u>		ELEVATION	DISTANCE	ELEVATION	DISTANCE
PIER	PANEL	ELEVATION W.L. OF TRUSS	ROADWAY SURFACE NORTH TRUSS	R. S. TO W.L. OF NORTH TRUSS	ROADWAY SURFACE SOUTH TRUSS	R.S. TO W.L. OF SOUTH TRUSS
	311	705.322		4.377		
	312	705.522	709.699 709.888	4.377	709.699 709.888	4.377 4.377
	313	705.700	710.077	4.377	710.077	4.377
Pier 2	314	705.700	710.269	4.383	710.263	4.377
Pier 3	315	706.073	710.462	4.389	710.449	4.376
	316	706.264	710.650	4.386	710.638	4.374
	317	706.454	710.839	4.385	710.827	4.373
	40	706.624	711.028	4.404	711.016	4.392
		† ·····	711.028	4.402	711.205	4.390
	41	706.815	711.404	4.402	711.396	4.390
	43 44	707.196	711.591	4.395 4.392	711.588	4.392 4.393
	45	707.577	711.965	4.388	711.971	4.394
•	46	707.767	712.152	4.385	712.162	4.395
	47	707.958	712.338	4.380	712.353	4.395
	48	708.148	712.525	4.377	712.545	4.397
	500	708.161	712.547	4.386	712.568	4.407
	501	708.329	712.712	4.383	712.736	4.407
	502	708.519	712.899	4.380	712.927	4.408
	503	708.710	713.085	4.375	713.118	4.408
Pier 4	504	708.881	713.281	4.400	713.289	4.408
	505	709.051	713.477	4.426	713.459	4.408
	506	709.242	713.664	4.422	713.650	4.408
	507	709.433	713.850	4.417	713.841	4.408
	508	709.624	714.037	4.413	714.032	4.408
	509	709.815	714.224	4.409	714.224	4.409
	510	710.006	714.410	4.404	714.415	4.409
	511	710.198	714.597	4.399	714.606	4.408
	512	710.389	- 714.784	4.395	714.797	4.408
	513	710.580	714.971	4.391	714.988	4.408
Pier 5	514	710.752	715.165	4.413	715.160	4,408
	515	710.865	715.345	4.480	715.322	4.457
	516	710.990	715.482	4.492	715.467	4.477

PIER	PANEL POINT	ELEVATION W.L. OF TRUSS	ELEVATION ROADWAY SURFACE NORTH TRUSS	DISTANCE R. S. TO W.L. OF NORTH TRUSS	ELEVATION ROADWAY SURFACE SOUTH TRUSS	DISTANCE R.S. TO W.L. OF SOUTH TRUSS
	517	711.115	715.584	4.469	715.575	4.460
	518	711.225	715.642	4.417	715.636	4.411
	60	711.271	715.650	4.379	715.646	4.375
	61	711.284	715.680	4.396	715.679	4.395
	62	711.298	715.674	4.376	715.675	4.377
	63	711.239	715.633	4.394	715.633	4.394
	64	711.179	715.556	4.377	715.554	4.375
	65	711.046	715.444	4.398	715.437	4.391
	66	710.913	715.295	4.382	715.283	4.370
	701	710.614	715.111	4.497	715.092	4.478
	702	710.367	714.891	4.524	714.863	4.496
	703	710.119	714.636	4.517	714.597	4.478
Pier 6	704	709.897	714.333	4.436	714.326	4.429
	705	709.616	714.017	4.401	714.046	4.430
	706	709.304	713.712	4.408	713.734	4.430
	707	708.992	713.407	4.415	713.422	4.430
	708	708.680	713.102	4.422	713.110	4.430
	709	708.368	712.798	4.430	712.798	4.430
	710	708.056	712.493	4.437	712.485	4.429
	711	707.744	712.188	4.444	712.473	4.429
	712	707.432	711.883	4.451	711.861	4.429
	713	707.120	711.578	4.458	711.549	4.429
Pier 7	714	706.841	711.260	4.419	711.270	4.429
	715	706.562	710.940	4.378	710.991	4.429
	716	706.250	710.636	4.386	710.679	4.429
	717	705.939	710.331	4.392	710.367	4.428
	718	705.665	710.063	4.398	710.092	4.427
	80	705.649	710.026	4.377	710.055	4.406
	81	705.337	709.721	4.384	709.743	4.406
	82	705.026	709.416	4.390	709.430	4.404
	83	704.714	709.111	4.397	709.118	4.404
	84	704.403	708.806	4.403	708.806	4.403

PIER	PANEL POINT	ELEVATION W.L. OF TRUSS	ELEVATION ROADWAY SURFACE NORTH TRUSS	DISTANCE R.S. TO W.L. OF NORTH TRUSS	ELEVATION ROADWAY SURFACE SOUTH TRUSS	DISTANCE R.S. TO W.L. OF SOUTH TRUSS
	85	704.092	708.501	4.409	708.493	4.401
·	86	703.780	708.196	4.416	708.181	4.401
	-					
	901	703.500	707.891	4.391	707.869	4.369
	902	703.188	707.584	4.396	707.560	4.372
	903	702.877	707.275	4.398	707.251	4.374
Pier 8	904	702.572	706.961	4.389	706.949	4.377
	905	702,269	706.646	4.377	706.646	4.377
	906	701.961	706.338	4.377	706.338	4.377
	907	701.652	706.029	4.377	706.029	4.377
	908	701.344	705.721	4.377	705.721	4.377
,	909	701.035	705.412	4.377	705.412	4.377
	910	700.727	705.104	4.377	705.104	4.377
	911	700.418	704.795	4.377	704.795	4.377
	912	700,110	704.487	4.377	704.487	4.377
j	913	699.801	704.178	4.377	704.178	4.377
. End Pier	914	699.493	703.870	4.377	703.870	4.377

PART 3

U. S. ROUTE 42 RELOCATION

INNER BELT FREEWAY - CENTRAL VIADUCT

BR. NO. CU - 42R-175

GRADES AND ELEVATIONS

CLEVELAND CUYAHOGA COUNTY OHIO

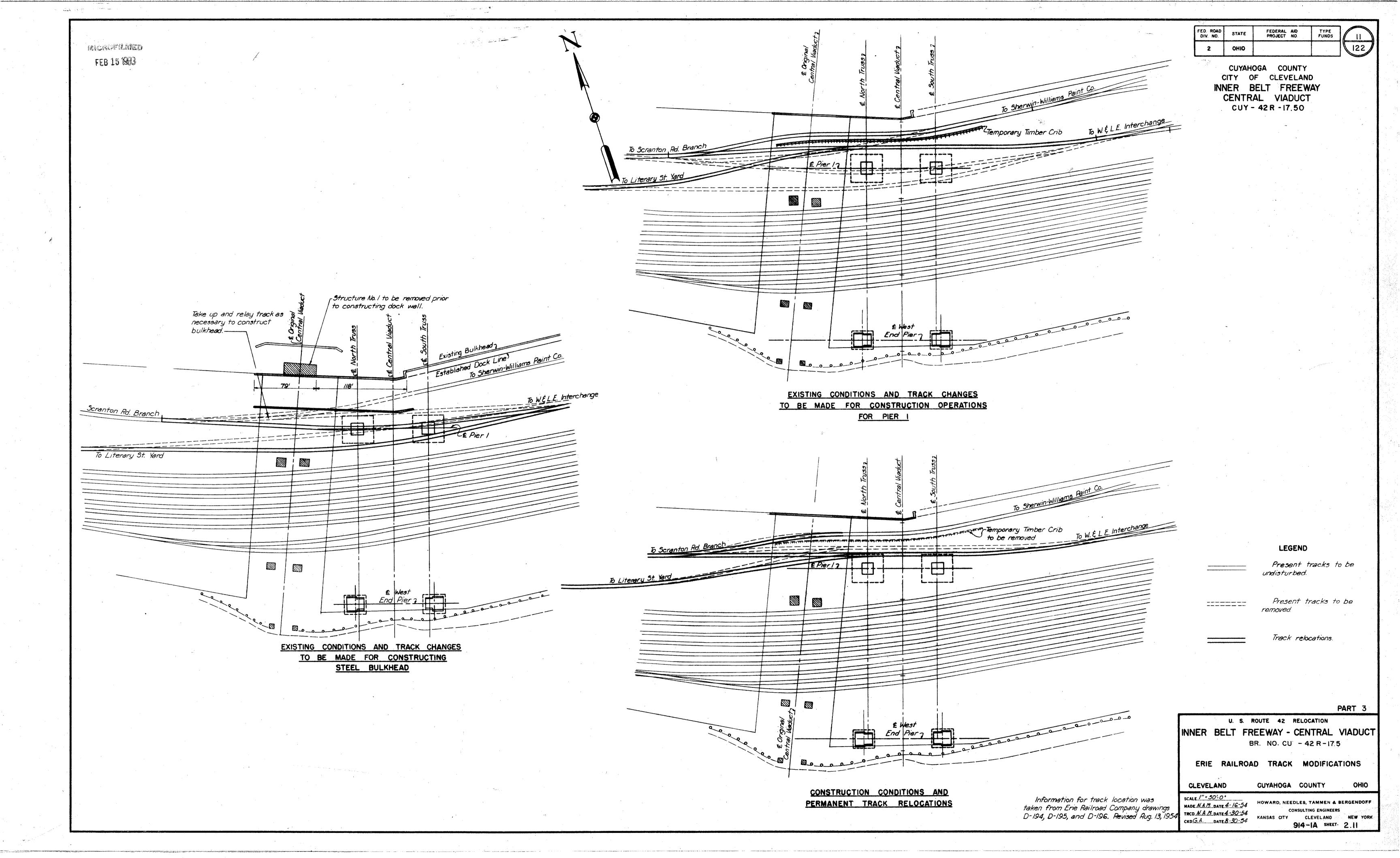
MADE NAME DATE 4-15-54
TRCD DATE
CKD C.J.C. DATE 4-29-54

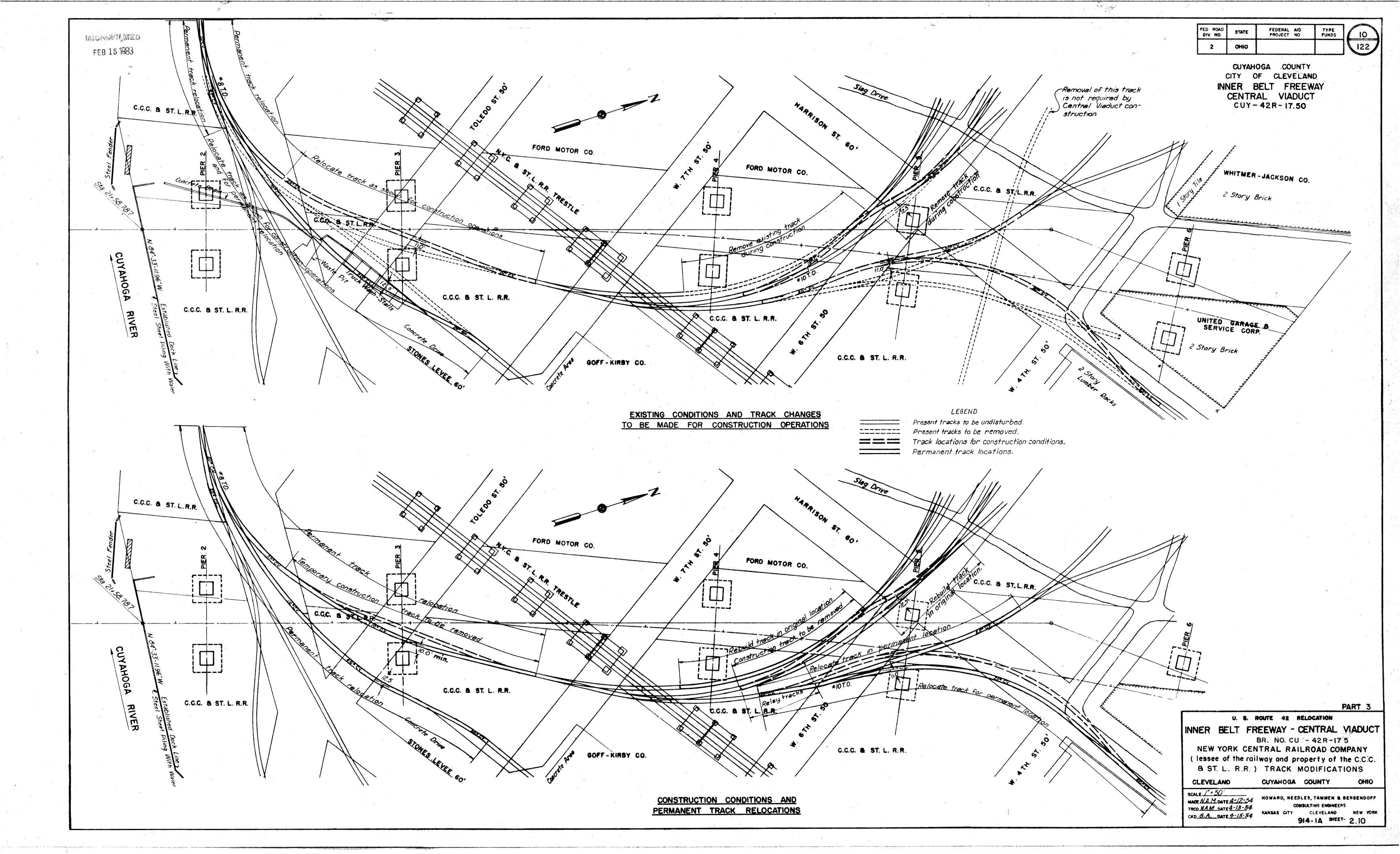
HOWARD, NEEDLES, TAMMEN & BERGENDOFF

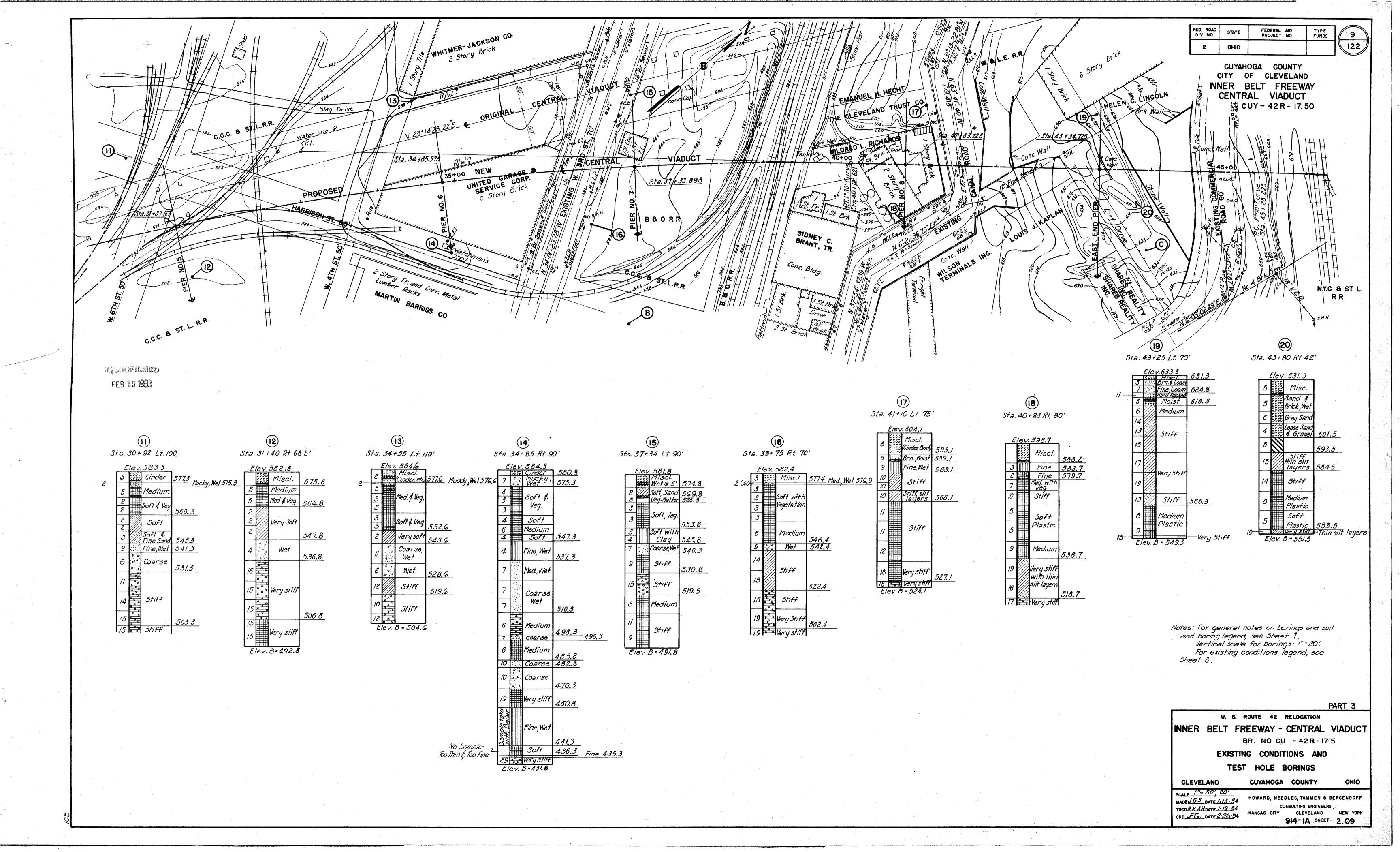
CONSULTING ENGINEERS

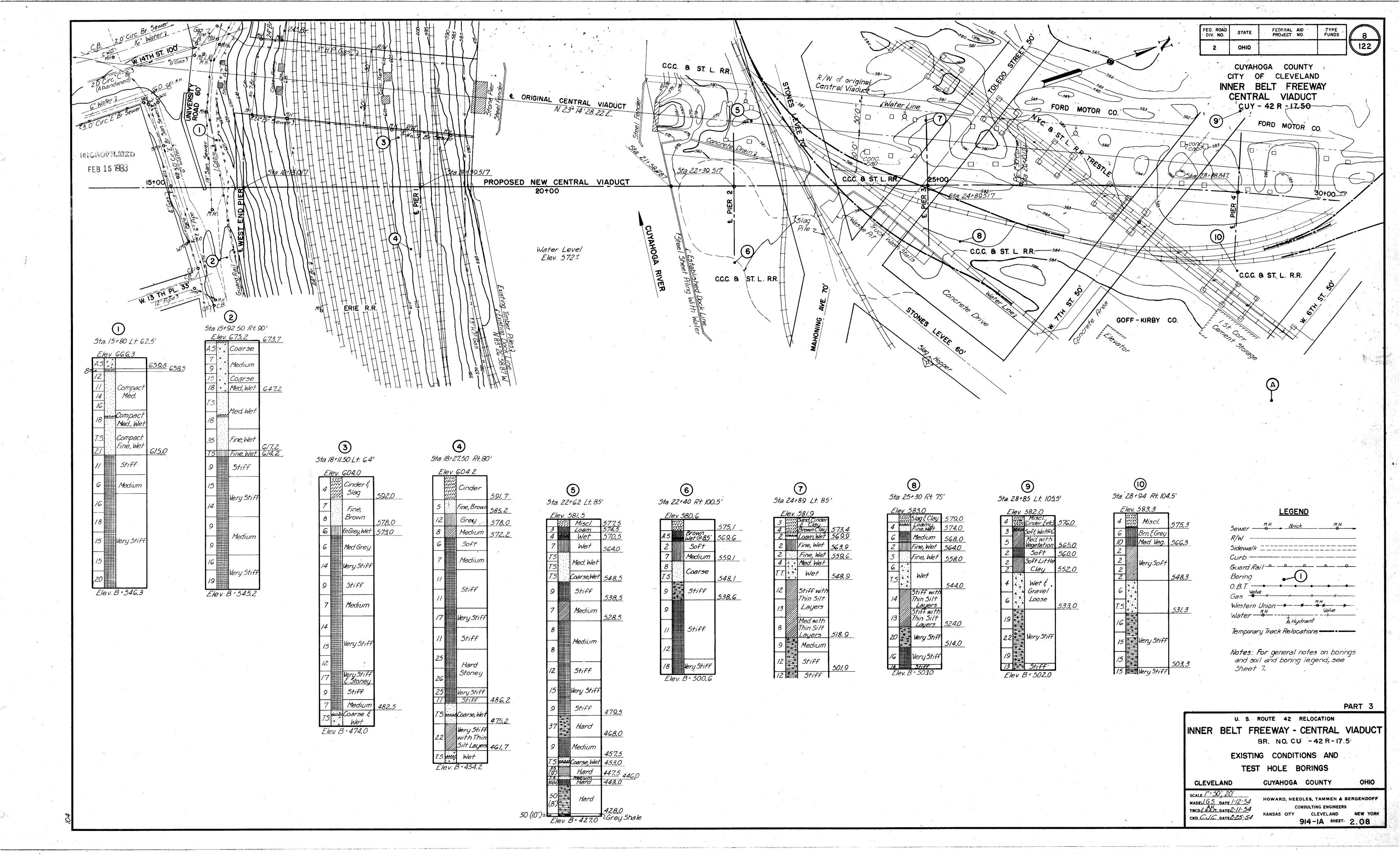
KANSAS CITY CLEVELAND NEW YORK

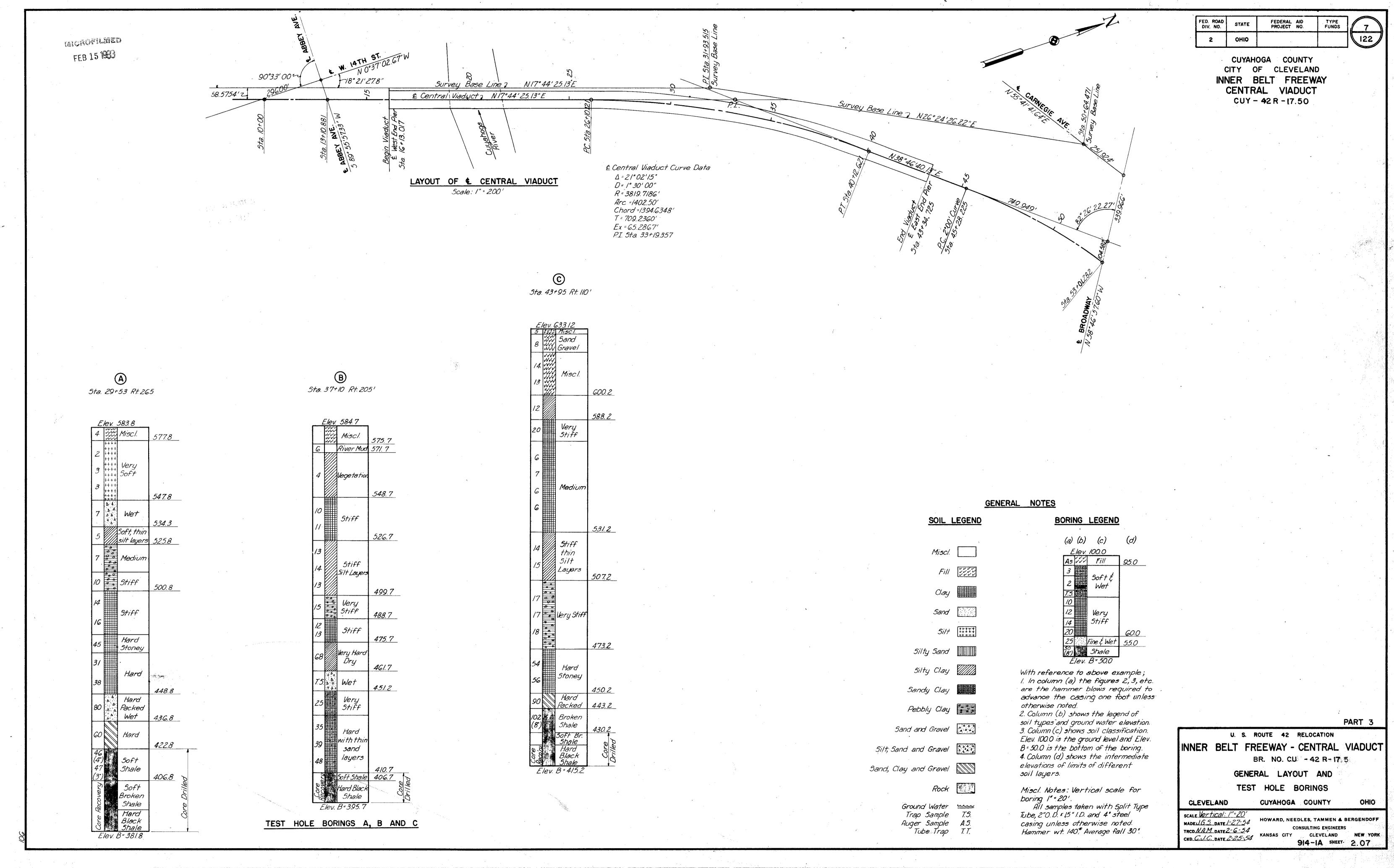
914-1A SHEET 2.12











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FED. ROAD DIV. NO.	STATE	FEDERAL AID PROJECT NO.	TYPE FUNDS	6
2	оню			122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY
CENTRAL VIADUCT

ITEM	DESCRIPTION	TOTAL	UNIT	PROJECT IN GENERAL	STIMATE	UNIT 2	UNIT 3	UNIT 4	UNIT 5	UNIT 6	UNIT 7	UNIT 8	UNIT 9	AS BUILT
S-1·	Class "C" Concrete	7,280.1	Cu. Yds.		869.5	540.1	1,197.9	540.2	1,186.0	409.7	1,189.7	405.8	941.2	
S -4	Reinforcing Steel	2,324,480	Pounds		279,192	170,930	383,408	171,730	378,565	129,320	382,258	128,565	300,512	
S-7	Structural Carbon Steel	15,011,600 <del>15,000,000</del>	Pounds		1,790,000	1,080,000	2,470,000	1,060,000	2,610,000	840,000	2,460,000	830,000	1,860,000	C-10,-18,520 C-1,+30,120
S – 7 ‡ Special	Structural Manganese Steel	9,594,001 9,660,000	Pounds		1,130,000	640,000	1,990,000	620,000	1,770,000	310,000	1,680,000	: 310,000	1,210,000	C-10,-88,664 C-4,+22,665 9,594,001
5-8	Field Painting Structural Steel and Drainage System	25,646,771 - <del>25,733,000</del>	Pounds		3,080,000	1,765,000	4,670,000	1,725,000	4,580,000	1,152,000	4,350,000	1,181,000	3,230,000	C-19-86,229 Z5, 646,771
S-9	Copper Water Stops including 1" hot poured joint sealer, Sec. M-10.23	2,592	Lin.Ft.	,	324	108	540	108	432	108	540	108	324	
S-9	1" Preformed Gray Rubber Expansion Joint Filler, Sec.M-10.02	73.2	Sq.Ft.		6.1	6.1	12.2	6.1	12.2	6.1	12.2	6.1	6.1	
S-14	Handrail (Aluminum)	5,404	Lin. Ft.		633.4	403.0	897.0	403.0	887.6	303.0	890.6	303.0	683.4	
SS-24	Walkway grating	8,225	Sq. Ft.		1,,275	. 350	1,610	265	1,600		1,600	265	1,260	
S - 25	Roadway Lighting System , Part A	1	Lump Sum	1	1 1			.4	, ; *	<i>,</i>				
S-25	Roadway Lighting System, Part B	1	Lump Sum	1										
S –25	Navigation Lights	1	Lump Sum	1										
S-25	Electrical Grounds	1	Lump Sum	1			,		,					
S-29	Copper Tubes for Sub-drainage Wearing Surface Course		Each		108	<i>36</i>	126	36	126	36	126	36	108	
S-29	Roadway Drainage System	1,093,955 1,073,000	Pounds		160,000	45,000	210,000	45,000	200,000	2,000	210,000	41,000	160,000	C-10, +20,955 1,093,955
							,							
	•													

<sup>\*</sup> See General Notes, Sheet 4, paragraph 8, for items included for payment.

\*\* \* See General Notes, Sheet 5, paragraph 6, for division of items for payment.

\*\* \* \* See General Notes, Sheet 4, paragraph 7, for items included for payment.

(1) No State \*\* \*\* participation.

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42R-175

ESTIMATED QUANTITIES

CLEVELAND CUYAHOGA COUNTY

SCALE

MADE NAIM DATE 6-1-54

TRCD AH DATE 4-13-55

CKD GA DATE 4-20-55

CONSULTING ENGINEERS
KANSAS CITY CLEVELAND NEW YORK
914-1A SHEET-2.06

GENERAL

## FED. ROAD DIV. NO. FEDERAL AID PROJECT NO. 122

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT

# GENERAL NOTES, CONTINUED

The steel shaft of the lighting standard shall be fabricated from not less than #11 manufacturers' standard gauge. The shaft shall be formed and welded with only one longitudinal. automatically electrically welded joint and shall have no horizontal joints or welds. The weld shall be of full penetration. After forming and welding, the tapered shaft shall be cold rolled or worked under sufficient pressure to flatten out the weld, to increase the elastic limit of the metal in the completed shaft, and to produce a true tapered tube without flat spots and a circular cross-section throughout the length of the shaft. If the shaft is fabricated by means of a brake or other process which does not utilize the cold rolling principle, it shall be fabricated from a steel sheet having a thickness of #7 manufacturers\*

Each standard shall have a mast or bracket arm ten feet in length made of standard pipe of the size shown on the plans. The inner end of the bracket shall be welded to a cast steel head block so designed that the block can be boilted through a cast iron neck piece to a plate welded to the top of the pole to permit radial adjustment of the bracket arm. Provisions shall be made to permit passage of the concealed wires to bracket arm. The ornamental casting welded to the outer end of the bracket shall be arranged with a leveling device or "Plumbizer" for adjustment of a pendant lighting fixture and shall be tapped for 1-1/4 inch pipe connection.

Each standard shall have two 9/16 inch holes provided, where shown on Sheet No. 122.

The luminaire shall consist of a supporting hood, and external body or casing, an internal main reflector, and a refractor globe. The hood shall be made of cast aluminum and shall be tapped for I-I/4" standard pipe. The external body or casing shall be made of cast aluminum and shall be firmly attached to the hood by means of adequate screws or bolts. The main reflector shall be made of heavy gauge aluminum sheet, Alzak finished and polished. The entire reflecting element shall be rigidly attached to the external body by means of screws or bolts.

The globes shall be supplied with a non-rusting metal supporting ring or band with clamps around the rim or flange of the globe. The supporting ring shall be so designed that broken globes can be replaced at the lamp location with the use of simple hand tools. All screws, nuts, washers, etc., which must be removed in order to replace a broken globe shall be non-ferrous and corrosion-proof. The globe supporting ring shall be attached to the reflector by means of a hinge or its equivalent on one side and a latch, thumb screw, or equivalent on the opposite side. These devices shall be so designed that with the globe in place, the latch or thumb screw can be released by hand the globe swung down and then lifted off the hinge so that the globe can be washed separately from the fixture. The design shall be such that after washing, the globe can be hooked on to the hinge and then pushed up into place against the gasket with one hand while the latch or thumb screw is tightened with the other hand. The best design shall be that which combines simplicity and ease of operation with the most effective seal between the glass globe and the reflector. Fixtures having the reflector permanently attached or "spun on" to the glass globe will not be accepted. A skeleton type mogul multiple socket shall be mounted in the hood and shall be suitable for 10,000 or 15,000 lumen 20 ampere lamps. The fixture shall produce an I.E.S. Type IV light distribution curve equal to the curve produced by the General Electric Form 79AR.

Lamps for navigation fixtures shall be 50 watt, vibration service, and for luminaires shall be 15,000 lumen, PS-40 bulbs, mogul base, as indicated on Sheet No. 122.

For navigation lighting, suspension bridge lamps shall be provided where indicated on the plans. The channel margin suspension bridge lamps shall be galvanized cast iron with 180° red fresnel lens, equipped with shock absorbing sockets, retriever chains, and similar to Western Railroad Supply Company Figure #2. The channel center pivot type suspension bridge lamps with 360° green fresnel lens shall be equipped with retriever chains, and equal to Western Railroad Supply Company Figure #11.

External parts of all luminaires shall be finished aluminum, Gaskets used for sealing vices and in order to deliver the performance required they must have the lamp filaoptical center. If the manufacturer's design provides for vertical adjustment of the reference point, such as the lower edge of the reflector or casing, so that the pur-Refracting globes shall preferably be keyed to the supporting reflector so that they

as a complete unit.

All the street lighting transformers will be connected with their primary windings in a 6.6 ampere 60 cycle regulated circuit, and shall be located in the sidewalk junction boxes. The secondary of the transformer for the navigation lights shall be 60 watt, 120 volt, multiple secondary and shall be equal to Westinghouse No. 348293. The secondary of the 10,000/15,000 lumen transformers will supply 20 amperes to one lamp rated 15,000 lumens. When the lamp wattage varies between 8% above and 20% below normal, the secondary or lamp current shall not vary more than 1% from 20 amperes with 6.6 amperes at 60 cycles supplied to the primary winding. Each transformer shall be given a dielectric test by the manufacturer and shall withstand 22,000 volts between primary winding and all other parts of the transformer and 1,500 volts between the secondary winding and all other parts of the transformer. Both of the above tests shall be applied for one minute, without failure. The street lighting transformers shall be, as nearly as obtainable, like that shown on Drawing No. 3863 of the Division of Light and Power of the City of Cleveland, which is the type preferred by the City and will be the criterion in judging the adequacy of the type proposed by the contractor. Individual transformers shall be furnished for each light.

Each transformer shall be supplied with a noncorrosive name plate showing the following data: Maker's name and style or catalog number

Rating in Lumens Primary current Secondary current

Conductor for Roadway lighting shall be #8 AWG solid soft drawn copper of not less than 98% conductivity and shall be coated with lead, tin, or antimony alloy. Insulation shall consist of 10/64 inch of rubber-like compound known commercially as ozone resistant type insulation. The insulating compound shall conform in every respect and shall be tested in accordance with ASTM Designation D574-46T, or the latest revision thereof. The outside jacket or sheath shall be 4/64 inch thick and shall be made of GR-M Polychloroprene (Neo Prene) sheath compound. The sheath compound shall conform in every respect and shall be tested in accordance with ASTM Designation D753-44T, or the latest revision thereof. The cable shall be shipped on reels. Each reel shall be marked "Street Lighting Cable" and marking card shall carry manufacturer's descriptive data for the conductor and insulation.

The junction boxes for branches to lights from 3" longitudinal conduit runs shall be suitably attached under sidewalk where indicated. Brass or monel screws shall hold cover tigntly. The finish inside shall be hot-dip galvanizing. Boxes shall be similar to Hopes 1252 size 24 x 12 x 6, with no lugs. See Sheet 122 for an alternate welded sheet metal junction box.

Conductors on truss spans of bridge shall be in asbestos cement conduit conforming to Supplemental Specification No. N - 206.14 or in fiber conduit equivalent to Orange-·burg Nocrete. The conduits shall be 3 inch inside diameter and be placed on hangers that are furnished with the structural steel and shown on Sheet 100. All conduits on the bridge shall be supported at not over 6 ft. spaces.

Conduits cross the structure transversely in span I and span 9, as shown on Sheets 18, 26 and 122. These four conduits shall be 2 inch diameter asbestos cement conduit conforming to Supplemental Specification No. M - 206,14 or fiber conduit equivalent to Orange-

Rigid metal conduit from junction boxes to navigation lights shall be I inch. National "Sherarduct" or an approved equivalent. This conduit shall be furnished with tapered threaded fittings as required.

The circuit conductors for the IIO volt multiple circuit lighting cable to the navigation lighting units shall be No. 12 AWG conductors, as specified on Sheet No. 122. The conductors at pivot type fixtures shall be No. 12 AMG, 600 V., extra flexible, ASTM Class D. The conductors shall be continuous from outlet to outlet, and no splices shall be made except within outlet or junction boxes. The conductors shall have 3/64 inch insulation and 3/64 inch Neoprene jacket.

#### CONSTRUCTION METHODS

The installation as a whole shall be carried out in conformance with the requirements herein stated and implied, and upon completion of the work shall present a neat and workmanlike finished appearance. Safe construction and operating practices meeting the requirements of the National Electric Safety Code shall be maintained. All wiring-tonavigation lights is to be placed in rigid metal conduit fastened by suitable clamps. Longitudinal runs of conduits on the trusses are to be placed on hangers that are furnished with the structural steel and shown on Sheet 122.

Poles shall be carefully set, they shall be vertical, and the luminaires shall be supported with brackets about 28'-1" above pavement as indicated on the plans. The careful aligning and grading of poles is considered to be an essential feature of the installation. The work shall be as nearly perfect as practicable, and no perceptible tolerances will be permitted. In order to accomplish the desired perfection of alignment of the luminaires, the poles shall be carefully aligned and welded in place.

The installation of all luminaires and wiring shall conform to the recommendations of the equipment manufacturers and the practice of the power company.

Cables shall be installed in continuous lengths without splices, from terminal to terminal. At the terminals, cable shall be spliced to the equipment leads in strict conformity with the manufacturer's instructions. Care shall be taken to insure water-

Splices shall not be made in conduits. Splices of conductors shall be made mechanically and electrically secure and flooded with solder, and wrapped in accordance with the recommendations of the manufacturer of the cable so that the insulation and the mechanical and electrical qualities of the splices shall be equal to that of the remainder of the conductor.

Conduits shall be firmly clamped to the structures to prevent rattling, shall be run in lines parallel and perpendicular to lines of structures and shall be so placed that dirt will not accumulate around them. Supports shall not be at more than 6 ft. centers. There shall be at least one inch clearance between conduits. If on a horizontal surface for over one foot, they shall clear the surface by at least three inches. Adequate approved provision for the movement of conduits shall be made wherever conduits cross expansion or fixed joints in the supporting structures. Where asbestos cement conduit is on the structures, one expansion coupling with rubber ring shall be used at least every 75 feet. Rigid conduit across expansion joints if used shall have an expansion coupling similar to O.Z. Type EX or AX as required, complete with bonding jumper, or be in flexible couplings equal to Crouse Hinds Type EC.

It is anticipated that the work under this contract will be completed prior to the completion of the adjoining girder spans. The Contractor shall install the series lighting cable in the conduits to the ends of the project and leave pig tails for connection by others to the lighting circuits.

The Contractor shall furnish all equipment and appliances necessary to test the completed cable systems. A burning test will not be necessary for the street lights on the truss spans. The City of Cleveland will make a "megger" test of all circuits. It shall be the Contractor's responsibility to demonstrate to the satisfaction of the Director of Highways, that all lighting circuits are continuous and free from short circuits and unspecified grounds, that all circuits are properly connected in accordance with the applicable wiring diagrams and that the resistance to ground of nongrounded series

circuits is not less than 50,000 OHMS.

In the event that the truss spans are completed ahead of the approach spans which. will be in a subsequent contract, it will be necessary to provide power for the navigation lights. If this power is needed, the Bridge Contractor will furnish and install a separate circuit consisting of two number 6 wires or a low voltage cable, on each side of the bridge. Each such circuit would serve the three navigation lights on the respective side of the bridge. These temporary circuits for the navigation lights would extend to the end of the truss spans only and the Contractor would there leave pig tails for connections by others to an existing 120 volt line on University Road near the west end pier. Separate conduits would not be required for these temporary navigation light circuits as the temporary circuits would be carried in the street lighting conduits.

#### 5. GUARANTEE

The Contractor shall be responsible for the proper performance in part and as a whole of the structural, mechanical and electrical equipment provided for the roadway and navigation lighting circuits and related parts for the period of one year after final acceptance of the work, to the extent that he shall correct at his own expense any difficulties with the operation which may arise during this period as the result of defects in material, equipment, manufacture and erection. Responsibility for such correction shall include the repair, readjustment and replacement not only of defective parts, but of other parts which may be damaged therby. The State of Ohio and City of Cleveland reserve the right to themselves to correct any such defects and the Contractor shall pay the cost thereof. The Contractor shall give a written guarantee satisfactory to the State and City to insure the carrying out of these obligations.

#### 6. PAYMENT FOR ROADWAY AND NAVIGATION LIGHTING

Payment for the three inch diameter conduit under each sidewalk; two inch diameter conduit across the structure in spans I and 9; conduit attachments and U bolt hangers; junction boxes; couplings; expansion couplings; standards; base castings; mast arms; ornamental pole tops; plumbizers; and all bolts, nuts, screws, fittings, clamps and other miscellaneous accessories shall be made in a lump sum payment for Item S-25, Roadway Lighting system, Part A.

Payment for cable; flexible cables and connections; wiring; splices; luminaires; globes; sockets; lamps; lighting transformers; ballasts; clamps; tests; removing waste; and all incidentals necessary for completing the Roadway Lighting System in an acceptable operating condition shall be made in a lump sum for Item S-25. Roadway Lighting System, Part B.

Payment for conduit from the navigation lights to the junction boxes of the Roadway Lighting System; pull boxes; splicing boxes; fixtures; globes; lamps; retriever chains; bolts; wiring of the navigation lights from the secondaries of the lighting transformers located in the junction boxes of the Roadway Lighting System; fittings; couplings; splices; attachments; tests; and all incidentals necessary for the installation and satisfactory operation of the six navigation lights, shall be made in a lump sum for Item S-25. Navigation Lights.

Payment for Item S-25 Electrical Grounds, shall include all materials and work described under paragraph 18. Electrical Grounds, on Sheet 3.

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CUT-42R-17.50

GENERAL NOTES

CLEVELAND

CUYAHOGA COUNTY

HOWARD, NEEDLES, TAMMEN & BERGENDOFF

CLEVELAND NEW YORK 914-1A SHEET 2.05

MADE GA DATE 10-7:54 9:54 CKD DME DATE 2-9-55

## requirements, such items may be rejected.

will be acceptable.

latest approved design.

aire similar to General Electric Form 79-AR. Luminaires lighting the roadway shall meet the general requirements of LES. Type IV distribution. Luminaires shall overhang about 6 ft. out from curb.

Drawing M-20.35, of the City of Cleveland as to general design and finish, height. base, mast arm and dimensions. In general, the standards shall consist of a cast steel anchor base to which shall be welded a tapered steel pole. To the steel pole shall be fastened an ornamental pole top to which shall be welded a mast arm for supporting the lighting unit.

Sheet No. 122 shall be secured to the lower end of the shaft by means of a double shall be on the inside at the top of the base.

This Specification shall govern for the materials used and for the installation of a

ROADWAY AND NAVIGATION LIGHTING

complete series roadway and navigation lighting system for the viaduct. The type and location of lights, the circuits and the location of cables and conduits shall be as indicated on the plans. The installation for roadway lights shall be in fiber or asbestos-cement conduit. For the roadway lighting, 15,000 lumen incandescent lights are to be installed as indicated on the plans, and are to be operated on a 6.6 amp. series circuit. The navigation lights are to be 50 watt, their branch circuits are to be in rigid conduit, and are to be installed for 115 volt secondary operation through

insulating transformers from the 6.6 amp. series circuit. The Contractor shall cooperate with the Cleveland Division of Light and Power and the Cleveland Electric Illuminating Company, but he will not be required to furnish, install or connect meters, meter mounts, metering equipment or housing for same. The Contractor shall provide proper termination of loop circuits for connection to future adjacent series circuits.

The Contractor shall furnish and install lighting equipment, including all lamps, luminaires, navigation lighting fixtures, wiring, luminaire brackets, poles, expansion couplings, flexible couplings, tops of posts (bases for poles), pole cap screws, cable, all conduit for lighting circuits, and all incidentals necessary for a complete circuit installation, installed and connected for operation. The loops of lighting circuits shall be complete, and the Contractor shall furnish and install all equipment necessary for the satisfactory future operation of the circuits and for the complete operation of the lighting system, (excluding the future adjacent sections, leads, primary transformers, primary fuse cutouts, primary arresters, and primary connections to the power sources) whether specifically mentioned or not.

The lighting installation, when completed shall comply with the applicable provisions of the A.I.E.E. Standards and Practices, American Standards, and National Electric Manufacturers' Association Standards, and shall conform to all local and special laws or ordinances governing such installation, and to the special requirements herein set forth. Should the plans and detail specifications be in conflict with these requirements, through error or omission, the Contractor shall call such conflict to the attention of the Engineer, and the Contractor shall make the necessary corrections in the installation as may be directed by the Engineer.

Insofar as practicable, all major items of electrical equipment such as luminaires, cable, poles, insulating transformers, etc., shall consist of products of the same manufacturer in order to secure single responsibility and most satisfactory service. Unless specifically noted otherwise, all electrical equipment shall be equal to the best grade of that type of equipment as manufactured by the General Electric Company. The Westinghouse Electric Company, or the Line Material Company, Reference to any name, make or manufacturer's number for an article of equipment or material is intended to

A layout wiring diagram showing in general the arrangements and location of the equipment is shown on the plans. This shall be considered only as illustrative and, subject to the approval of the Engineer, the Contractor shall modify it as necessary for complete and proper construction and operation. The location of the transformers, services, conduit and luminaires shown on the plans are diagrammatic only, and may be subject to shifting as the Engineer may direct in order to conform to local conditions.

Before commencement of installation of the roadway lighting system, a complete schedule of materials and equipment proposed for installation shall be submitted for the approval of the Engineer. The schedule shall include catalogs, cuts, diagrams, drawings, and other such descriptive data as may be required by the Engineer. In the event any items of material or equipment contained in the schedule fail to comply with specification

## MATERIALS AND EQUIPMENT

All bolts, nuts, studs, washers, pins, terminals, springs, and similar fastenings and fittings shall be, where practicable, of an approved corrosion-resisting material such as brass or bronze, or of a material treated in an approved manner to render it adequately resistant to corrosion. Hot-dip galvanizing shall be considered such approved treatment. All materials furnished shall be new, shall be of the best quality and workmanship, shall be the best standard product of a manufacturer regularly engaged in the production of this type of equipment and shall be of the manufacturer's

Each roadway lighting unit shall comprise a pole with a 10 ft. bracket and a lumin-

Light standards shall conform as nearly as possible to the specifications and

A cast steel anchor base of adequate strength and of the shape and size shown on electric weld. To obtain this construction, the base shall telescope the shaft, and one weld shall be on the outside of the shaft at the end of the shaft and the other

Painting shall be as specified under paragraph 20, Sheet 3.

the joint between globes and reflectors or casings shall be preformed cork or felt and shall be cemented in place. The fixtures as specified are precision optical dement correctly located with reference to the reflecting or refracting elements. The sockets shall preferably be solidly mounted, with the lamp filament at the correct socket, he shall furnish a drawing showing the proper dimension to some convenient chaser can make a gauge to be used for accurately setting and locking the sockets. cannot be placed in any other than the correct angular location. In any event, the globes must be plainly marked to indicate the "street side" and the "house" or "sidewalk side". All lamps used in these fixtures will be standard 20 ampere, base

up. Wazda type with mogul bases and 7 inch light center. Lamp sockets used in enclosed fixtures of the types specified are subjected to high temperatures and the sockets furnished shall be for heavy duty and shall incorporate all the latest design features available such as center spring loaded contacts. plated parts and extra heavy cast terminals, to reduce the possibility of contact troubles and welding of the lamp base to the socket shell. Each fixture shall preferably be completely assembled at the factory and shipped in a single container

## FEDERAL AID PROJECT NO. OHIO

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT

# GENERAL NOTES, CONTINUED

STRUCTURAL STEEL, DRAINAGE SYSTEM, AND ALUMINUM HANDRAIL

#### CHARACTER OF METAL

Thickness of Specimen) 1

A. Metal not otherwise specified shall be copper-bearing carbon structural steel. In general, trusses, trussed floorbeam horizontal bottom struts at piers, and top laterals adjacent to piers shall be of a special high strength steel, known hereinafter as manganese structural steel. These special steel parts are identified on the drawings by the suffix "S". Other parts of the spans, including the entire floor system, shall be of copper-bearing carbon structural steel. All rivets and bolts shall be copper-bearing rivet steel. Pins not otherwise specified shall be cold rolled or forged. Castings not otherwise specified shall be steel.

B. Copper-Bearing carbon structural and rivet steel shall conform to Sec. M-7.4 (b) of the specifications.

C. Manganese structural steel shall conform to the following specifications:

#### Chemical €omposition - Per Cent

	L	adle	Check		
Carbon	0.28	Wax.	0.32 Max.		
Manganese	1.10	to 1.60	1.65 Max.		
Phosphorous	0.04	5 Wax.	0.055 Max.		
Sulphur	0.05	Max.	\ .		
Silicon		Max.	•		
Copper		Min.	0.18 Min.		
	Phys ic	al Properties			
	1/2" and	over 1/2 to 3/4"	over 3/4 to 1"	over 1 to 1-1/2"	
Thickness	Under	incl.	incl.	incl.	
Yield Point	50,000	47,000	46.000	45,000	
Tensile Strength	70,000	70,000	67,000	67,000	
Elongation in 8*	18% Min.	18% Nin.	19% Win.	19% Min.	
Bend Test			<u>-</u> •	•	
(Ratio of Bend Dia.	to				

All other requirements shall be in accordance with A.S.T.M. A6 and A7. All parts of manganese structural steel shall be identified by paint marks and stamping at the mill, and these identification marks with some characteristic painting shall be retained throughout the work of fabrication, so that there shall be no mistakes in the use of manganese structural steel parts where required.

D. Steel castings not otherwise specified shall conform to Sec. M-7.7 of E. Steel forgings shall conform to Sec. M-7.5 of the Specifications. except

alloy steel forgings shall conform to A.S.T.M. Specification A237+52T. Class B. F. Wrought Iron. Wrought Iron plates shall conform to A.S.I.M. Specifications for wrought iron plates, designation A42. Wrought Iron Rivets shall conform to A.S.T.M. Specifications for wrought iron rivets, designation AI52.

G. Cold rolled steel shall conform to Sec. M-7.17 of the Specifications. H. Soft steel in bent curb plates shall conform to A.S.T.M. Specifications low and intermediate tensile strength carbon steel plates of structural quality, designation A283+52T, Grade A.

1. For materials in fixed and expansion shoes, see Sh. 97. J. High strength bolts shall conform to Supplemental Specification

No. S-207 dated 4-28-55.

K. Lead Plates under shoes shall conform to Specification M-7.14. Wrought iron pipe shall be "Standard Weight", conforming to Specification N-6.10.

M. Copper-bearing steel is not required for castings, cold rolled or forged pins, or forgings, or for high-strength bolts.

N. Where wrought iron is specified for flashing, troughs, hoppers and downspouts of the roadway drainage system, Mayari R or Corten steel may be used as an alternate.

## FABRICATION

A. Shop assemblies and camber. The trusses of the deck truss spans shall be cambered so that when erected and under full dead load they will have their normal outline with all members of the normal length shown on the plans. The lengths of unstressed members shall be so determined. Except as otherwise approved each truss shall be separately completely assembled in the shop. The chord members of each truss shall be assembled in correct geometric pattern conforming to the final outline and the holes for field rivets in the splices of the chords shall be reamed. These splices shall then be fitted with sufficient numbers of tight fitting bolts and pins to prevent any movement of the members at the splices as the chords are adjusted into cambered position. The assembly of each truss in the shop in cambered position shall be completed by addition of the web members, and the holes for field rivets in web member connections shall be reamed or drilled while the truss is so assembled. Care shall be taken to keep the centerlines of all truss members in a plane and to set the web members at their correct geometric angles with the chords.

In lieu of the complete shop assembly of each truss as specified above, alternate procedures will be considered which will provide for the assembly and reaming of truss chords and truss web members according to an approved plan-which will insure accuracy of field holes and fitting of parts equivalent to that to be secured by complete assembly. In case the Contractor should desire to use such a method, complete data regarding the method to be used and precautions which will be followed to assure accuracy shall be submitted to the Engineer for approval or modification. Final approval of the exact details of the operations must be secured before the work progresses, and if not approved there shall be complete assembly of the trusses. B. Holes in all parts of trusses, except diaphragms, and in all metal

All single and double story floorbeam trusses shall be completely assembled in the shop, matchmarked, and all field holes reamed. Connections for lateral bracing shall be reamed to steel templates. Floorbeam cantilevers shall be assembled with the floorbeams and the top chord, and the holes in the tension tie plates reamed.

connected to the trusses through these holes shall be reamed.

C. Plates 36 inches wide and under shall have rolled edges. Edges of angles cut to special size shall be finished by machining or grinding. Sheared edges of steel plates in excess of 3/4" shall be planed to a depth of one quarter inch. Sheared edges of irregular shaped truss gusset plates shall be planed to a depth of one-quarter inch.

Wherever there is flame cutting of manganese steel and carbon steel gusset plates 3/4" or more in thickness, the flame cut edges shall be machined off or ground off to a depth not less than 1/4". In lieu of such machining or grinding, the flame cut edges may be flame softened or annealed, provided these operations restore the metal to substantially its original degree of hardness and other physical properties. Flame softening or annealing shall be done with suitable equipment operated by experienced operators and in general shall consist of heating with a gas flame directed at right angles to the cut surface so that the edge of the work is heated 1/8" deep along its entire length to a cherry red color visible in daylight. To demonstrate the efficiency of the flame softening or annealing, the Contractor may be required to prepare samples by flame cutting and flame softening or annealing of portions of the steel cut away. and shall test these for tensile strength, bending and for hardness, and for comparison shall prepare similar samples by machining or other methods not involving flame cutting and shall test these control samples similarly for the same qualities. The numbers of such tests shall depend upon the extent of flame cutting, and shall be made at intervals of time as the work progresses sufficient to demonstrate the efficiency and uniformity of the operations.

Details not covered by the Design Specifications for Highway Structures of the State of Ohio, shall meet the requirements of the American Association of State Highway Officials Standard Specifications for Highway Bridges, 1953.

#### ERECTION OF SUPERSTRUCTURE METALWORK

Unless otherwise required and approved for particular erection conditions, laterals shall not be riveted until after spans are swung and are supporting their own dead load weight of steel. In cantilever erection, laterals may be riveted at any time when the stresses in the chord members adjacent to the specific laterals are approximately the same as the final dead load stresses which will be in these chord members after the span is completed. Prior to riveting, laterals subject to wind loads and other stresses under erection conditions shall be connected with sufficient bolts and drift pins to provide suitably for all such possible stresses.

Should the Contractor elect to provide increased section in certain truss members or in other parts of the superstructure metalwork, for methods of erection which the Contractor may adopt, such increases of sections and parts may be incorporated in the structure, subject to the approval of the Engineer, but shall be paid for by the Contractor and will not be included in final pay quantities.

The contractor may also provide any other additional members or parts to be temporarily attached to but not permanently incorporated in the final structure for any erection purpose. All such parts shall be classed as erection equipment and falsework and shall not be included in the final pay quantities.

Should changes in any members or other portions of the truss spans, made for purposes of erection, increase the weights of the trusses, the Contractor shall calculate the camber of the structure as affected by such modifications, and shall modify the camber of the trusses as the changed conditions make necessary. The Contractor shall have full responsibility to provide the completed structure, adjusted and in correct final position. The strain in each truss member to be used in computing the camber

including the slab L = length of member, c+c panel points, in inches.  $A = 1.05 \times 10^{-5}$ gross area, in sq. inches. E = modulus of elasticity = 29,000,000 lb. per sq. inch.

## 4. GENERAL

A. Welding shall be class "A".

B. Welds shown as field may, at the Contractor's option, be made in the shop. C. Rivets shall be 7/8 inch in diameter unless otherwise specified. In the preparation of working drawings, the spacing of rivet holes shall be made to maintain the full net section shown on the plans for all tension members. Where rivet grips exceed 6 diameters specially designed rivets or high strength bolts shall be used. D. Drain holes of character and locations as approved by the Engineer shall be provided in metal work parts wherever water might collect and have no other means of drainage. Should it become evident after erection that sufficient drain holes have not been provided in fabrication, the Contractor shall provide additional drainage holes of character and locations as may be approved. E. Bending of steel plates shall conform to A.A.S.H.O. 1953 Specifications;

## 5. EXPANSION JOINTS

Section 2.10.29.

Steel castings for roadway expansion: joints shall be machined on bottom surfaces which will contact supporting steel and top surfaces shall be spot faced for nuts. All sections for both sides of each joint (except for end piers) shall be shop assembled with nominal clearance of 3/4 inch between ends and roots of mating projections. While thus assembled the joint shall be checked and corrected to provide not less than I/8 inch clearance between sides of projections and not less than 5/8 inch clearance between ends and roots of projections. All parts of roadway joints so assembled shall be matchmarked.

Roadway expansion joint castings shall be erected according to the shop matchmarking and shall be set to the longitudinal clearance required for the temperature at the time of setting, to the required grade of roadway, and to provide equal side clearance between mating projections. Holes in the supporting steel shall be drilled in the field after the castings are adjusted in final position.

Sidewalk and curb joints shall be shop assembled, corrected to provide uniform close contact between any two mating parts of each joint, matchmarked and erected to required lines and grades.

### CURBS, SIDEWALK, FASCIA AND HANDRAIL

A. The edge of pavement and curb lines are defined on the plans. On the horizontal and vertical curves, the curb, sidewalk, fascia and handrail shall be fabricated in straight panels between floorbeams.

B. Curbs shall be formed of soft steel bent plates. The curb units thus formed shall be erected so that after the spans have deflected under the dead load of slab and steel, the curbs shall depart not more than one-eighth inch from the required line and grade shown on the plans and shall show no abrupt kinks. Vertical adjustment of the curb supports shall be accomplished by shimming on the horizontal supporting struts. Holes for rivets attaching the curb supports to the struts shall be subpunched and field reamed to provide lateral adjustment.

C. The fascia beams supported at the ends of the sidewalk brackets shall be adjusted, before the roadway slab and wearing surface are in place, so as to depart not more than one-eighth inch from the required line and grade shown on the plans, and shall show no abrupt kinks. Adjustments shall be made by reaming the con-

D. The raised pattern floor plate similar and equivalent to Carnegie Multigrip floor plate, shall be field welded to the fascia, curb and supporting angles. The plates shall be furnished in sections not to exceed one floor beam panel in length. Care shall be exercised in field assembly to maintain a neat line of the edge of the plate along the top of the supporting curb, Joints shall be accurately formed, so that they may be completely filled with weld. The plates shall not be placed and attached until after the roadway slab is in place with the full dead load on the supporting steel work. The floor plate shall be neatly cut and tightly fitting adjacent to steel posts supporting the light pole units. After adjustment of the posts a seal weld shall be run entirely around the post at the surface of the plate, except adjoining access doors to junction boxes.

### PAYMENT FOR STRUCTURAL STEEL

Item S-7, Structural carbon steel, includes all structural carbon steel, castings, forgings, rivets, bolts, shoes, roadway and curb expansion joints, curbs, walkways, stringers, beams, laterals, trusses, inspection walks (except grating), sidewalk hatches, ladders, wrought iron, lead plates, and every other item of metalwork for which payment is not otherwise provided, including shop painting of all metalwork covered by this item.

## ROADWAY DRAINAGE SYSTEM

A complete roadway drainage system with inspection walkways and access ladders, is shown on the plans. Access is provided to the drainage collection troughs beneath the roadway surface by hatches in the sidewalk area giving access to ladders and inspection catwalks near the water collection troughs. The inspection catwalks, made up of a light grating floor between channel stringers, are hung from the roadway stringers by angle hangers. The walkway grating for these inspection catwalks and for the walks providing access to the navigation lights, shall be I inch grating. The grating shall be securely attached in place by field tack welding. All walkway grating shall conform to Supplemental Specifications No. 24 dated May 28, 1948.

Item S-29, Roadway Drainage System, includes the following: Perforated roadway cross drains with parts shop welded thereto; wrought iron flashing; transverse collection troughs; angle frameworks connected to the inspection walkway but supporting the transverse collection troughs; hoppers; frameworks supporting hoppers; downspouts; split collar connectors and bolts; longitudinal collection troughs; hoppers and their supports on pier tops; and all other angles and plates and miscellaneous parts required solely for the attaching and support of parts of the drainage system.

Painting of the drainage system is included in Item S-8, and shall consist of the two red lead and the two white lead paint coats specified for the structural steel except that the first red lead coat may be applied in the field to those members that require no shop fabrication.

Access ladders and the supporting frameworks of the transverse inspection walkways with the handrail and walkway stringers and bracing are included in Item S-7. Structural Carbon Steet. Walkway grating is paid for under Item S 5-24.

Item 5-7, Manganese structural steel, includes all manganese steel used in trusses, laterals, struts and connecting plates, including shop painting of all metalwork covered by this item.

In accordance with Sec. S-7.28 of the Construction and Material Specifications, the weight of waste material, such as is removed by burning, cutting, coping, clipping, machining, punching, drilling, etc., shall not be considered as pay weight, but material removed to form rivet and bolt holes shall be included in the pay quantity provided that only those portions of the rivets and bolts projecting beyond the holes are included. Furthermore, any thickness and weight of members in excess of that called for on the plans (due to overweight or other cause) shall not be included in determining the weight to be paid for, unless an increase in the size of a member is authorized by the Director.

## ALUMINUM TUBE HANDRAIL

The handrail for this structure shall consist of aluminum tubes and posts mounted on the attaching brackets extending through the sidewalk plate. The borizontal members of the rail shall consist of three round tubes, with the top tube of 4-1/2 inch outside diameter and a wall thickness of 3/16 inch, and with the center and bottom tubes of 3-1/2 inch outside diameter and a wall thickness of 5/16 inch or 3" Extra Strong Pipe (3-1/2" O.D.). Each post shall be a cast aluminum curved H section with a monolithic recessed base and tubular sockets for insertion of the rails. The horizontal tubes shall be fastened in the post socket with aluminum bolts. Posts shall be attached to the brackets with steel stud bolts welded into the brackets.

Fabrication of aluminum alloy shall in general conform to the practices recommended in Aluminum Company of America's Structural Handbook, and the following specific re-

- 1. Material shall be sawed or milled.
- 2. Flame cutting is not permitted.
- 3. Material may be heated to a temperature not exceeding 400° F. for a period not exceeding 15 minutes to facilitate bending.
- 4. Holes in extruded alloys shall be drilled. All holes in castings shall be cored, and rail socket holes shall be reamed.
- 5. Welding shall be done by the inert gas shielded arc method and no flux shall be used. Welding is permitted only where specifically called for

In handling aluminum materials in the shop and in the field every precaution shall be taken to avoid scoring or marring of the surfaces, and any such scoring or marring of the surfaces, sufficient in the opinion of the Engineer to give an objectionable appearance, shall be cause for rejection of the material. Cast parts shall have all fins, pipes or other irregularities removed. Tubing shall be seamless and uniform in quality and temper. Exterior and interior surfaces shall be clean, smooth and free from seams, slivers, laminations, grooves, cracks or other defects. End plugs shall be welded and ground smooth.

Aluminum alloy tubing shall conform to A.S.T.M. Tentative Specifications for Aluminum Alloy Extruded Tubes, Designation 8235-54T, and shall be alloy GSIIA, Temper T6. Aluminum posts shall conform to either A.S.T.M. Tentative Specifications for Aluminum Base Alloy Sand Castings, Designation B26-54T, Alloy SG70A, Condition T6: or A.S.T.W. Tentative Specifications for Aluminum Base Alloy Permanent Mold Castings, Designation BIO8-54T, Alloy SGTOA, Condition T6. Aluminum bolts and nuts shall be produced from rods and bars conforming to A.S.T.M. Tentative Specifications for Aluminum-Alloy Bars. Rods and Wire, Designation 8211-54T and shall be alloy CG42A, Temper T4. Aluminum bolts for attaching rails to posts shall be Semi-finished Regular Carriage Bolts. Aluminum nuts shall be Hexagon Semi-finished Regular Nuts. Threads shall be American Standard Coarse Thread Series Class 2 free fit. Anchor bolts shall be structural steel, and shall be galvanized. All nuts and washers for anchor bolts shall be galvanized. Aluminum alloy tubing and posts shall have no special finish. The cast aluminum posts shall be given a light sand blast finish. Aluminum materials shall have all fabrication marks and irregularities corrected after all drilling, reaming, welding or other fabrication or erection operations are completed.

Before the posts are set in place the bottoms of the posts shall receive a heavy coating of Alumilastic compound, Consistency "K", or equal, completely filling the recesses in the post base and the space between the sidewalk plate and the post-supporting bracket. Anchor bolt studs and the top of bases of posts under the bolt nuts and washers shall also be coated with alumilastic material of a heavy brushing consistency. Before the nuts are tightened the holes through the base of the post shall be filled with Alumilastic compound, Consistency "K", completely filling the bolt hole which is not occupied by the bolt. Alumilastic compound shall be as manufactured by the Parr Paint and Color Company, Cleveland, Ohio, or approved equivalent.

Erection of rails and posts shall continue successively until all of the handrail of any one unit of the structure is erected. The handrail shall then be aligned by adjustment of the steel tees to which the posts are bolted. The adjustment of the handrail shall be such that the top rail shall not depart more than one-eighth inch from correct line and grade. Handrail on curve shall be aligned in straight panels between floor

The Contractor shall furnish a pattern of the cast aluminum handrail post to the City of Cleveland for use in the future replacement of damaged posts.

Payment for furnishing and placing the aluminum tube handrail complete including rails, aluminum posts, bolts, etc., shall be made at the contract unit price per lineal foot of handrail, which payment shall be complete compensation for all materials, equipment, tools, labor and all work incidental to the manufacture, fabrication and erection of the handrail. Payment will be made on the basis of the measured length of handrail between ends of handrail, measured at the top of top rail.

Payment for stud anchor bolts will be included in payment for Item S-7. Structural

PART 3

U. S. ROUTE 42 RELOCATION INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU -42R-175

GENERAL NOTES

CLEVELAND

CKD DME DATE 2-9-55

CUYAHOGA COUNTY

HOWARD, NEEDLES, TAMMEN & BERGENDOFF MADE GA DATE 10-7-54 CONSULTING ENGINEERS TRCD\_\_\_\_DATE\_\_\_

NEW YORK CLEVELAND

914-1A SHEET- 2, 04

FEB 15 1983

# GENERAL NOTES

#### DESIGN SPECIFICATIONS

"Design Specifications for Highway Structures", State of Ohio, Department of Highways, dated October 1, 1951, as revised July 15, 1952, Aprill, 1954, and February 1, 1955, (with a load frequency rating of CF 1200-51) are used in the design of this structure. The A.A.S.H.O. standard specifications for highway bridges, Article 3.4.8, (structural silicon steel) are used for the allowable unit stresses in manganese structural steel.

#### CONSTRUCTION SPECIFICATIONS

"Construction and Material Specifications", State of Ohio, Department of Highways, dated January 1, 1955, as modified by notes on the plans and in the proposal, shall govern.

#### SCOPE OF CONTRACT

The work included in this contract consists of the following: Furnishing and erecting the entire steel superstructure of the bridge from Sta. 16 + 13.02 to Sta. 43 + 34.72 including lead plates under shoes; shoes; steel superstructure; the bridge drainage system including downspouts, drainage troughs, hoppers, and connection to the downspouts in the pier shafts; the expansion joints; inspection walkways; ladders; the aluminum handrail, steel sidewalk and curbs; the reinforced concrete roadway slab; the navigation lighting system; the bridge roadway lighting system; and any and all other incidentals including painting of metal-work, but not including roadway surface course, necessary to complete the work, ready for use.

### DIMENSIONS

Dimensions given are measured horizontally and at 60° F., unless otherwise noted.

#### DATUM PLANE FOR ELEVATIONS

All elevations are regional geodetic survey datum.

### FIELD OFFICE

The Contractor shall provide a field office, in accordance with Sec. S-0.01 (b) of the "Construction and Material Specifications" as soon as possible after the award of the contract, having a minimum of 500 square feet of floor space. The office shall be of watertight construction with suitable windows and doors, properly screened, and with interior walls and ceiling finished with celotex or similar insulating board. The floor shall be double thickness. The office shall be provided with heating. lighting and telephone facilities and shall be equipped with one desk, one camp type plan table, one camp type work table and two chairs. The Contractor shall maintain the office and services until completion of his contract.

### BORINGS

The log of each of the test hole borings is shown in these plans,

## TRAFFIC

Portions of this project shall be constructed under traffic and the Contractor. to the satisfaction of the Engineer, shall plan and conduct his operations so that traffic shall be maintained as herein specified.

Local traffic shall be maintained as per Sec. G-4.05, during the entire construction period. If any street is closed to traffic temporarily, work on that particular street shall be prosecuted to the fullest to allow for its reopening as soon as possible. Existing streets adjacent to the project shall remain open as long as possible and feasible.

Construction operations may interfere with traffic on existing railroad tracks. The tracks will in some cases be relocated by the owners, and in other cases will be removed. The Confractor shall coordinate his construction operations so as to interfere the least possible amount with train movements. Flagmen and watchmen shall be supplied as required by the railroads, at the expense of the Contractor.

## MINIMUM TEMPORARY CONSTRUCTION CLEARANCE FOR RAILROAD TRACKS

The minimum temporary construction clearance for railroad tracks shall be 21' -0" vertically above top of rail and 8'-0" horizontally from centerline of the nearest

## 10. WORK IN NAVIGABLE WATERS

All construction operations in the river shall conform to the requirements or directions of the District Engineer, U. S. Army. and to the requirements of the U. S. Coast Guard. The Contractor shall notify the District Engineer's Office, Corps of Engineers. U. S. Army, seven days in advance of commencement of work in the river so that navigation interests may be notified of the presence of construction equipment and also shall notify the same office when work in the river is completed. The Contractor shall provide and maintain navigation lights and other navigation signals or facilities which may be required on temporary constructions or vessels, and shall provide and maintain navigation lights on partially or entirely completed spans for the duration of his contract, in accordance with the requirements of the U. S. Coast Guard. The Contractor shall apply for and secure all necessary Department of the Army permits for dredging and dumping and for constructing falsework or other temporary constructions in the river. The Contractor shall provide areas for disposal of excavated materials at his own expense.

## 11. SEWAGE

The Contractor shall so conduct his operations that the flow of all existing sewers will be maintained at all times.

## 12. SIGNS

In addition to the requirements of Section G-7.07. "Barricades", "Danger" and "Warning" signs, the Contractor shall display one "Please - Men Working on Road" sign. Section 6-7.07, furnished by the State at each end of each zone where work is in progress and in such a position as to be visible to the traffic approaching the zone.

The Contractor shall be responsible for the preservation of these signs, shall advance the signs as work progresses and shall return the signs to the state at the completion of work.

In addition to the above, the Item of "Maintaining Traffic" shall include furnishing lights, signs (other than those mentioned above), barricades and watchmen to assure the flow of traffic twenty-tour (24) hours daily.

## 13. CONCRETE

All concrete shall be class "C".

A. The concrete roadway slabs shall be so constructed that, after completion and after removal of forms and any falsework, and after the steelwork has deflected under the weight of the concrete and wearing surface, the top surface of the roadway shall conform as nearly as practicable to the elevations and contour lines shown on the plans.

B. The roadway slabs shall, in general, be of uniform thickness between stringers. The thickness of the slab over the stringers shall vary to compensate for the deflection of the stringer due to dead load.

C. The theoretical deflections for each span are to be computed by the Contractor. The allowances to be made in screed setting to compensate for the deflections due to the dead load weight of the concrete, the asphaltic concrete surface course and the structural steel not yet in place at the time the slab is poured are to be computed; such allowances to be made above the elevations stipulated on the plans for finished pavement surfaces. Screeds may require further adjustment due to irregularities in the fabricated steel.

D. The concrete of the roadway slabs on the steel spans shall be poured in special sequence. There are shown on the plans the sequences, extent and direction of individual pours for each unit. The Contractor may submit for approval by the Engineer. alternate schemes of placing concrete slabs. The sequence of slab construction shown on the plans does not apply to the median strip.

E. Any pouring sequence may be used which adheres to the following general rules:

a. For units with one cantilever arm, pour the adjacent suspended span first, i.e.:

(1) Pour Unit No. 2 before Unit No. 1.

(2) Pour Unit No. 8 before Unit No. 9. b. For units with double cantilever arms, pour both adjacent suspended spans first, i.e.:

(1) Pour Units No. 2 and No. 4 before Unit No. 3.

(2) Pour Units No. 4 and No. 6 before Unit No. 5. (3) Pour Units No. 6 and No. 8 before Unit No. 7.

c. Pour the adjacent slabs on the cantilever arms of the particular

d. Complete the pouring of the unit by placing the slabs on the anchor arms.

A particular sequence starting at the west end of the viaduct is shown on the plans.

The slab must be placed for the full width of the roadway for a particular pour before proceeding with the next pour. Longitudinal construction joints in the slab will be permitted only over the center stringer. Transverse construction joints through the slab are shown on the plans. The Contractor may provide additional transverse construction joints at other locations, conforming to the details shown on Sheet +14:103 The Contractor's proposed general arrangement of construction joints must be approved by the Director of Highways before any slab concrete is placed.

Concrete base for wearing surface shall be finished according to Section 5-1.23.

## 14. REINFORCING BARS

All laps in reinforcing bars at splices shall be 30 diameters of the bar. All bars are designated on the plans by bar numbers. The bar size is indicated by the first digit of three-digit numbers and by the first two digits of four-digit

Clear distance from face of concrete to bars shall be 2 inches, except for slabs the clear distance shall be I inch or as shown on the plans.

### 15. ASPHALTIC CONCRETE SURFACE COURSE AND TYPE 'C' WATERPROOFING The asphaltic concrete wearing surface course and type "C" waterproofing are not a part of this contract.

## SUB-DRAINAGE FOR WEARING SURFACE COURSE

The copper tubes required on the bridge deck slab, for sub-drainage will be paid for at the contract unit price each bid for Item S-29. "Sub-Drainage for Wearing Surface Course". There shall be a line of copper tubes within one foot of each expansion joint, contraction joint, and roadway drain.

The steel angles will be included in a later contract with the asphaltic concrete wearing surface course and type "C" waterproofing.

## 17. CLEANING AND REPAIRING SUBSTRUCTURE

The Contractor shall, without additional compensation, clean and repair any portion of the substructure which is soiled or damaged as a result of his operations.

## 18. ELECTRICAL GROUNDS

All parts of the superstructure steelwork and the entire roadway lighting system shall be thoroughly grounded at pier shafts. The contractor for substructure will embed in the concrete of each of these pier shafts a No. O solid copper wire brazed at its lower end to a steel concrete pile casing, or steel pile, and at its upper end extending sufficiently above top of concrete to provide for convenient splicing and extension by the contractor for superstructure. At each such pier shaft the trusses shall be grounded by a No. 6 copper wire bolted or brazed to the bottom chord of the truss and to the bottom casting of the shoe, and carried to connection with the ground wire extending to the foundation pile. Across all roadway expansion joints at both trusses. there shall be provided a No. 6 stranded tinned copper wire suitably looped to allow

for expansion of the steelwork, and connected to each side of the expansion joint by boiling or brazing so as to provide an effective electrical connection for grounding the entire structural steelwork.

Payment will be made under "Item S-25, Electrical grounds",

#### PAINTING

Painting of superstructure metalwork shall be according to Item S-8 of the Construction and Material Specifications except as modified herein.

A. Coats of Paint. The paint shall be applied by brushing in four coats as

a. A first coat of red lead paint applied in the shop on clean metal surfaces prepared for painting as specified in Sec. S+8.03.

b. A second coat of red lead paint applied in the field after erection. For surfaces that will be inaccessible after erection, this second coat may be applied either in the shop or in the field.

c. A fhird and a fourth coat consisting of white lead paint. The fourth coat shall be finfed a medium shade of gray that meets the approval of the Director of Highways and the City of Cleveland.

d. Light standards and the steel parts of handrails shall be painted with a first and a second coat of red lead paint as specified for the remainder of the structural steel, but the third and fourth coats shall be of aluminum paint.

a. The paint to be used for the first and second red lead coats shall be of the following composition and properties:

Red Lead (97% grade) 99.6% (minimum) 0.3-0.4% Aluminum Stearate

Vehicle Raw Linseed Oil

35% to 50% \*Pale Heat Bodied Linseed Oil (Z2) 15% to 30%

Volatile Mineral Spirits and Drier

\*The acid number of this oil shall not be over 11, the color not darker than 7 (Gardiner 1933) and shall have a Wijs iodine value of 110-125.

Second Coat First Coat 73% (minimum) 77% (minimum) 23% (maximum) 27% (maximum) Vehicle 21.0 pounds (minimum) 24.0 pounds (minimum) Weight per gallon 175 grams to 250 grams (ASTM Method Consistency D562-42-T or Federal Specification TT-P-141a, Method 428.1)

Fineness of grind 5 (minimum) Drying Time

Set to touch Dry through

36 Hours (maximum) The paint shall be well ground, shall not settle excessively or cake in the container. shall be readily broken up with a paddle to a smooth uniform paint having good brushing properties. The paint when brushed on a clean, smooth steel panel maintained in

6 Hours (maximum)

35% (maximum)

unevenness, streaking, separation, running, curtaining and sagging. For contrast between the first and second coats, the second coat shall be finted with lampblack-in-cil to change its color to a chocolate brown.

c. The aluminum third and fourth coats of paint shall conform to Sec. >

a vertical position, shall dry to a smooth uniform finish free from roughness, grit,

b, The white lead third and fourth coats of paint shall conform to Sec. M-9.6 (b) of the Construction and Material Specifications.

N-9. 12 of the Construction and Material Specifications.

## GRAVEL

If gravel is used as the coarse aggregate it shall meet the requirements of Section M - 3.93 of the Construction and Material Specifications

FED. ROAD DIV. NO. TYPE FUNDS FEDERAL AID PROJECT NO. STATE 122 OHIO

CUYAHOGA COUNTY CITY OF CLEVELAND INNER BELT FREEWAY CENTRAL VIADUCT

PART 3

OHIO

INNER BELT FREEWAY - CENTRAL VIADUCT BR. NO. CU - 42 R - 17 5

GENERAL NOTES

U. S. ROUTE 42 RELOCATION

CUYAHOGA COUNTY CLEVELAND HOWARD, NEEDLES, TAMMEN & BERGENDOFF MADE GA DATE 10-6-54

TRCD\_\_\_\_DATE\_\_\_\_

CKD\_\_\_\_DATE\_\_\_\_

CONSULTING ENGINEERS CLEVELAND NEW YORK 914-1A SHEET- 2.03

